MDEQ SUBDIVISION APPLICATION REPORT

Horse Creek Hills 1 Subdivision

Located in a Portion of Section 31 Township 9 N, Range 2 E, P.M.M. Broadwater County, MT

> Project # 19-072 June 2020

> > **Prepared By:**



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June 11, 2020

Montana Department of Environmental Quality Rachel Clark, Engineering Bureau 1520 E Sixth Avenue PO Box 200901 Helena, MT 59620 Ph: 406-444-6722 E-Mail: rclark@mt.gov

RE: Horse Creek Hills 1 Subdivision Located in a Portion of Sec 31, T9N, R2E, P.M.M. Broadwater County, Montana

Dear Ms. Clark:

This report presents Allied Engineering's wastewater system evaluation for the Horse Creek Hills 1 Subdivision. The proposed project is located approximately 0.25 miles east of Canyon Ferry Reservoir at the location where Lower Confederate Road reaches the lake. The legal description of the approximately 435-acre is Section 31, Township 9 North, Range 2 East, Principal Meridian Montana, Broadwater County, Montana. The subject property is currently used for cattle grazing purposes.

In short, there are four different projects proposed to develop the property. The current projects are proposing to develop the subject property into a 41-lot major subdivision. Horse Creek Hills 1 Subdivision will be one of four projects through MDEQ and will consist of developing the 435-acre parcel into 11 residential lots and 1 commercial lot – ranging in size from 5-acres to 12-acres. The remaining portion of the property is proposed to be developed into residential and commercial lots in Subdivision projects #2-4.

Refer to the Test Well Drilling Program and Summary included in the appendix for details on how site-specific data was gathered in order to determine the groundwater gradient and direction, hydraulic conductivity, background nitrates, and overall subsurface properties. Nodegradation was evaluated on lots that did not meet the Categorical Exemption #1 as outlined in Appendix P of the Non-degradation manual. As a result, the non-degradation calculations shown in Appendix D show the worst-case scenario for the entire development as a whole – which includes the lots that were exempt from non-degradation review. However, lots that were exempt from non-degredation were not included in the cumulative effects calculations. Thus, only the lots that did not meet the requirements for exemption under Category #1 were evaluated for cumulative effects. The worst-case scenario for non-exempt lots in cumulative effects were lots 15 & 16 of Horse Creek Hills 2 Subdivision – as they were the closest in distance. Overall, a maximum of two total drainfields line up in the direction of groundwater in the entire development – thus lots 15 & 16 were the worst-case scenario for cumulative effects because they were the closest together of any of the drainfields that overlapped in the direction of groundwater.

Groundwater monitoring has been required by the Broadwater County Sanitarian for lots #1, 2, 3, & lot 41 (Horse Creek Hills 4 Subdivision). Signs of groundwater were not entirely evident during the site evaluation; however, monitoring is being required for these sites due to their proximity to Lower Confederate Creek.

An 8-hour pump test was conducted on a production well that was drilled on lot #13 of the Horse Creek Hills 2 Subdivision. Pumping was conducted at a rate of 15 gallons-per-minute for 8 hours in total. The production well was drilled beyond the upper 15-ft of the aquifer, and will be proposed to be utilized for lot #13 pending subdivision approval. The Razack Huntley equation was used to estimate Hydraulic conductivity based on the 8-hour pump test. This hydraulic conductivity value was used for non-degradation analysis for all four subdivision projects.

Each lot is proposed to be served by an onsite water supply well, and an on-site wastewater treatment system consisting of a septic tank and a subsurface gravity fed drainfield. The enclosed application is seeking approval for 11 lots located in a proposed subdivision with each lot consisting of one (1) single family dwelling with up to 5-bedrooms. Each lot in the proposed development corresponds to 400-gpd according to Circular DEQ-4. This project is also pursuing an approval of a proposed wastewater treatment systems to serve one (1) commercial lot with up-to 24 employees. According to Circular DEQ-4, the design wastewater flow for an employee in a commercial unit is 13-gallons per day, thus a commercial lot will have 312-gallonss per day of effluent flow.

As part of this application, a site evaluation was conducted, an extensive Test Well Drilling Program was completed, a non-degradation analysis has been performed, and a wastewater treatment system consisting of septic tanks and gravity fed drainfields have been proposed where wastewater systems were conservatively over-sized to ensure soils absorption over a larger area. The non-degradation analysis including cumulative effects shows the groundwater impacts will not be significant.

Vicinity maps, soils information, non-degradation analysis, wastewater sizing, etc. has been included in this report.

If you have any questions or comments, please contact the undersigned. Thank you.

Sincerely,

Allied Engineering Services, Inc.

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Hunter Morrical, El Staff Engineer

cc: 71 Ranch LP (Ownership Entity) Jesse Merrit (Project Representative)

> P:\2019\19-072 71 Ranch - Major Subdivision\04 Permitting & Entitlements\03 - MDEQ Sub Application\Horse Creek Hills 1 Subdivision\Documents\Horse Creek Hills 1 Sub-Cover Letter_2020_04_01.docx



I. INTRODUCTION

This report presents Allied Engineering's wastewater system evaluation for the Horse Creek Hills 1 Subdivision. The proposed project is located approximately 0.25 miles east of Canyon Ferry Reservoir at the location where Lower Confederate Road reaches the lake. The legal description of the approximately 435-acre is Section 31, Township 9 North, Range 2 East, Principal Meridian Montana, Broadwater County, Montana. The subject property is currently used for cattle grazing purposes. The current projects are proposing to develop the subject property into a 41-lot major subdivision.

The Horse Creek Hills 1 Subdivision is proposed to develop the underlying 435-acre property into eleven (11) residential lots and one (1) commercial lot. The rest of the property will be developed into residential and commercial lots in subsequent MDEQ subdivisions (Horse Creek Hills 2-4 Subdivisions). Lots int project #1 range in size from 5-acres to 12-acres. One open space lot will be included as part of the Horse Creek Hills 4 Subdivision.

Several dry gullies are within the extents of the property that show up as "Blue Line Streams" on the USGS 7.5k quad maps. The elevation of the groundwater in the property was measured using three test wells that were drilled into the first aquifer. The elevation of groundwater is considerably lower than the elevation of the dry gullies on site - thus the blue line streams can be shown to be losing streams. The elevation of groundwater is 3795' above sea level at the locations where the lower elevation of the dry gullies is approximately 3840' above sea level. Additionally, these dry gullies were walked by AESI staff and no noticeable springs or visible groundwater seepage into the gullies was observed.

Groundwater monitoring has been required by the Broadwater County Sanitarian for lots #1, 2, 3, & lot 41 (Horse Creek Hills 4 Subdivision). Signs of groundwater were not entirely evident during the site evaluation; however, monitoring is being required for these sites due to their proximity to Lower Confederate Creek.

Each lot is proposed to be served by an onsite water supply well, and an on-site wastewater treatment system consisting of a septic tank and a subsurface gravity fed drainfield.

The enclosed application is seeking approval for 11 residential lots located in a proposed subdivision with each lot consisting of one (1) single family dwelling with up to 5-bedrooms. Additionally, the application is seeking approval for 1 commercial lot that will not serve more than 24 employees utilizing up to 13gpd of wastewater. Each residential lot in the proposed development corresponds to 400-gpd according to Circular DEQ-4. The commercial lot in the subdivision corresponds to 312 -gpd according to Circular DEQ-4.

As part of this application, a site evaluation was conducted, a non-degradation analysis has been performed for Lots #1-4. Lots #5-12 were not evaluated for non-degradation, as they meet the Category

#1 exemption listed in Appendix P of the non-degradation manual. These lots meet this exemption as they: are greater than 1,000 feet from Canyon Ferry in the direction of groundwater; they have a perc rate between 16 and 50 mpi based on the soil type; they have soil profiles that show 6 feet or more of VFS, sCL, CL, or SiCL or finer; they have background nitrate levels in the first aquifer of less than 2 mg/l; the lots are larger than 2 acres; the percolation rate is greater than or equal to 16 mpi based on the soil texture type; the soil beneath the trench is VFS, SCL, or finer material; depth to bedrock was greater than 8-ft; and the separation between the proposed mixing zones and any water supply well is greater than 100-ft. See test pit logs in Appendix B for soil profile data. Wastewater treatment systems consisting of septic tanks and gravity fed drainfields has been proposed. The non-degradation analysis shows the groundwater impacts will not be significant. Please note that although this project was submitted concurrently with Horse Creek Hills 2-4 Subdivisions and presents some of the same information, they are separate projects.

Vicinity maps, soils information, non-degradation analysis, wastewater sizing, etc. has been included in this report.

II. WATER SUPPLY

Each lot is planned to be served by an onsite domestic water supply well. The approximate location of each proposed well is shown on the proposed Lot Layout (see Appendix Table of Contents). A pump test was conducted on a future water supply well that was drilled in November of 2019. The pump test was conducted for 8-hours, and the pump rate from the well was approximately 15gpm. The static water level in the well recovered in less than 8-hours, thus adequate water supply in the aquifer can be anticipated.

As part of our septic evaluation, a water sample was taken from the three on-site test wells that were drilled to the first aquifer, and analyzed for background nitrates, and conductivity. Samples were obtained in the upper 15 ft of the aquifer for each Test Well. The water sample analysis results found the following:

Sample Location	GWIC ID#	Nitrate and Nitrite as N	Conductivity
Sampie Zeession		(mg/L)	(uS/cm)
TW #1	304166	0.50	522
TW #2	304169	1.30	380
TW #3	304167	0.97	607

Table 1: Horse Creek Hills 1 Subdivision – Background Water Samples

The average background nitrate as outlined by the Non-degradation manual of 0.92 mg/L was used for this application.

III. WASTEWATER SYSTEM

Each of the proposed wastewater systems will consist of one (1) 1,500-gallon double compartment concrete septic tank with effluent filter and an individual sub-surface gravity fed drainfield. Test Pits were conducted in the areas of the proposed absorption areas and have been included in Appendix B.

Site Evaluation:

On February 6th and 10th of 2020, twelve (12) test pits were conducted by personnel from Allied Engineering Services, Inc. in the vicinity of Horse Creek Hills 1 Subdivision. We have also included the

test pits that were conducted as part of the overall development (Horse Creek Hills 2-4 Subdivisions). Overall, forty-four (44) test pits were excavated on the property as part of the overall development plan for wastewater system sizing.

Test pits logs for lots #1-12 are summarized below. The test pit number corresponds to the lot number on which it was excavated – i.e. Test pit #6 was excavated on lot #6. Complete test pit logs for all 4 subdivisions have been included as part of Appendix B. Additionally, hydrometer tests from six locations are included with the Test Pit logs. Hydrometer tests were performed on the material samples that best represented the majority of the test pits on-site - to help confirm on-site findings. Hydrometer test results corresponded with soil textures found in the lab after the test pit samples had been brought into the AESI laboratory. No groundwater, bedrock, or limiting layer was encountered.

Test Pit	Soil Texture	Percolation Rate (min/inch)	Application Rate – Test Pits (gpd/ft ²)	Application Rate – Perc Tests (gpd/ft ²)	* Required Absorption Area (ft ²)	Type of Wastewater System
TP-1	Silty Loam	16-31	0.4	N/A	780	Gravity-Fed
TP-2	Silty Loam	16-31	0.4	N/A	1,000	Gravity-Fed
TP-3	Silty Loam	16-31	0.4	N/A	1,000	Gravity-Fed
TP-4	Silty Loam	16-31	0.4	N/A	1,000	Gravity-Fed
TP-5	Silty Loam	16-31	0.4	N/A	1,000	Gravity-Fed
TP-6	Silty Loam	16-31	0.4	N/A	1,000	Gravity-Fed
TP-7	Silty Loam	16-31	0.4	N/A	1,000	Gravity-Fed
TP-8	Silty Loam	16-31	0.4	N/A	1,000	Gravity-Fed
TP-9	Silty Loam	16-31	0.4	N/A	1,000	Gravity-Fed
TP-10	Silty Loam	16-31	0.4	N/A	1,000	Gravity-Fed
TP-11	Silty Loam	16-31	0.4	N/A	1,000	Gravity-Fed
TP-12	Silty Loam	16-31	0.4	N/A	1,000	Gravity-Fed

Table 2: Horse Creek Hills 1 Subdivision – Test Pit Results

* Required Absorption for Residential Area based on (1) 5-bdrm home = 400-gpd

* Required Absorption for Commercial Area based on (1) Commercial building with less than or equal to 24 employees = 312-gpd

Soil survey data from the Natural Resources Conservation Service (NRCS) was evaluated as part of this application. Soil map units in the vicinity of the project location include AoB, AoC, Chc, MxE, MwE, and Te. The NRCS Engineering Properties for these map units range from Silt Loam to gravelly loam – as shown on the NRCS soil data included in Appendix B. NRCS data generally correlates with data found during the field investigations.

The proposed gravity fed drainfields have been sized according to the results obtained from test pits performed on-site which provide for an overall conservative application rate of 0.4 gpd/ft^2 for all lots per the sizing criteria of Circular DEQ-4, Chapter 2, Section 2.1.7.

The subject property is located within the FEMA FIRM Map Panel 30007C0350C – Included in Appendix E.

Wastewater System Sizing

A septic site plan has been provided for the proposed wastewater treatment systems (see Appendix Table of Contents). A master table shown on sheet WW3.4 of the design plans shows wastewater sizing for the entire development based on the soil profile corresponding to each lot. The primary and replacement areas are within 25 feet of the test pit locations.

Wastewater Flow. This project is pursuing an approval of a proposed wastewater treatment systems to each serve one (1) single family dwelling with up-to a 5-bedrooms for the residential lots. According to Circular DEQ-4, the design wastewater flow for a 5-bedroom home is 400-gallons per day. This project is also pursuing an approval of a proposed wastewater treatment systems to serve one (1) commercial lot with up-to 24 employees. According to Circular DEQ-4, the design wastewater flow for an employee in a commercial unit is 13-gallons per day, thus a commercial lot will have 312-gallonss per day of effluent flow.

Primary Treatment (Septic Tank Size). According to DEQ-4, a 5-bedroom home requires a 1,500-gallon septic tank. We are proposing to utilize one (1) 1,500-gallon double compartment concrete septic tank for the homes. The commercial lot will utilize one (1) 1,000-gallon double compartment concrete septic tank. The 1,000-gallon tank has more than 2.5 times the design flow, so it will be sufficient for the commercial lot.

Effluent Filter. All septic tank effluent must pass through an effluent filter, thus, an effluent filter will be installed in the septic tank. According to a standard maintenance frequency of 5-years, a 4" Biotube effluent filter is sufficient to accommodate the projected daily sewage flow of the 400-gpd for the proposed single-family home. A high level alarm is recommended to be installed in each septic tank to signal that the filter has clogged and needs maintenance.

Secondary Treatment (Drainfield Size). Wastewater treatment systems in the proposed subdivisions will vary slightly because of varying soil profiles and anticipated effluent flows. Because of this, four different drainfield designs have been established for the overall development and are shown on Sheets WW3.1 and WW3.2 of the design plans in Appendix H. A general table on Sheet WW3.4 outlines which system can be utilized on which lot. Additionally, the system type for each lot is shown on the proposed Subdivision Wastewater Treatment System overview sheets in the design plans.

If the system needs to be replaced, the 100% replacement is designated adjacent to the primary drainfield location and is sized assuming no reduction.

Gravity Distribution Design. The sewage gravity services will consist of 4-inch diameter Schedule 40 PVC solid sewer pipe. The sewage gravity line shall maintain grade (no humps or bellies) in order to allow for proper drainage, which will minimize the potential of freezing of the effluent in the pipe. The 4-inch diameter pipe will gravity to a distribution box. From the box, four or five (depending on the drainfield type) 4-inch Schedule 40 PVC solid sewer pipes will gravity to the proposed trenches. Depending on whether the owner chooses to install the standard trench or gravelless trench, the 4-in line will either run to the end of each lateral or terminate at the beginning of the infiltrator chamber – per manufacturer recommendations.

IV. SOLID WASTE DISPOSAL

Solid waste will be disposed of by individual lot owners at two different locations: – One waste container located and operated by Townsend Solid Waste - located in Townsend, Montana. The other location also operated by Townsend Solid Waste is at the Dry Gulch located – in Broadwater County.

V. DRAINAGE

A storm drainage evaluation has been performed as part of this application. Please see the appendix table of contents.

Non-Degradation Analysis

Based on our analysis, the new wastewater system improvements will have a non-significant impact on surface and ground water supplies. The closest distance to the nearest surface water in the direction of groundwater of greater than 1,000 feet. Lots #5-12 were not evaluated for non-degradation, as they meet the Category #1 exemption listed in Appendix P of the non-degradation manual. These lots meet this exemption as they: are greater than 1,000 feet from Canyon Ferry in the direction of groundwater; they have a perc rate between 16 and 50 mpi based on the soil type; they have soil profiles that show 6 feet or more of VFS, sCL, CL, or SiCL or finer; they have background nitrate levels in the first aquifer of less than 2 mg/l; the lots are larger than 2 acres; the percolation rate is greater than or equal to 16 mpi based on the soil texture type; the soil beneath the trench is VFS, SCL, or finer material; depth to bedrock was greater than 8-ft; and the separation between the proposed mixing zones and any water supply well is greater than 100-ft. When taking cumulative effects into account, the worst-case scenario for lots not meeting the categorical exemption was two drainfields overlapping together in the direction of groundwater. The worst-case scenario for the entire subdivision is two drainfields that are separated by 466 feet – those two lots being lot 15 & lot 16 of Horse Creek Hills 2 Subdivision. For the lot with the most downgradient overlapping wastewater systems (Lot 15), the phosphorous breakthrough is 155 years - accounting for the distance to surface water being the distance between drainfields. The nitrate concentration at the end of the final 200-ft mixing zone for lot 15 is 3.70 mg/L. Each of these values satisfies the non-degradation requirements of 5.0-mg/L for nitrate (maximum) and 50-year breakthrough for phosphorous (minimum). Besides the constant values that are accepted as input for all analyses and the dimensions of the drainfield areas, a few site-specific parameters were entered. A summary of the variables we selected and our reasoning is listed as follows:

Hydraulic Conductivity = 100.5-ft/day

The hydraulic conductivity was calculated using the Razack Huntley Equation on data obtained from an 8-hour pump test that was conducted on site. Pump test data has been included in Appendix D. Included are the pump test results from the three test wells that were drilled (TW-1, TW-2, TW-3). These wells were drilled into the first aquifer and pump test data from when they were drilled (11/26/19) was used along with the longer pump test from the production well to determine the average hydraulic conductivity for the aquifer.

Hydraulic Gradient = 0.0021 ft/ft

Hydraulic gradient and direction was determined using onsite monitoring wells that were part of an overall comprehensive groundwater monitoring well program and evaluation of the subject property. These wells were drilled to a depth of the first aquifer in November of 2019. The hydraulic gradient was determined to be 0.021 ft/ft with a direction of S38° 34' 40"W. A groundwater direction Exhibit has been included in Appendix A.

Mixing Zone Length = 200-ft

The acceptable mixing zone length based on each property size $(\pm 2.0 \text{ Acres})$ is 500-ft. However, a source specific mixing zone of 200-ft is being proposed for all lots within the project, as non-degradation calculations show a 200-ft mixing zone being acceptable given the site conditions.

 <u>Background Nitrate = 0.923-mg/L</u> Three nitrate concentrations from water samples taken from three onsite monitoring wells, in the top 15 ft of the first aquifer were analyzed – as shown in table 1 of this report. The three values were averaged together because the values do not differ significantly throughout the site – as outlined by the non-degradation manual.

- <u>Precipitation = 14-in/year</u> Based on information from the Western Regional Climate Center (see Appendix A).
- Depth to limiting layer = 9-ft

No groundwater or limiting layer was observed in the test pits that were performed near the vicinity of the proposed wastewater absorption systems. The Test Pits extended to a depth of at least 12-ft below ground surface throughout the subdivision, and a gravity fed drainfield is proposed with a trench depth of 24"-36" below ground surface.

Distance to Surface Water = 1,000-ft

Several dry gullies shown as blue line streams on the 7.5k quad map on-site have closer separations to drainfield than the above distance; however, because of the groundwater elevation related to the bottom of the gullies is significant, those dry gullies have been assumed to be losing. A minimum of 1,000-ft of separation between drainfields and surface water is required for the categorical exemption to remain in effect, thus 1,000 ft was conservatively analyzed as the distance to surface water. Canyon Ferry Reservoir is the closest surface water to any drainfield within the development, and it is greater than 1,000-ft away in the direction of groundwater. An adjacent to state waters calculation was conducted for the development and is shown in Appendix D. The calculation shows that impacts to surface water will be non-significant due to the large conveyance of Canyon Ferry Reservoir in relation to the number of drainfields being constructed.

SUBDIVISION REVIEW JOINT APPLICATION FORM

Montana Department of Environmental Quality Local Government Joint Application Form Parts I, II, III, IV, and Checklist

Section 76-4-129, Mont5ana Code Annotated (MCA), provides that this Subdivision Review Joint Application Form may be used to apply for Montana Department of Environmental Quality (DEQ) approval of subdivisions under the Sanitation in Subdivision laws and for subdivision approval by local governments under the Subdivision and Platting Act. The form replaces DEQ Form E.S. 91 and local preliminary plat approval forms. Landowners thus are relieved from the burden of providing similar information on different forms under two separate laws. <u>Please consult with your local planning board</u>, health department, or DEQ regarding the proper submittal of this application and supporting materials.

- A. When applying for subdivision review by the planning board and local governing body, the following parts of this form must be completed and submitted to the governing body or its designated agent.
 - 1. Part I must be completed for all subdivisions required to be reviewed and approved by the local governing body.
 - 2. Parts I, II, and III must be completed for all subdivisions for which local subdivision regulations require submittal of an environmental assessment.
- B. When applying for review of subdivisions by DEQ, Parts I and II of this form must be completed and submitted to DEQ. If the proposed subdivision is located in a county contracted to perform the review of subdivisions, the application must be submitted to the local health department.
- C. When applying for concurrent review of the subdivision by the local governing body and by DEQ, the following parts of this form must be completed and submitted to the local governing body or its designated agent, or to DEQ:
 - 1. Parts I and II must be completed for all subdivisions for which concurrent review is requested.
 - 2. Parts I, II and III must be completed for all subdivisions for which local subdivision regulations require submittal of an environmental assessment.
- D. Although not a requirement of this Joint Application, <u>it is highly recommended that the applicant</u> <u>complete Part IV Subdivision Checklist and submit the checklist with Part I and the information</u> <u>required by Part II</u>. The checklist identifies the application items (with references to applicable rules and technical circulars) that are typically required by the reviewing authority. Depending on the technical complexity of the proposed subdivision, the checklist may not necessarily identify all of the required application items. However, it does provide general guidance to assist the applicant in preparing a more complete application so as to expedite the review/approval process by the reviewing authority.

Copies of this Joint Application Form are available from:

- Montana Department of Environmental Quality, Permitting and Compliance Division;
- Montana Department of Commerce, Economic and Community Development Division;
- Local health departments and sanitarians; and
- Local planning offices.

MONTANA DEPARTMENT OF ENVIRONMENTAL QUALITY/ LOCAL GOVERNMENT JOINT APPLICATION FORM

PART I. GENERAL DESCRIPTION & INFORMATION

Name of proposed development: Horse Creek Hills 1 S	Subdivision
Location: City: <u>Townsend</u>	
	eocode: <u>43-1792-31-1-01-0000</u>
Legal description: $1/_4$ $1/_4$ of Section 3	
Type of Review Division of Land, Boundaries Relocated, or Removal of Restrictions Condominiums/Townhomes/Mobile Homes/Recreational Vehicles	Type of water supply system Individual well Individual surface water supply or spring Cistern Shared well (2 connections)
Rewrite – No Boundaries Changing, Aggregation, Change of Use Modified Site Plan Descriptive Data	Multiple-user (3-14 connections) Multiple-user (3-14 connections & < 25 people)
12 Number of lots Number of condominiums, townhomes, or	25+ people)
spaces	Type of wastewater treatment system
117.98 Total acreage of lots being reviewed Indicate the proposed/existing use(s) Residential, single family Residential, multiple family Type of multiple family structure (e.g. duplex) Planned unit development Condominium/townhomes Mobile home park Recreational vehicle park Other (please describe) Name of solid waste (garbage) disposal site:	 Individual wastewater treatment system Shared wastewater treatment system (2 connections) Multiple-user (3-14 connections & < 25 people) Service connection to multiple-user Extension of multiple-user main Service connection to public system Extension of public main New public system (15+ connections or serving 25+ people)
Designated representative, if any (e.g., engineer, surve	
	Allied Engineering Services, Inc.
Print name as my representative for purposes of this application. Address: <u>32 Discovery Drive, Bozeman MT 59718</u>	Print Company Name
Street or P.O. Box, C Email: mfasting@alliedengineering.com	Phone: <u>406-582-0221</u>
Owner Name: Errie J. Doett	71 Ranch, LP by Errol T. Galt, President
Signature of all owners of record Address: 40 71 Ranch Lane, Martinsdale, MT 59053	Print name of owner (s)
Street or P.O. Box, C	
Email: errol@71ranch.net	Phone: 406 572-3312
Date: 05/22/2020	
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Reviewer	Арр	licant	
Yes Missing NA	Initials	Page(s) in Report	ELEMENT DESCRIPTION
			General
			Application form provided & signed by owner, plus contact info for consultant.
			Filled out fee sheet & check made out to DEQ
			Completed & signed copy of Part 4 Checklist
			Vicinity Map Provided
			Copy of plat or COS (or deed if aliquot parts or proposing Aggregation of lots)
			4 copies of lot layout sheet(s); Facilities labeled as Existing or Proposed.
			Copy of any existing COSA for reviewed lot(s)
			Floodplains shown on drawings & any applicable documentation provided (LOMAs).
			Onsite Wastewater
			Copy of any existing WWTS permits for reviewed lot(s).
			Proof of pumping for septic tanks within last 3 years, unless system less than 5 years old.
			Soil profile descriptions
			Seasonal high groundwater addressed (results or letter indicating in process)
			Non-degradation
			Nondegradation info IF new development proposed, if expansion of existing development proposed, or for change in use (residential to commercial, etc.)
			Onsite Water
			Copy of any existing well logs for wells on reviewed lot(s), for wells sampled, & for wells used for hydraulic conductivity estimates
			Information about water quality, quantity & dependability (water tests & aquifer well logs)
			Public Water or Sewer
			If extensions or connections to existing public water/wastewater proposed, "will serve" letter or copy of current bill from public facility owner if connected
			Stormwater
			Stormwater drainage report & plans
			Other documents
			Special Requests - Prior to full design (waivers, deviations, water availability analysis, non- degradation predetermination, etc.)
			Sage Grouse documentation provided
			Copy of submittal to DNRC requesting Water Rights review or, if available, review letter from DNRC.
			Modified Site Plan
Copy of T	his check	list AND	circle one)
- •			NCOMPLETE LETTER sent on:
			AGENCY:

PART II REQUIRED INFORMATION FOR A OF SUBDIVISIONS UNDER SANITATION IN SUBDIVISIONS LAWS (e.g., parcels less than 20 acres, trailer courts, RV parks, condominiums)

All applications must include the information required in ARM 17.36.101-805 and the appropriate circulars. In order to facilitate review, the application should be organized in the same manner as this application form and follow closely the submittal requirements in the rules and circulars.

A. Physical Conditions

Provide the following attachments.

- 1. A vicinity map showing the location of the proposed subdivision in relation to the nearest town, highway(s).
- 2. Soils survey map and most recent interpretations of soil suitability for the proposed land uses.
- 3. Topographic map of the development with contour intervals meeting the preliminary plat requirements of the local subdivision regulations.
- 4. A copy of a preliminary plat* (a minor subdivision plat, if applicable) prepared in accordance with local subdivision regulations, or a final plat, show the location of:
 - a. Any rock outcroppings.
 - b. Any areas subject to flood hazard or, if available, 100- year floodplain studies. (The local floodplain administrator or the Floodplain Management Section of the Water Resources Division of the Department of Natural Resources and Conservation may be contracted for assistance in determining flood hazard locations.)
 - c. Any natural water systems such as streams, rivers, intermittent streams, lakes or wetlands. (Also indicate the names and sizes of each).
 - d. Any man-made water systems such as wells, ponds, canals, ditches, aqueducts, reservoirs and irrigation systems. (Also indicate the names, sizes and present use of each).
 - e. Any existing or proposed utilities located within or adjacent to the subdivision, including electrical power, natural gas, telephone service, and water and sewer pipelines or facilities.

*Submit a preliminary plat or certificate of survey with complete and accurate legal description adequate for DEQ to initiate and complete its review of the subdivision.

B. Water Supply

- 1. <u>Where an individual water supply system is proposed or existing for each parcel</u>
 - a. For a proposed system, provide all information required in ARM 17.36.328 336, indicate the distance to the nearest public water system.
 - b. If an existing system will be used, provide all information required in ARM 17.36.335.
 - c. Attach four copies of the lot layout showing the proposed or existing location of each water supply source (spring, well, or cistern) and indicating the distance to existing or proposed wastewater treatment systems.
- 2. <u>Where a multiple user water system is proposed or existing</u>
 - a. If an existing system will be used:
 - 1) Identify the system and the person, firm, or agency responsible for its operation and maintenance.
 - 2) Indicate the system's capacity to handle additional use and its distance from the development.
 - 3) Provide evidence that permission to connect has been granted.
 - 4) Provide three copies of the following attachments:
 - a) Map or plat showing location, sizes, and depth of any existing water supply lines and facilities that may directly serve parcels within the proposed development.

- Provide plans and specifications for all proposed extensions and b) additional lines and facilities as required by ARM 17.36.335 and DEO-3.
- b. If a new system will be used
 - 1) Indicate who will install the system, who will bear the costs, when it will be completed and who will own it.
 - Provide all information required in ARM 17.36.330 336 and DEQ-3. 2)
- 3. Where a public water system is proposed or existing
 - If an existing system will be used a
 - Identify the system and the person, firm, or agency responsible for its operation 1) and maintenance.
 - 2) Provide evidence that the system is approved by DEQ and is in compliance with the regulations.
 - 3) Provide evidence that the managing entity has authorized the connections, the system has adequate capacity to meet the needs of the subdivision, the system is in compliance with department regulations, and the appropriate water rights exist or have been applied for the connections.
 - 4) Provide three copies of the following as attachments.
 - a) A map or plat showing the location, sizes, and depth of any existing water lines and facilities that will directly serve parcels within the proposed development.
 - Plans and specifications for all proposed extensions and additional lines b) and facilities as required by ARM 17.36.328 - 330 and DEQ-1 or DEQ-3.
 - If a new system will be used b.
 - Indicate who will install the system, who will bear the costs, when it will be 1) completed, and who will own it.
 - 2) Provide plans and specifications for all proposed extensions and additional lines and facilities as required by ARM 17.36.328 - 330 and DEQ-1 or DEQ-3.

С. Wastewater Treatment

- 1. Where individual wastewater treatment systems are proposed for each parcel
 - a. Indicate the distance to the nearest public wastewater treatment system.
 - b. Provide all information required in ARM 17.36.320 - 345 and in DEQ-4.
- 2. For a proposed multiple user wastewater treatment system a.
 - Where an existing system is to be used
 - Identify the system and the person, firm, or agency responsible for its operation 1) and maintenance.
 - Indicate the system's capacity to handle additional use and its distance from the 2) development.
 - Provide evidence that permission to connect has been granted. 3)
 - Provide two copies of the following attachments. 4)
 - A map or plat showing the location, sizes, and depth of any existing a) sewer lines and facilities that will directly serve parcels within the proposed development.
 - Provide plans and specifications for all proposed extensions and b) additional lines and facilities as required by ARM 17.36.320-345 and DEQ-4.
 - Where a new system is proposed b.
 - Indicate who will install the system, who will bear the costs, when it will be 1) completed, and who will own it.
 - 3) Provide all information required in ARM 17.36.320 326 and DEQ-4.

3. For a proposed public wastewater treatment system:

- a. Where an existing system is to be used
 - 1) Identify the system and the person, firm, or agency responsible for its operation and maintenance.
 - 2) Provide evidence that the system is approved by DEQ and is in compliance with the regulations.
 - 3) Provide evidence that the managing entity has authorized the connections, the system has adequate capacity to meet the needs of the subdivision, and the system is in compliance with department regulations.
 - 4) Provide three copies of the following as attachments.
 - a) A map or plat showing the location, sizes, and depth of any existing sewer lines and facilities that will directly serve parcels within the proposed development.
 - b) Plans and specifications for all proposed extensions and additional lines and facilities as required by ARM 17.36.328 and DEQ-2 or DEQ-4.
- b. Where a new system is proposed
 - 1) Indicate who will install the system, who will bear the costs, when it will be completed, and who will own it.
 - Provide plans and specifications for all proposed extensions and additional lines and facilities as required by ARM 17.36.320 - 326 and DEQ-2 or DEQ-4. (Also see ARM 17.38.101).

D. Solid Waste

- 1. Describe the proposed method of collecting and disposing of solid waste.
- 2. Indicate the name and location of the department-licensed or appropriate out-of-state solid waste disposal site where solid waste will be disposed in accordance with ARM 17.36.309.

E. Drainage

- 1. Streets, roads, and unvegetated areas.
 - a. Describe measures for disposing of storm run-off from streets, roads, parking lots, and other unvegetated areas within the subdivision or onto adjacent property.
 - b. Indicate type of road surface proposed.
 - c. Describe facilities for stream or drainage crossing (e.g., culverts, bridges).
 - d. Describe how surface run-off will be drained or channeled from parcels.
 - e. Indicate if storm run-off will enter state waters and describe any proposed treatment measures. (A DEQ storm-water discharge permit may be required)
 - f. Describe any existing or proposed streambank or shoreline alteration, any proposed construction or modification of lakebeds or stream channels. Provide information on location, extent, type, and purpose of alternation.
 - g. Provide storm drainage plans and specifications as required by ARM 17.36.310 and DEQ-8.

- F. Other Permits That May Be Necessary
 - 1. Water Use Permit (Water Rights)

The Montana Water Law requires new water developments (after July 1, 1973) to be filed with the Department of Natural Resources and Conservation to receive a water right. For ground water developments, wells and developed springs, the amount of water to be used will determine which form to file with the department.

Form 602 – Notice of Completion of Ground Water Development This form is to be filed when the ground water development is a well, developed spring or a ground water pit. The amount of water to be used cannot exceed 35 gallons per minute or 10 acre-feet per year. The form is to be filed within 60 days after the well or spring development is completed and the water has been put to the intended beneficial use. Do not file until the well is hooked up and being used.

Form 600 – Application for Beneficial Water Use Permit When the ground water development is a well, developed spring or ground water pit and the intended use will be over 35 gallons per minute and 10 acre-feet per year, a water use permit must be issued <u>before</u> water can be appropriated. A correct and complete application with the criteria supplement and filing fee must be filed with the Department.

Forms are available at the Water Resources Regional Office at the following addresses: **Helena:** Water Resources Regional Office, 1424 9th Avenue, PO Box 201601, Helena,

- MT 59620-1601, 406-444-6999, or the regional office in your area
- **Billings:** Water Resources Regional Office, Airport Industrial Park, 1371 Rimtop Dr., Billings, MT, 59105-1978, 406-247-4415
- **Bozeman:** Water Resources Regional Office, 151 Evergreen Dr., Suite C, Bozeman, MT 59715, 406-586-3136
- **Glasgow:** Water Resources Regional Office, 222 6th St South, Glasgow, MT 59230, 406-228-2561
- Havre: Water Resources Regional Office, 210 6th Ave., Havre, MT 59501, 406-265-5516
- Kalispell: Water Resources Regional Office, 109 Cooperative Way, Suite 110, Kalispell, MT 59901, 406-752-2288
- Lewistown: Water Resources Regional Office, 613 NE Main St., Suite E, Lewistown, MT 59457, 406-538-7459
- Missoula: Water Resources Regional Office, Town & Country Shopping Center, 1610 S. Third St. West, Suite 103, Missoula, MT 59806, 406-721-4284
- For a complete listing of environmental permits required by the state, please reference the Montana Index of Environmental Permits from the Legislature Office of Environmental Quality (LEPO) at 406-444-3742 or visit the LEPO Web site: <u>http://www.leg.state.mt.us/css/publications/lepo/permit_index/permit_tofc.asp</u>. In addition, there may be other permits required by the federal government or local government agencies.
 - ____ Montana Department of Environmental Quality (DEQ), Water Quality web site (<u>deq.state.mt.us/wqinfo</u>)
 - MPDES Wastewater Discharge—All discharges to surface water, including those related to construction dewatering. Contact DEQ, Water Protection Bureau 406-444-3080.
 - ____ Storm Water Discharge—Construction activity greater than 1 acre disturbance. Contact DEQ, Water Protection Bureau 406-444-3080.

- MGWPCS Discharge—All construction and/or operation of wastewater impoundments or conveyances which may cause pollution of ground water. Also, includes land application of wastewater on a case-by-case basis. Contact DEQ, Water Protection Bureau at 406-444-3080.
- _____ 318 Authorization—Any activity in any state water that will cause unavoidable short-term violations of water quality standards. Contact DEQ, Water Protection Bureau at 406-444-3080.
- _____ 310 Permit/SPA (124)—Any activity that physically alters or modifies the bed or banks of a stream. Contact the local Conservation District.
- 404 Permit—Any activity resulting in the discharge or placement of dredged or fill material into waters of the U.S., including wetlands. Contact U.S. Army Corp of Engineers at 406-441-1375.
- Montana Land-Use License or Navigable Waters Easement—The construction, placement, or modification of a structure or improvement on land below the low water mark of navigable streams. Contact DNRC at 406-444-2074.
- Water Right Permit—Required before constructing new or additional diversion, withdrawal, impoundment, or distribution works for appropriation of ground water or surface water. Contact DNRC at 406-444-6614.
- Lakeshore Protection Act—Any project in or near a body of water within a county's jurisdictional area. Contact county government offices.
- Public Water Supply—New construction, alteration, extension or operation of a public water supply or non-State Revolving Fund (SRF) public sewage systems requires approval from the Department of Environmental Quality. Contact DEQ, Public Water and Subdivisions Review Bureau at 406-444-4400.
- Shoreline Protection—Any work in, over, or near any stream, river, lake, or wetland on the Flathead Reservation. Contact the Shoreline Protection Office at 406-883-2888 or 406-675-2700 ext. 7201.
- UST Permits—Activities involving any type of work related to underground storage tanks (petroleum and hazardous substances). Contact DEQ, Technical Services Bureau at 406-444-1420.
- ____ RW-20 Permit—A permit is required when work is to be done within a Montana Department of Transportation (MDT) right of way. Contact the local MDT District Office.
- Floodplain Development Permit—Anyone planning new construction within a designated 100-year floodplain. Contact DNRC, Water Operation Bureau, Floodplain Management at 406-444-0860 or local Floodplain Administrator.

PART III INFORMATION REQUIRED FOR ENVIRONMENTAL ASSESSMENT UNDER THE SUBDIVISION AND PLATTING ACT

Information specified in this Part must be provided in addition to that required in Parts I and II of this application form, when the preparation of an environmental assessment is required by the Montana Subdivision and Platting Act.

A. Geology

- 1. Locate on a copy of the preliminary plat, or on a plat overlay, any known hazards affecting the development that could result in property damage or personal injury due to:
 - a. Falls, slides or slumps soil, rock, mud, snow; or
 - b. Seismic activity.

Describe any proposed measures to prevent or reduce the danger of property damage or personal injury from any of these hazards.

2. Identify any geological conditions that might affect development, such as areas of bedrock, unsuitable soils, or high ground water. Describe any measures proposed to minimize the problems presented by the identified conditions.

B. Vegetation

- 1. Locate on a copy of the preliminary plat, or on a plat overlay, the location of the major vegetation types such as marsh, grassland, shrub, and forest.
- 2. Describe measures to be taken to protect trees and vegetative cover (e.g., design and location of lots, roads, and open spaces).
- 3. Identify areas containing noxious weed growth. Describe proposed means of weed control, especially to prevent weed growth on areas disturbed by construction.

C. Wildlife

- 1. Identify any major species of fish and wildlife use the area to be affected by the proposed subdivision.
- 2. Locate on a copy of the preliminary plat, or on a plat overlay, any known important wildlife areas, such as big game winter range, waterfowl nesting areas, habitat for rare or endangered species, and wetlands.
- 3. Describe any proposed measures to protect wildlife habitat or to minimize degradation (e.g., keeping buildings and roads away from shorelines or setting aside marshland as undeveloped open space).

D. Historical Features

- 1. Describe and locate on a copy of the preliminary plat, or on a plat overlay, any known or possible historic, archaeological, or cultural sites that may be affected by the proposed subdivision.
- 2. Describe any plans to protect such sites or properties.

E. Roads

- 1. Describe any required construction of new public or private access roads or substantial improvements to existing public or private access roads.
- 2. Describe the proposed closure or modification of any existing roads.
- 3. If any of the individual lots is accessed directly from an arterial street or road, explain why access was not provided by means of a frontage road or a road within the subdivision.
- 4. Indicate who will pay the costs of installing and maintaining dedicated or private roadways.

- a. Estimate how much daily traffic the subdivision, when fully developed, will generate on existing streets and arterials.
- b. Discuss the capability of existing and proposed roads to safely accommodate this increased traffic.
- c. Describe any increased maintenance problems and cost that will be caused by this increase in volume.
- 5. Describe any potential year-round accessibility concerns for conventional automobiles over legal rights-ofway available to the subdivision and to all lots and common facilities within the subdivision.
- 6. Identify the owners of any private property over which access to the subdivision will be provided and indicate whether easements for access have been obtained from those landowners.

F. Utilities

- 1. Identify the utility companies involved in providing electrical power, natural gas, and telephone service. Indicate whether utility lines will be placed underground.
- 2. Identify on the preliminary plat or overlay the locations of any needed utility easements [as required by 76-3-608(3)(c), MCA].
- 3. Indicate whether the preliminary plat has been submitted to affected utilities for review.
- 4. Estimate the completion date of each utility installation.

G. Emergency Services

- 1. Describe the emergency services available to the residents of the proposed subdivision, including number of personnel and number of vehicles or type of facilities and road distance to facilities for:
 - a. Fire protection Indicate whether the proposed subdivision is in an urban or rural fire district. If not, describe plans to form or extend an existing fire district, or describe other fire protection procedures. Where applicable, provide information regarding subdivisions planned in areas of high fire hazards.
 - b. Police protection.
 - c. Ambulance service.
 - d. Medical services.
- 2. Indicate whether the needs of the proposed subdivision for each of the above services will be met by present personnel and facilities.
 - a. If not, describe the additional expenses necessary to make these services adequate.
 - b. Explain who will pay for the necessary improvements.

H. Schools

- 1. Describe the available educational facilities that would serve this subdivision and the road distance to each.
- 2. Estimate the number of school children that will be added by the proposed subdivision. Provide a statement from the administrator of the appropriate school system indicating whether the increased enrollment can be accommodated by the present personnel and facilities and by the existing school bus system.

I. Land Use

- 1. Describe land uses on lands adjacent to the subdivision.
- 2. Describe any comprehensive plan or other land use regulations covering the area proposed for subdivision or adjacent land. If the subdivision is located near an incorporated city or town, describe any plans for annexation.

- 3. Where public lands are adjacent to or near the proposed development, describe the present and anticipated uses of those lands (e.g., grazing, logging, and recreation). Describe how the subdivision will affect access to any public lands.
- 4. Describe any health or safety hazards on or near the subdivision, such as mining activity, high-pressure gas lines, dilapidated structures, high-voltage power lines, or irrigation ditches. Any such conditions should be accurately described and their origin and location identified.
- 5. Describe any on-site or off-site uses creating a nuisance such as unpleasant odor, unusual noises, dust, or smoke. Any such conditions should be accurately described and the origin and location of each identified.

J. Parks and Recreation Facilities

Describe park and recreation facilities to be provided within the proposed subdivision and other recreational facilities that will serve the subdivision.

POSSIBLE SOURCES OF INFORMATION TO CONTACT WHEN COMPLETING THE FORM

Local Agencies_____

City or County Health Departm City Engineer or County Survey County Road Supervisor Conservation District County Extension Service Planning Board Staff Floodplain Administrator		School District Fire District or Departme Police or Sheriff's Depart Hospital or Ambulance S Chamber of Commerce Telephone, Electrical Pow Cable Companies	ment ervice
State Agencies	Information		Location
Dept of Fish, Wildlife, and Parks	Fisheries, vegetation and wildlife	on	Helena and regional offices
Dept of Environmental Quality	Water quality		Helena
Dept of Transportation	Access to state hig data maps, aerial p	5	Helena
Dept of Natural Resources and Conservation (DNRC)	Surface and ground floodplains, well lo rights, fire hazards	ogs, water	Helena and regional offices
Bureau of Mines and Geology	Geology, ground w quality well logs, t		Butte and Billings
Federal Agencies	Information		Location
Farm Service Agency	Aerial photographs	3	County offices
Bureau of Land Management	Vegetation, maps, topography		Billings and district offices

Topography, surface water,

fire hazards, maps

topographic maps

Soils, surface water,

flood hazards, erosion

soil maps, vegetation, wildlife

Geology, surface and ground water, water quality, floodways,

Forest Service

Geological Survey

Natural Resources Conservation Service Bozeman and county offices

Missoula regional,

national forest and

district offices

Helena

Part IV SUBDIVISION CHECKLIST

Subdivision:

E.Q. Number (provided by DEQ):

Please complete the checklist with your initials or N/A.

County: Date:

<u>Applicant</u> or <u>Representative</u> Initial or N/A	County Initial or N/A	DEQ Initial or N/A	Question	Refer to ARM 17.36 Subsections	Reviewer's Comments
			 Have deviation or waiver requests been submitted with appropriate fees? 	17.36.601	
			2. Is check included with correct fee?	17.36.103 and 17.36.802	
			3. Is application included with owner's signature/address/phone/date?	17.36.102	
			4. Is legible copy of Preliminary Plat or COS included?	17.36.103	
			5. Is legal description included on the Preliminary Plat or COS?	17.36.103	
			6. Are all lots described on survey being reviewed and any exclusions clearly stated on Preliminary Plat or COS?	17.36.103, 17.36.605	
			7. Are state letters of approval included (DNRC water rights permit, Groundwater discharge permit, public water etc.?	17.36.103	
			8. Is local health officer approval included?	17.36.103 , 17.36.106, 17.36.108	
			9. Are Planning Board or County Commissioner comments included?	17.36.103(1)(t)	
			10. Is a clear copy of USGS or other topo map included to show ground slope of property?	17.36.103 and 17.36.322 - subsurface wastewater treatment system (SWTS); 17.36.310 - stormwater;	
			11. Are 4 copies of lot layout included with the subdivision name on each?	17.36.103, 17.36.104, 17.36.112	
			12. Is all required information (e.g., scale, legend, north arrow, etc.) included on the lot layout?	17.36.104	
			13. Are locations of water and sewer lines (extensions and connections) shown?	17.36.104	
			14. Are on-site sewer systems designed in conformance with DEQ 4?	17.36.320	
			15. Is the slope given for drainfield areas?	17.36.104, 17.36.322	
			16. Is sewage treatment system type allowed?	17.36.321	
			17. Are drainfield replacement areas shown?	17.36.104	
			18. Are minimum setback requirements met?	17.36.323	
			19. Are soil pits (test holes) labeled, and adequate soil pit data provided?	17.36.104, 17.36.325	
			20. Are sewage system agreements, easements, O & M plan addressed?	17.36.326	
			21. Is information to verify depth to seasonal high ground water or bedrock provided?	17.36.325	
			22. If conducted, does perc test value(s) correspond to soil type?	17.36.325	
			23. Is gray water reuse system proposed?	17.36.319	
			24. Is adequate water supply quantity substantiated?	17.36.103, 17.36.330	
			25. Are water quality analyses (nitrate, nitrite, specific conductivity, and bac-T (for existing wells) provided, along with well log and well location?	17.36.331 (proposed) 17.36.335 (existing)	

			26. Is existing well over 25 ft. in depth and grouted to 25 feet?	17.36.335	
<u>Applicant</u> or <u>Representative</u> Initial or N/A	<u>County</u> Initial or N/A	DEQ Initial or N/A	Question	Refer to ARM 17.36 Subsections	Reviewer's Comments
			27. Will alternative water supply be used (cistern, spring)?	17.36.336	
			28. Is nondegradation addressed and supporting data to determine background water quality, hydraulic conductivity and hydraulic gradient provided?	17.36.103, 17.36.312, 17.30.501-518, 17.30.715	
			29. Is nitrate level at end of mixing zone < 5 ppm (< 7.5 ppm, if level 2 provided), and phosphorous breakthrough > 50 years <u>and</u> <u>trigger analysis for n and p</u> addressed?	17.36.103, 17.36.312, 17.30.715	
			30. Are all supporting legal documents included (shared users agreements easements, covenants, HOA,water/sewer districts)?	17.36.103, 17.36.326, 17.36.310, 17.36.334	
			31. Is a copy of the local septic permit (if issued) for an existing septic system provided?	17.36.327	
			32. Is a septic pumper's report stating an existing septic tank has been pumped within the last 3 years provided?	17.36.327	
			33. Is evidence demonstrating proper hydraulic functioning of an existing septic system provided?	17.36.327	
			34. Are wells, drainfields and/or mixing zones within 100 ft. perimeter outside of subdivision boundaries shown?	17.36.103, 17.36.104	
			35. Is proposed subdivision within 500 feet of public water supply and/or sewer system?	17.36.328	
			36. Is authorized statement to connect to existing public water and/or sewer system and statement of adequate capacity provided?	17.36.328	
			37. Is existing public water system approved by DEQ and PWS # provided?	17.36.328	
			38. Do appropriate water rights exist for the public water connection?	17.36.328	
			39. Are subdivisions adjacent to state waters addressed?	17.36.312	
			40. Are plans and specs stamped and signed by PE?	17.36.314	
			41. Is letter from owner stating PE certification of construction and "as-builts" will be submitted included?	17.36.314	
			42. Are 100-year floodplain requirements met, and floodplains and drainages shown?	17.36.104, 17.36.323, 17.36.324	
			43.Is solid waste disposal addressed?	17.36.103, 17.36.309 (waste stored on-site)	
			44. Has storm water drainage been addressed?	17.36.310, DEQ 8	

Notes:

 Applicant/representative:
 Name
 Date
 /

 County reviewer:
 Name
 Signature
 Date
 /

 DEQ reviewer:
 Name
 Signature
 Date
 /

Subdivision Review Fee Calculation Checklist

SUBDIVISION NAME: Horse Creek Hills 1 Subdivision EQ#

 $Choose \ type \ of \ lots, water \ system, was tewater \ system, \ nondegradation, \ and \ other \ components \ as \ necessary$

Condominium, trailer court, RV campground unit or space	Unit lot or parcel unit or space lot or parcel unit unit unit hour lineal foot lot/unit iot/unit oranfield design* drainfield hour unit* hour infield hour unit*	Unit cost \$160 \$60 \$90 \$110 \$400 \$130 \$0.30 \$90 \$90 \$120 \$240 \$240 \$60 \$120 \$120 \$130 \$130	Number of Units 12 12 12 12.00 If Required per 17.38.106 12 12 12 If Required 12 12 If Required 12 12 12 12 12 12 12 12 12 12 12 13 14 15 16 17 18 19 110 111 112 112 112 112 112 112 112 112 112 112 112 112 112 113 114 115 115 116 117 <th>Total (unit cost x no. of units) \$1,920.00 \$0.00 \$0.00 \$0.00 \$0.00 To be invoiced \$0.00 To be invoiced \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 \$0.00 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connection to distribution system Public water system DEQ 1 or DEQ 3 Water System TYPE OF WASTEWATER SYSTEM Existing systems New gravity fed system New gravity fed system New dosed systems, elevated sand mound, ET systems, intermittent sand filter, ETA system, recirculating sand filter, recirculating trickling filter, aerobic treatment unit, nutrient removal, and whole house subsurface drip irrigation *plus \$130 per hour for review in excess of 2 hours Gray water reuse, holding tanks, sealed pit privies, unsealed pit privies, seepage pits, waste segregation systems, experimental systems *plus \$130 per hour for review in excess of 2 hours New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system	lot/unit component unit drainfield design* drainfield hour unit* hour unit*	\$90 \$90 \$120 \$240 \$60 \$130 \$120	12	\$0.00 To be invoiced \$0.00 \$1,440.00 \$0.00 \$0.00 \$0.00 To be invoiced
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DEQ 1 or DEQ 3 Water System TYPE OF WASTEWATER SYSTEM Existing systems New gravity fed system New dosed systems, elevated sand mound, ET systems, intermittent sand filter, ETA system, recirculating sand filter, recirculating trickling filter, aerobic treatment unit, nutrient removal, and whole house subsurface drip irrigation *plus \$130 per hour for review in excess of 2 hours Gray water reuse, holding tanks, sealed pit privies, unsealed pit privies, seepage pits, waste segregation systems, experimental systems *plus \$130 per hour for review in excess of 2 hours New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system	unit drainfield design* drainfield hour unit* hour	\$120 \$240 \$60 \$130 \$120	12	\$0.00 \$1,440.00 \$0.00 \$0.00 To be invoiced
TYPE OF WASTEWATER SYSTEM Existing systems New gravity fed system New dosed systems, elevated sand mound, ET systems, intermittent sand filter, ETA system, recirculating sand filter, recirculating trickling filter, aerobic treatment unit, nutrient removal, and whole house subsurface drip irrigation *plus \$130 per hour for review in excess of 2 hours Gray water reuse, holding tanks, sealed pit privies, unsealed pit privies, seepage pits, waste segregation systems, *plus \$130 per hour for review in excess of 2 hours New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system	unit drainfield design* drainfield hour unit* hour	\$120 \$240 \$60 \$130 \$120	12	\$0.00 \$1,440.00 \$0.00 \$0.00 To be invoiced
Existing systems New gravity fed system New dosed systems, elevated sand mound, ET systems, intermittent sand filter, ETA system, recirculating sand filter, recirculating trickling filter, aerobic treatment unit, nutrient removal, and whole house subsurface drip irrigation *plus \$130 per hour for review in excess of 2 hours Gray water reuse, holding tanks, sealed pit privies, unsealed pit privies, seepage pits, waste segregation systems, experimental systems *plus \$130 per hour for review in excess of 2 hours New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system	drainfield design* drainfield hour unit* hour hour	\$120 \$240 \$60 \$130 \$120		\$1,440.00 \$0.00 \$0.00 To be invoiced
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New dosed systems, elevated sand mound, ET systems, intermittent sand filter, ETA system, recirculating sand filter, recirculating trickling filter, aerobic treatment unit, nutrient removal, and whole house subsurface drip irrigation *plus \$130 per hour for review in excess of 2 hours Gray water reuse, holding tanks, sealed pit privies, unsealed pit privies, seepage pits, waste segregation systems, experimental systems *plus \$130 per hour for review in excess of 2 hours New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system	design* drainfield hour unit*	\$240 \$60 \$130 \$120		\$0.00 \$0.00 To be invoiced
intermittent sand filter, ETA system, recirculating sand filter, recirculating trickling filter, aerobic treatment unit, nutrient removal, and whole house subsurface drip irrigation *plus \$130 per hour for review in excess of 2 hours Gray water reuse, holding tanks, sealed pit privies, unsealed pit privies, seepage pits, waste segregation systems, experimental systems *plus \$130 per hour for review in excess of 2 hours New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system	drainfield hour unit* hour	\$60 \$130 \$120	If Required	\$0.00 To be invoiced
recirculating trickling filter, aerobic treatment unit, nutrient removal, and whole house subsurface drip irrigation *plus \$130 per hour for review in excess of 2 hours Gray water reuse, holding tanks, sealed pit privies, unsealed pit privies, seepage pits, waste segregation systems, experimental systems *plus \$130 per hour for review in excess of 2 hours New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system	hour unit* hour	\$130 \$120	If Required	To be invoiced
nutrient removal, and whole house subsurface drip irrigation *plus \$130 per hour for review in excess of 2 hours Gray water reuse, holding tanks, sealed pit privies, unsealed pit privies, seepage pits, waste segregation systems, experimental systems *plus \$130 per hour for review in excess of 2 hours New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system	unit*	\$120	If Required	
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unsealed pit privies, seepage pits, waste segregation systems, experimental systems *plus \$130 per hour for review in excess of 2 hours New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system	hour			\$0.00
experimental systems *plus \$130 per hour for review in excess of 2 hours New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system		\$130		
*plus \$130 per hour for review in excess of 2 hours New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system		\$130		
New multiple user wastewater system (non-public) *plus \$130 per hour for review in excess of 4 hours new collection system		\$130		T I · · I
*plus \$130 per hour for review in excess of 4 hours new collection system	unit		If Required	To be invoiced
new collection system	hann	¢120	Per Type Above	To be invoiced
· · · · · · · · · · · · · · · · · · ·	hour lineal foot	\$130 \$0.30	If Required	To be invoiced \$0.00
	lot/unit	\$0.30 \$90		\$0.00
Public wastewater system	101/ uIIIt	390		\$0.00
Treatment System	component		per 17.38.106	To be invoiced
OTHER	component		per 17.50.100	To be involced
	#2 grup st*	\$250		\$0.00
Deviation from Circular	request* hour	\$250 \$130	If Dequined	
plus \$130 per hour for review in excess of 2 hours Waiver from Rules	request	\$130 \$250	If Required	To be invoiced \$0.00
*plus \$130 per hour for review in excess of 2 hours	hour	\$230 \$130		To be invoiced
Reissuance of original approval statement	request	\$130		\$0.00
Review of revised lot layout document	request	\$160		\$0.00
Municipal Facilities Exemption Checklist	request	\$100		\$0.00
Nondegradation review - nonsignificance determinations	request	\$120		\$0.00
individual/shared	drainfield*	\$70	3	\$210.00
*plus \$130 per hour for review in excess of 2 hours	hour	\$130	If Required	To be invoiced
	ot/structure*	\$40		\$0.00
*plus \$130 per hour for review in excess of 2 hours	hour	\$130	If Required	To be invoiced
source specific mixing zone	drainfield	\$250	1	\$250.00
public	drainfield	\$ 2 00	If Required	To be invoiced
*		0100	n Requireu	
Storm drainage plan review - DEQ-8 Simple plan review	project	\$130 \$220	1.00	\$0.00
Storm drainage plan review - DEQ-8 Standard plan review	project	\$220 \$50	1.00	\$220.00
nlug \$120 non hour for any in process of 20 minutes and let	lot	\$50 \$130	12	\$600.00 To be invoiced
*plus \$130 per hour for review in excess of 30 minutes per lot	hour	\$130	If Required	To be invoiced
Preparation of environmental impact statements/EAs	actual cost		If Required	To be invoiced
Review for compliance with ARM 17.30.718	0000001*	6000		۵۵ م ۵
New Level 2 System Approval	approval*	\$900 \$130	If Dog.	\$0.00
*plus \$130 per hour for review in excess of 6 hours DEQ Page 26 Intal Review Fee	hour	\$130	If Required	To be invoiced \$5,960.00

Revised 03/01/2020

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- NRCS Soils Information
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- DNRC Well Appropriations Letter
- DNRC Sage Grouse Habitat Inquiry
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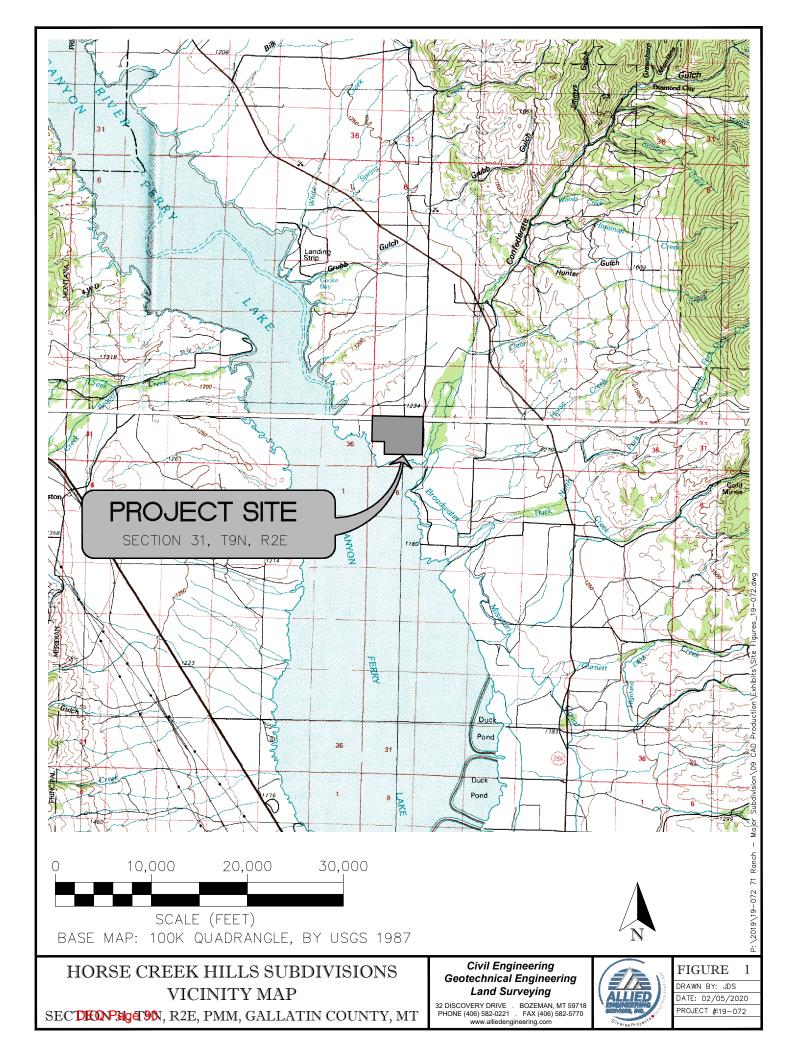
Appendix H – Wastewater System

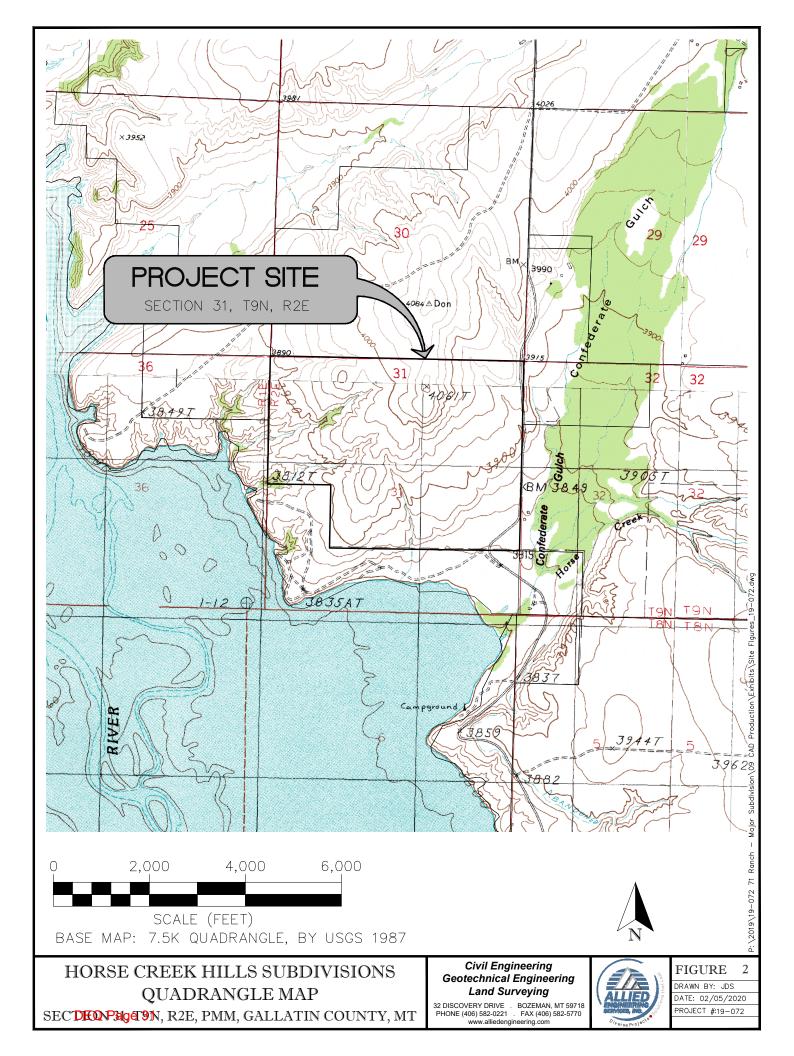
- Drainfield Sizing Calculations
- Biotube Effluent Filter Sizing
- Lot Layout (4 Copies)
- Details (4 Copies)

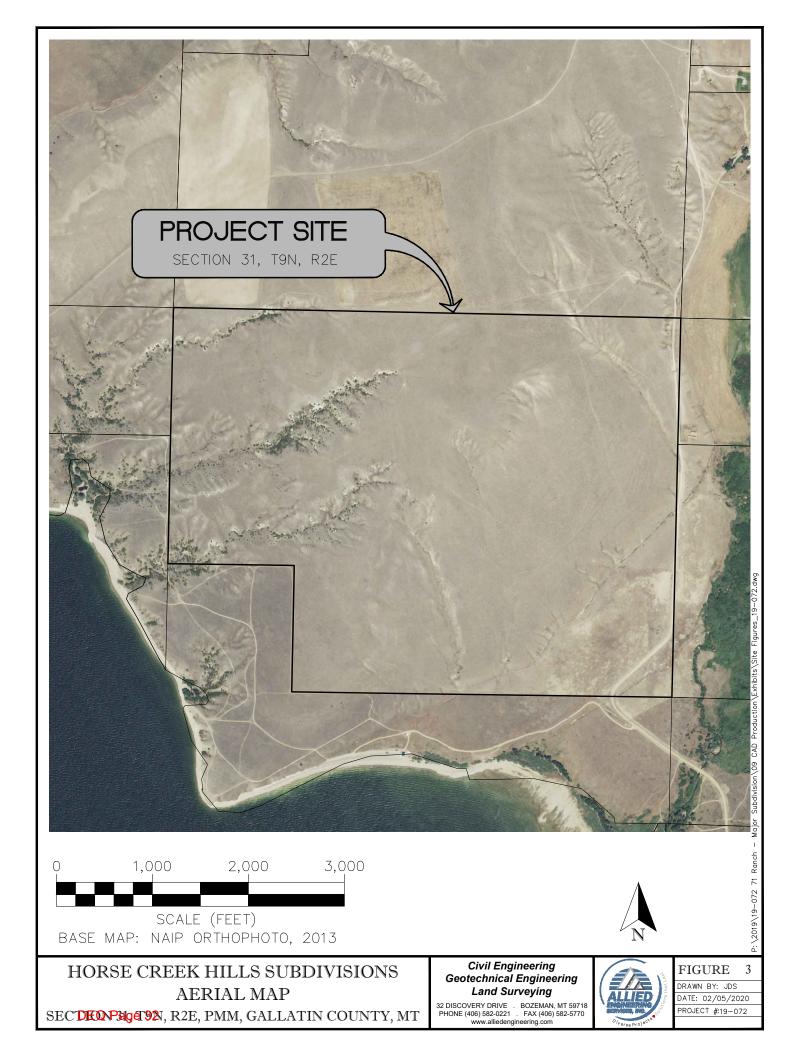
Appendix A

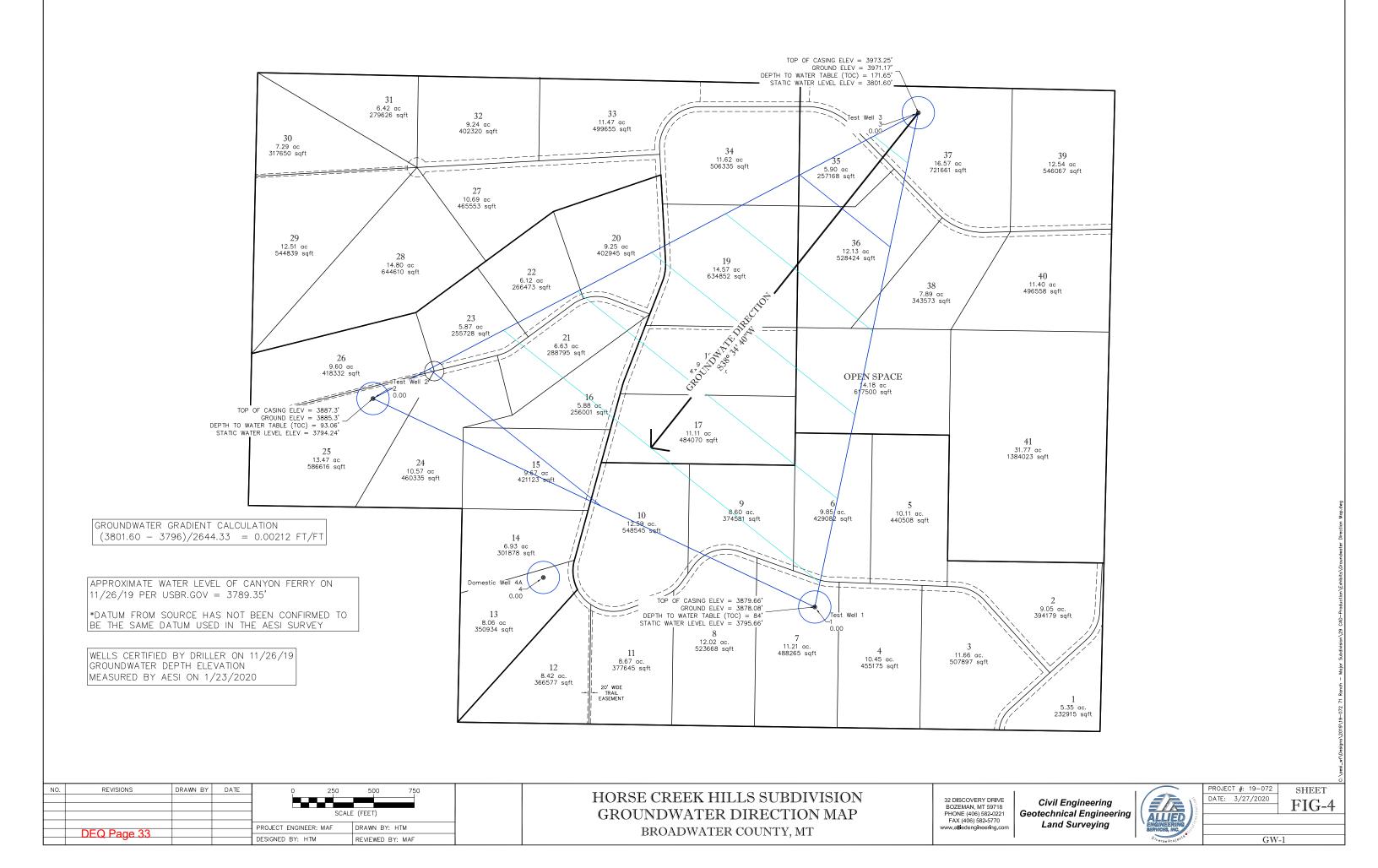
Vicinity Maps

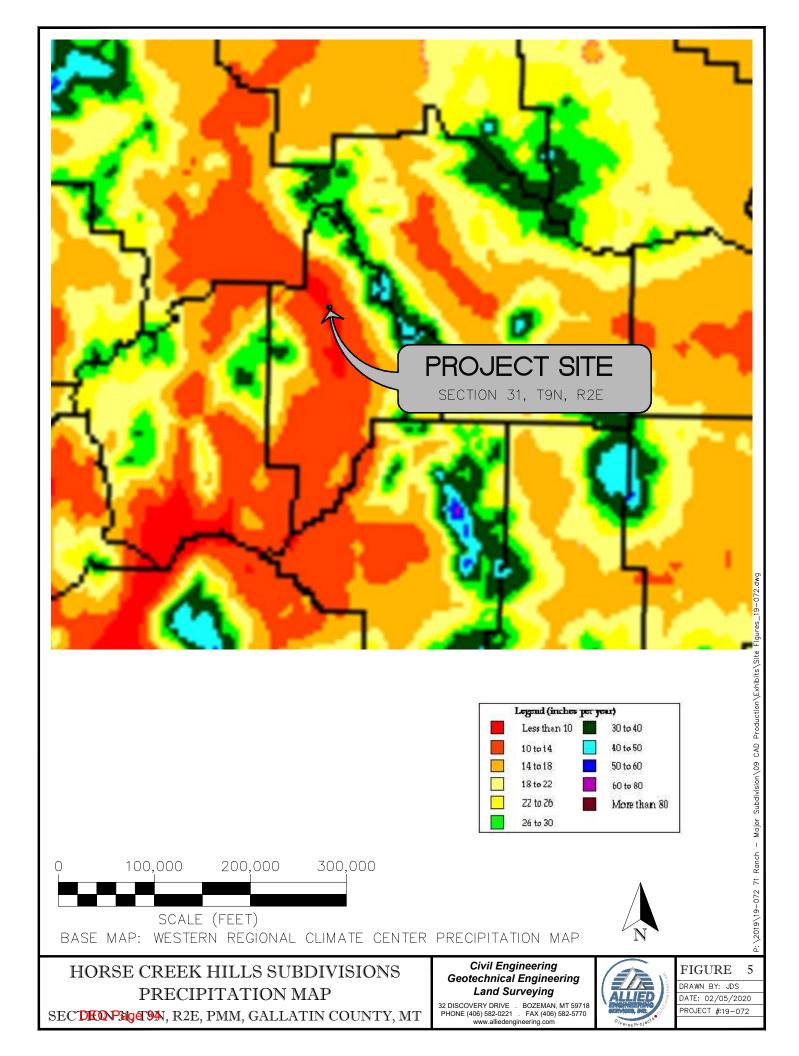
- Vicinity Map
- USGS Quadrangle Map
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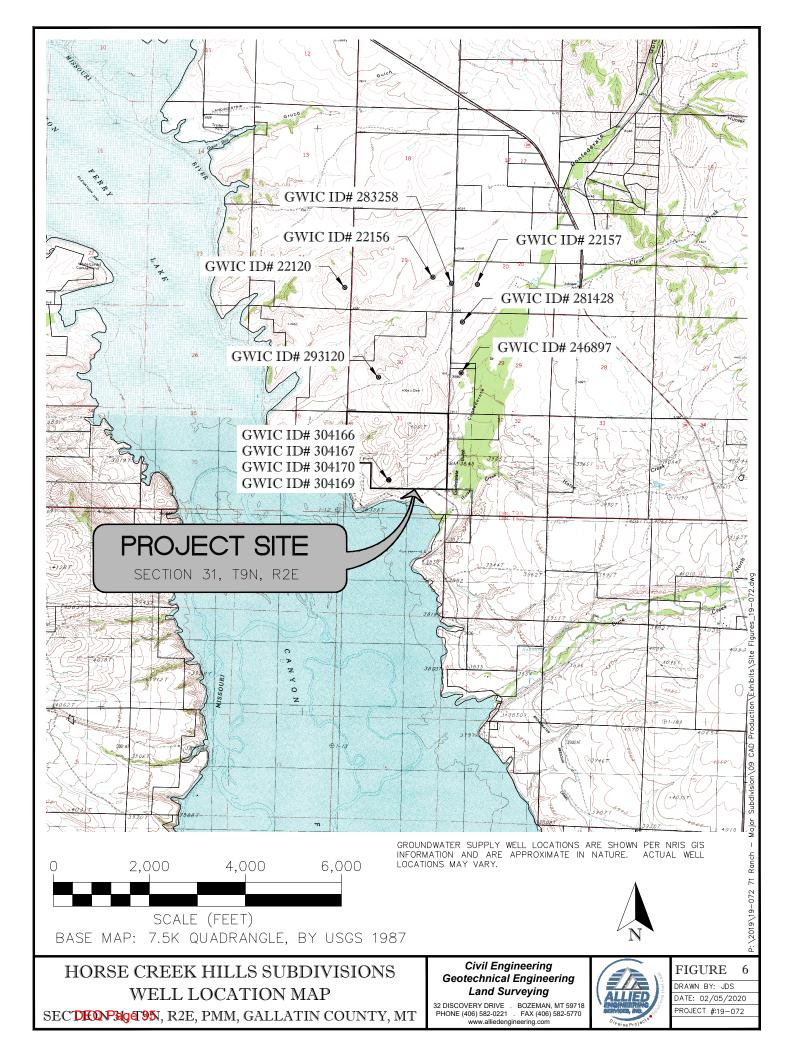


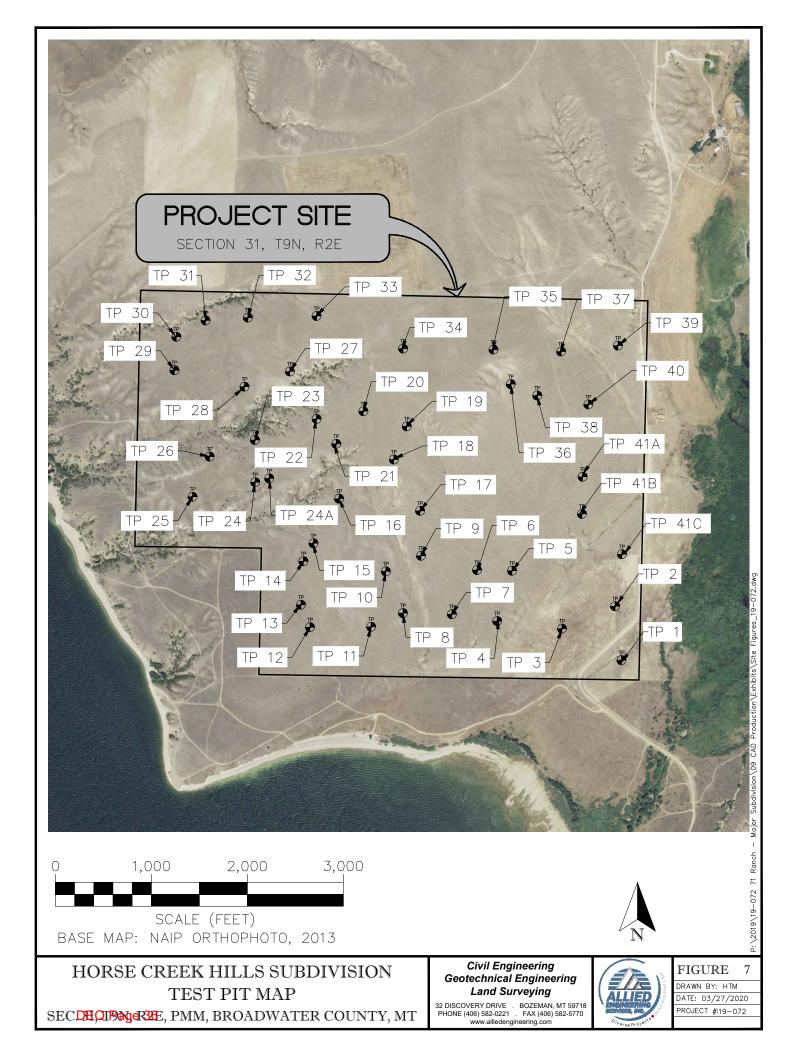








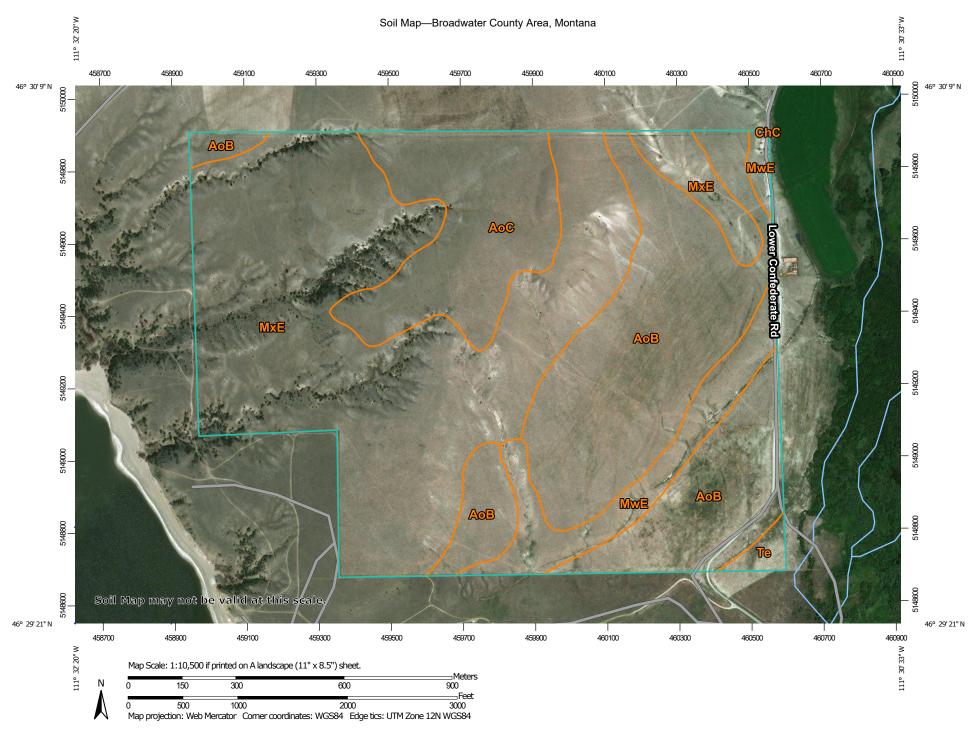




Appendix B

Soils Information

- NRCS Soils Map
- NRCS Soils Information
- Test Pit Logs



Conservation Service

5/28/2019 Page 1 of 3

MAP I	EGEND	MAP INFORMATION					
Area of Interest (AOI)	🗃 Spoil Area	The soil surveys that comprise your AOI were mapped at					
Area of Interest (AOI)	Stony Spot	1:24,000.					
Soils	Wery Stony Spot	Warning: Soil Map may not be valid at this scale.					
Soil Map Unit Polygons	wet Spot	Enlargement of maps beyond the scale of mapping can cause					
Soil Map Unit Lines	∆ Other	misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of					
Soil Map Unit Points	Special Line Features	contrasting soils that could have been shown at a more detaile					
Special Point Features	Water Features	scale.					
BlowoutBorrow Pit	Streams and Canals	Please rely on the bar scale on each map sheet for map measurements.					
X Clay Spot	Transportation ++++ Rails	Source of Map: Natural Resources Conservation Service Web Soil Survey URL:					
Closed Depression	Minterstate Highways	Coordinate System: Web Mercator (EPSG:3857)					
💥 Gravel Pit	US Routes	Maps from the Web Soil Survey are based on the Web Mercate					
Gravelly Spot	🧫 Major Roads	projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the					
🔕 Landfill	Local Roads	Albers equal-area conic projection, should be used if more					
🙏 🛛 Lava Flow	Background	accurate calculations of distance or area are required.					
Marsh or swamp	Aerial Photography	This product is generated from the USDA-NRCS certified data of the version date(s) listed below.					
Mine or Quarry Miscellaneous Water		Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 17, Sep 5, 2018					
Perennial Water		Soil map units are labeled (as space allows) for map scales					
Rock Outcrop		1:50,000 or larger.					
Saline Spot		Date(s) aerial images were photographed: Sep 10, 2012—Fe 15, 2017					
Sandy Spot		The orthophoto or other base map on which the soil lines were					
Severely Eroded Spot		compiled and digitized probably differs from the background					
Sinkhole		imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.					
Slide or Slip							
Sodic Spot							

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
АоВ	Amesha loam, 1 to 4 percent slopes	146.3	32.3%
AoC	Amesha loam, 4 to 9 percent slopes	58.4	12.9%
ChC	Chinook sandy loam, 4 to 9 percent slopes	0.0	0.0%
MwE	Musselshell-Crago channery loams, 15 to 35 percent slopes	31.7	7.0%
MxE	Musselshell-Crago cobbly loams, 8 to 20 percent slopes	213.5	47.1%
Те	Thess silt loam	3.4	0.8%
Totals for Area of Interest		453.4	100.0%



AoB—Amesha loam, 1 to 4 percent slopes

Map Unit Setting

National map unit symbol: 4ygg Elevation: 2,700 to 6,500 feet Mean annual precipitation: 10 to 14 inches Mean annual air temperature: 37 to 45 degrees F Frost-free period: 90 to 130 days Farmland classification: Prime farmland if irrigated

Map Unit Composition

Amesha and similar soils: 90 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Amesha

Setting

Landform: Alluvial fans, stream terraces Down-slope shape: Linear Across-slope shape: Linear

Typical profile

A - 0 to 4 inches: loam *Bk* - 4 to 49 inches: loam *C* - 49 to 74 inches: loam

Properties and qualities

Slope: 1 to 4 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 35 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: High (about 9.4 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 4e Hydrologic Soil Group: B Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT), Limy Grassland (R044BP804MT) Hydric soil rating: No

Minor Components

Mussel

Percent of map unit: 5 percent Landform: Fans, terraces Down-slope shape: Linear Across-slope shape: Linear Ecological site: Silty (Si) 10-14" p.z. (R044XC455MT) Hydric soil rating: No

Musselshell

Percent of map unit: 3 percent Landform: Terraces, fans Down-slope shape: Linear Across-slope shape: Linear Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT) Hydric soil rating: No

Amesha

Percent of map unit: 2 percent Landform: Alluvial fans, stream terraces Down-slope shape: Linear Across-slope shape: Linear Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT) Hydric soil rating: No

Data Source Information

Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 17, Sep 5, 2018

AoC—Amesha loam, 4 to 9 percent slopes

Map Unit Setting

National map unit symbol: 4ygh Elevation: 1,900 to 7,000 feet Mean annual precipitation: 10 to 14 inches Mean annual air temperature: 37 to 45 degrees F Frost-free period: 90 to 135 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Amesha and similar soils: 60 percent Minor components: 40 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Amesha

Setting

Landform: Alluvial fans, stream terraces Down-slope shape: Linear Across-slope shape: Linear

Typical profile

A - 0 to 4 inches: loam *Bk* - 4 to 49 inches: loam *C* - 49 to 74 inches: loam

Properties and qualities

Slope: 4 to 9 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 35 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: High (about 9.4 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 4e Hydrologic Soil Group: B Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT), Limy Grassland (R043BP804MT) Hydric soil rating: No

Minor Components

Amesha

Percent of map unit: 15 percent Landform: Alluvial fans, stream terraces Down-slope shape: Linear Across-slope shape: Linear Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT) Hydric soil rating: No

Chinook

Percent of map unit: 15 percent Landform: Hills, fans, terraces Down-slope shape: Linear Across-slope shape: Linear Ecological site: Sandy (Sy) 10-14" p.z. (R044XC451MT) Hydric soil rating: No

Crago

Percent of map unit: 10 percent Landform: Alluvial fans Down-slope shape: Linear Across-slope shape: Linear Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT) Hydric soil rating: No

Data Source Information

Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 17, Sep 5, 2018

ChC—Chinook sandy loam, 4 to 9 percent slopes

Map Unit Setting

National map unit symbol: 4ygy Elevation: 1,900 to 6,500 feet Mean annual precipitation: 10 to 14 inches Mean annual air temperature: 37 to 45 degrees F Frost-free period: 90 to 135 days Farmland classification: Prime farmland if irrigated

Map Unit Composition

Chinook and similar soils: 95 percent Minor components: 5 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Chinook

Setting

Landform: Hills, fans, terraces Down-slope shape: Linear Across-slope shape: Linear

Typical profile

Ap - 0 to 8 inches: sandy loam Bw - 8 to 14 inches: sandy loam Bk1 - 14 to 34 inches: sandy loam Bk2 - 34 to 60 inches: sandy loam

Properties and qualities

Slope: 4 to 9 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 15 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: Moderate (about 7.9 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 4e Hydrologic Soil Group: A Ecological site: Sandy (Sy) 10-14" p.z. (R044XC451MT), Upland Grassland (R044BP818MT) Hydric soil rating: No

Minor Components

Amesha

Percent of map unit: 5 percent Landform: Stream terraces, alluvial fans Down-slope shape: Linear Across-slope shape: Linear Ecological site: Sandy (Sy) 10-14" p.z. (R044XC451MT) Hydric soil rating: No

Data Source Information

Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 17, Sep 5, 2018



MwE—Musselshell-Crago channery loams, 15 to 35 percent slopes

Map Unit Setting

National map unit symbol: 4yhw Elevation: 1,900 to 7,000 feet Mean annual precipitation: 10 to 14 inches Mean annual air temperature: 37 to 45 degrees F Frost-free period: 90 to 135 days Farmland classification: Not prime farmland

Map Unit Composition

Musselshell and similar soils: 50 percent Crago and similar soils: 40 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Musselshell

Setting

Landform: Escarpments Down-slope shape: Linear Across-slope shape: Linear

Typical profile

A - 0 to 5 inches: channery loam Bk1 - 5 to 26 inches: gravelly loam Bk2 - 26 to 43 inches: gravelly loam 2C - 43 to 60 inches: very gravelly sandy loam

Properties and qualities

Slope: 15 to 35 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 60 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: Moderate (about 8.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6e Hydrologic Soil Group: B *Ecological site:* Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT), Limy Sagebrush Shrubland (R044BP805MT) *Hydric soil rating:* No

Description of Crago

Setting

Landform: Alluvial fans Down-slope shape: Linear Across-slope shape: Linear

Typical profile

A - 0 to 4 inches: channery loam

Bk1 - 4 to 27 inches: gravelly loam

Bk2 - 27 to 36 inches: extremely gravelly sandy loam

- 2C 36 to 60 inches: extremely gravelly loamy sand, extremely gravelly sandy loam, very gravelly sandy loam
- 2C 36 to 60 inches:
- 2C 36 to 60 inches:

Properties and qualities

Slope: 15 to 35 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 70 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)

Available water storage in profile: Low (about 4.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6e Hydrologic Soil Group: B Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT), Limy Sagebrush Shrubland (R044BP805MT) Hydric soil rating: No

Minor Components

Mussel

Percent of map unit: 5 percent Landform: Escarpments Down-slope shape: Linear Across-slope shape: Linear Ecological site: Silty (Si) 10-14" p.z. (R044XC455MT) Hydric soil rating: No

Cabbart

Percent of map unit: 3 percent

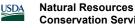
Landform: Hills, hills Down-slope shape: Linear Across-slope shape: Linear Ecological site: Shallow (Sw) 10-14" p.z. (R044XC452MT) Hydric soil rating: No

Rock outcrop

Percent of map unit: 2 percent Hydric soil rating: No

Data Source Information

Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 17, Sep 5, 2018



MxE—Musselshell-Crago cobbly loams, 8 to 20 percent slopes

Map Unit Setting

National map unit symbol: 4yhx Elevation: 2,400 to 7,000 feet Mean annual precipitation: 10 to 14 inches Mean annual air temperature: 37 to 45 degrees F Frost-free period: 70 to 135 days Farmland classification: Not prime farmland

Map Unit Composition

Musselshell and similar soils: 55 percent Crago and similar soils: 30 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Musselshell

Setting

Landform: Terraces, fans Down-slope shape: Linear Across-slope shape: Linear

Typical profile

A - 0 to 5 inches: cobbly loam Bk1 - 5 to 26 inches: gravelly loam Bk2 - 26 to 43 inches: gravelly loam 2C - 43 to 60 inches: very gravelly sandy loam

Properties and qualities

Slope: 8 to 20 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 60 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: Moderate (about 8.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6e Hydrologic Soil Group: B *Ecological site:* Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT), Limy Sagebrush Shrubland (R043BP805MT) *Hydric soil rating:* No

Description of Crago

Setting

Landform: Alluvial fans Down-slope shape: Linear Across-slope shape: Linear

Typical profile

A - 0 to 4 inches: cobbly loam Bk1 - 4 to 27 inches: gravelly loam Bk2 - 27 to 36 inches: extremely cobbly sandy loam 2C - 36 to 60 inches: extremely cobbly loamy sand

Properties and qualities

Slope: 8 to 20 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 70 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6e Hydrologic Soil Group: B Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT), Limy Sagebrush Shrubland (R043BP805MT) Hydric soil rating: No

Minor Components

Thess

Percent of map unit: 5 percent Landform: Fans Down-slope shape: Linear Across-slope shape: Linear Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT) Hydric soil rating: No

Thess

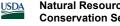
Percent of map unit: 5 percent Landform: Alluvial fans Down-slope shape: Linear Across-slope shape: Linear Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT) Hydric soil rating: No

Sappington

Percent of map unit: 5 percent Landform: Fans, hills Down-slope shape: Linear Across-slope shape: Linear Ecological site: Silty (Si) 10-14" p.z. (R044XC455MT) Hydric soil rating: No

Data Source Information

Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 17, Sep 5, 2018



Te—Thess silt loam

Map Unit Setting

National map unit symbol: 4yjh Elevation: 3,000 to 6,500 feet Mean annual precipitation: 10 to 14 inches Mean annual air temperature: 37 to 45 degrees F Frost-free period: 70 to 135 days Farmland classification: Prime farmland if irrigated

Map Unit Composition

Thess and similar soils: 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Thess

Setting

Landform: Terraces, fans Down-slope shape: Linear Across-slope shape: Linear

Typical profile

A - 0 to 5 inches: silt loam Bk - 5 to 22 inches: loam 2Bk - 22 to 60 inches: very gravelly sand

Properties and qualities

Slope: 1 to 3 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 40 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water storage in profile: Low (about 5.2 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 4e Hydrologic Soil Group: B Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT), Limy Grassland (R044BP804MT) Hydric soil rating: No

Minor Components

Amesha

Percent of map unit: 5 percent Landform: Alluvial fans, stream terraces Down-slope shape: Linear Across-slope shape: Linear Ecological site: Silty-Limy (SiLy) 10-14" p.z. (R044XC457MT) Hydric soil rating: No

Scravo

Percent of map unit: 5 percent Landform: Terraces, fans Down-slope shape: Linear Across-slope shape: Linear Ecological site: Shallow to Gravel (SwGr) 10-14" p.z. (R044XC454MT) Hydric soil rating: No

Toston

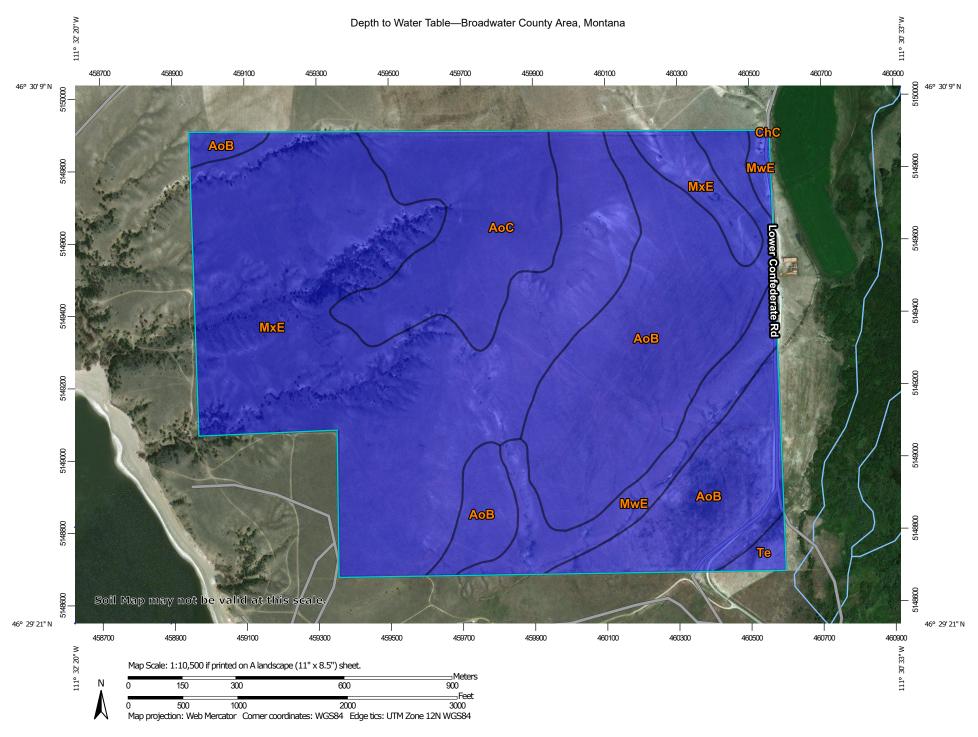
Percent of map unit: 5 percent Landform: Terraces Down-slope shape: Linear Across-slope shape: Linear Ecological site: Saline Lowland (SL) 10-14" p.z. (R044XC449MT) Hydric soil rating: No

Lothair

Percent of map unit: 5 percent Landform: Fans, terraces Down-slope shape: Linear Across-slope shape: Linear Ecological site: Clayey (Cy) 10-14" p.z. (R052XN162MT) Hydric soil rating: No

Data Source Information

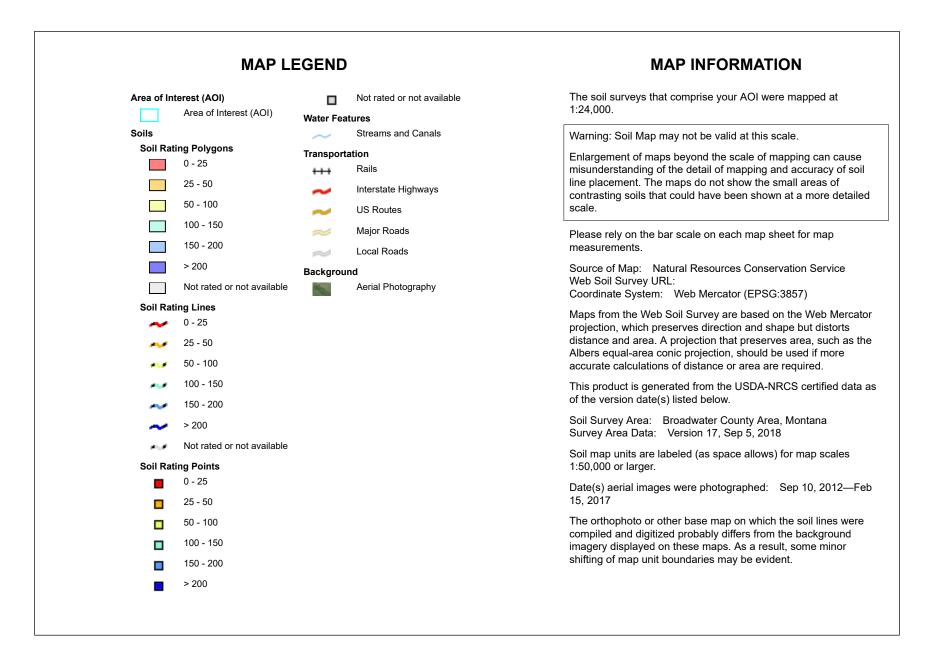
Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 17, Sep 5, 2018



DEQ Pageral Resources

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	1			
Map unit symbol	Map unit name	Rating (centimeters)	Acres in AOI	Percent of AOI
АоВ	Amesha loam, 1 to 4 percent slopes	>200	146.3	32.3%
AoC	Amesha loam, 4 to 9 percent slopes	>200	58.4	12.9%
ChC	Chinook sandy loam, 4 to 9 percent slopes	>200	0.0	0.0%
MwE	Musselshell-Crago channery loams, 15 to 35 percent slopes	>200	31.7	7.0%
MxE	Musselshell-Crago cobbly loams, 8 to 20 percent slopes	>200	213.5	47.1%
Те	Thess silt loam	>200	3.4	0.8%
Totals for Area of Inter	est		453.4	100.0%

Depth to Water Table

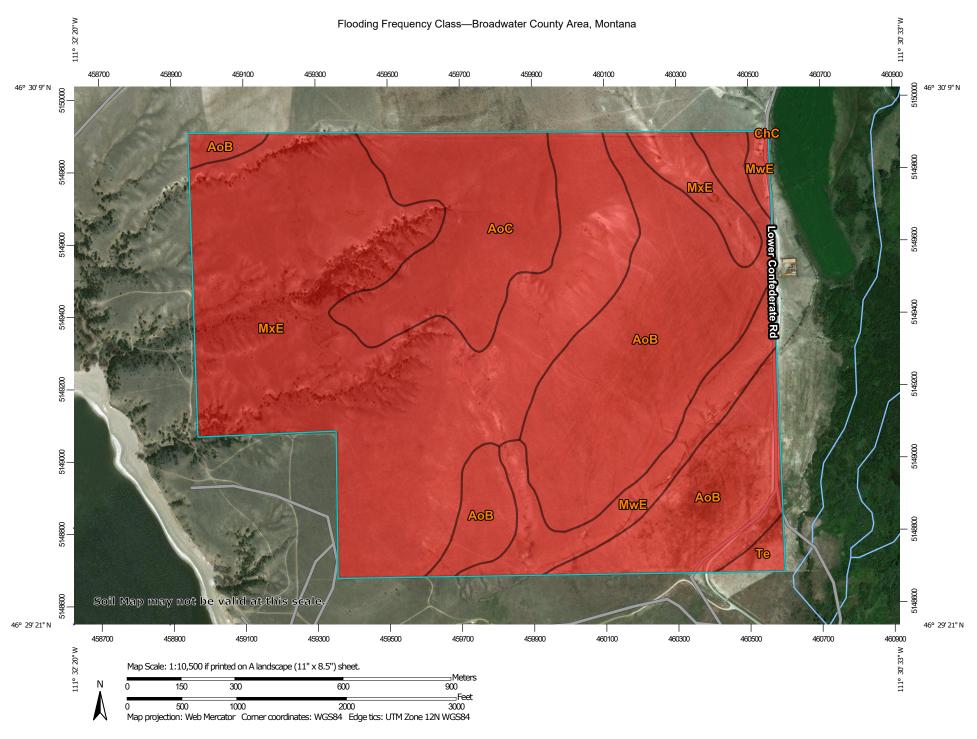
Description

"Water table" refers to a saturated zone in the soil. It occurs during specified months. Estimates of the upper limit are based mainly on observations of the water table at selected sites and on evidence of a saturated zone, namely grayish colors (redoximorphic features) in the soil. A saturated zone that lasts for less than a month is not considered a water table.

This attribute is actually recorded as three separate values in the database. A low value and a high value indicate the range of this attribute for the soil component. A "representative" value indicates the expected value of this attribute for the component. For this soil property, only the representative value is used.

Rating Options

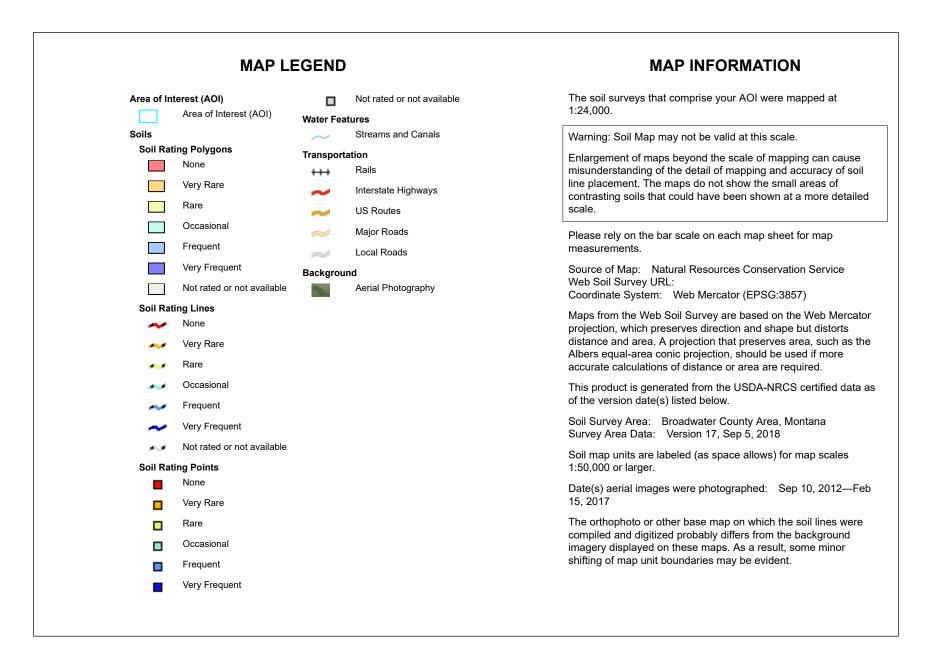
Units of Measure: centimeters Aggregation Method: Dominant Component Component Percent Cutoff: None Specified Tie-break Rule: Lower Interpret Nulls as Zero: No Beginning Month: January Ending Month: December



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Flooding Frequency Class

		1		
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
АоВ	Amesha loam, 1 to 4 percent slopes	None	146.3	32.3%
AoC	Amesha loam, 4 to 9 percent slopes	None	58.4	12.9%
ChC	Chinook sandy loam, 4 to 9 percent slopes	None	0.0	0.0%
MwE	Musselshell-Crago channery loams, 15 to 35 percent slopes	None	31.7	7.0%
MxE	Musselshell-Crago cobbly loams, 8 to 20 percent slopes	None	213.5	47.1%
Те	Thess silt loam	None	3.4	0.8%
Totals for Area of Inter	rest		453.4	100.0%



Description

Flooding is the temporary inundation of an area caused by overflowing streams, by runoff from adjacent slopes, or by tides. Water standing for short periods after rainfall or snowmelt is not considered flooding, and water standing in swamps and marshes is considered ponding rather than flooding.

Frequency is expressed as none, very rare, rare, occasional, frequent, and very frequent.

"None" means that flooding is not probable. The chance of flooding is nearly 0 percent in any year. Flooding occurs less than once in 500 years.

"Very rare" means that flooding is very unlikely but possible under extremely unusual weather conditions. The chance of flooding is less than 1 percent in any year.

"Rare" means that flooding is unlikely but possible under unusual weather conditions. The chance of flooding is 1 to 5 percent in any year.

"Occasional" means that flooding occurs infrequently under normal weather conditions. The chance of flooding is 5 to 50 percent in any year.

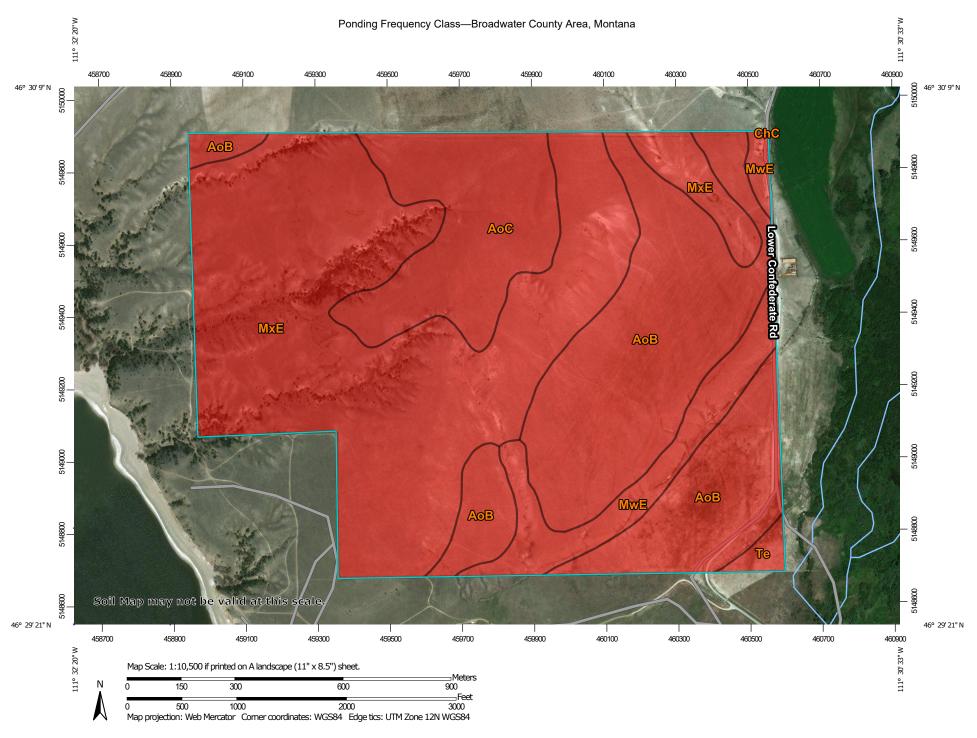
"Frequent" means that flooding is likely to occur often under normal weather conditions. The chance of flooding is more than 50 percent in any year but is less than 50 percent in all months in any year.

"Very frequent" means that flooding is likely to occur very often under normal weather conditions. The chance of flooding is more than 50 percent in all months of any year.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: More Frequent Beginning Month: January Ending Month: December





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MAP I	LEGEND	MAP INFORMATION
Area of Interest (AOI) Area of Interest (AOI) Soils	US Routes Major Roads	The soil surveys that comprise your AOI were mapped at 1:24,000.
Soil Rating Polygons None Rare Occasional Frequent Not rated or not available	e Local Roads	Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of so line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detail scale. Please rely on the bar scale on each map sheet for map measurements.
Soil Rating Lines None Rare Occasional Frequent		Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857) Maps from the Web Soil Survey are based on the Web Merca projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as t Albers equal-area conic projection, should be used if more
Not rated or not available	e	accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data of the version date(s) listed below.
RareOccasionalFrequent		Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 17, Sep 5, 2018 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.
Not rated or not available Water Features	e	Date(s) aerial images were photographed: Sep 10, 2012—F 15, 2017
Streams and Canals Transportation Rails Interstate Highways		The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

		-		
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
АоВ	Amesha loam, 1 to 4 percent slopes	None	146.3	32.3%
AoC	Amesha loam, 4 to 9 percent slopes	None	58.4	12.9%
ChC	Chinook sandy loam, 4 to 9 percent slopes	None	0.0	0.0%
MwE	Musselshell-Crago channery loams, 15 to 35 percent slopes	None	31.7	7.0%
MxE	Musselshell-Crago cobbly loams, 8 to 20 percent slopes	None	213.5	47.1%
Те	Thess silt loam	None	3.4	0.8%
Totals for Area of Inter	est		453.4	100.0%

Ponding Frequency Class

Description

Ponding is standing water in a closed depression. The water is removed only by deep percolation, transpiration, or evaporation or by a combination of these processes. Ponding frequency classes are based on the number of times that ponding occurs over a given period. Frequency is expressed as none, rare, occasional, and frequent.

"None" means that ponding is not probable. The chance of ponding is nearly 0 percent in any year.

"Rare" means that ponding is unlikely but possible under unusual weather conditions. The chance of ponding is nearly 0 percent to 5 percent in any year.

"Occasional" means that ponding occurs, on the average, once or less in 2 years. The chance of ponding is 5 to 50 percent in any year.

"Frequent" means that ponding occurs, on the average, more than once in 2 years. The chance of ponding is more than 50 percent in any year.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: More Frequent Beginning Month: January Ending Month: December



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Engineering Properties

This table gives the engineering classifications and the range of engineering properties for the layers of each soil in the survey area.

Hydrologic soil group is a group of soils having similar runoff potential under similar storm and cover conditions. The criteria for determining Hydrologic soil group is found in the National Engineering Handbook, Chapter 7 issued May 2007(http://directives.sc.egov.usda.gov/OpenNonWebContent.aspx? content=17757.wba). Listing HSGs by soil map unit component and not by soil series is a new concept for the engineers. Past engineering references contained lists of HSGs by soil series. Soil series are continually being defined and redefined, and the list of soil series names changes so frequently as to make the task of maintaining a single national list virtually impossible. Therefore, the criteria is now used to calculate the HSG using the component soil properties and no such national series lists will be maintained. All such references are obsolete and their use should be discontinued. Soil properties that influence runoff potential are those that influence the minimum rate of infiltration for a bare soil after prolonged wetting and when not frozen. These properties are depth to a seasonal high water table, saturated hydraulic conductivity after prolonged wetting, and depth to a layer with a very slow water transmission rate. Changes in soil properties caused by land management or climate changes also cause the hydrologic soil group to change. The influence of ground cover is treated independently. There are four hydrologic soil groups, A, B, C, and D, and three dual groups, A/D, B/D, and C/D. In the dual groups, the first letter is for drained areas and the second letter is for undrained areas.

The four hydrologic soil groups are described in the following paragraphs:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

Depth to the upper and lower boundaries of each layer is indicated.

Texture is given in the standard terms used by the U.S. Department of Agriculture. These terms are defined according to percentages of sand, silt, and clay in the fraction of the soil that is less than 2 millimeters in diameter. "Loam," for example, is soil that is 7 to 27 percent clay, 28 to 50 percent silt, and less than 52 percent sand. If the content of particles coarser than sand is 15 percent or more, an appropriate modifier is added, for example, "gravelly."

Classification of the soils is determined according to the Unified soil classification system (ASTM, 2005) and the system adopted by the American Association of State Highway and Transportation Officials (AASHTO, 2004).

The Unified system classifies soils according to properties that affect their use as construction material. Soils are classified according to particle-size distribution of the fraction less than 3 inches in diameter and according to plasticity index, liquid limit, and organic matter content. Sandy and gravelly soils are identified as GW, GP, GM, GC, SW, SP, SM, and SC; silty and clayey soils as ML, CL, OL, MH, CH, and OH; and highly organic soils as PT. Soils exhibiting engineering properties of two groups can have a dual classification, for example, CL-ML.

The AASHTO system classifies soils according to those properties that affect roadway construction and maintenance. In this system, the fraction of a mineral soil that is less than 3 inches in diameter is classified in one of seven groups from A-1 through A-7 on the basis of particle-size distribution, liquid limit, and plasticity index. Soils in group A-1 are coarse grained and low in content of fines (silt and clay). At the other extreme, soils in group A-7 are fine grained. Highly organic soils are classified in group A-8 on the basis of visual inspection.

If laboratory data are available, the A-1, A-2, and A-7 groups are further classified as A-1-a, A-1-b, A-2-4, A-2-5, A-2-6, A-2-7, A-7-5, or A-7-6. As an additional refinement, the suitability of a soil as subgrade material can be indicated by a group index number. Group index numbers range from 0 for the best subgrade material to 20 or higher for the poorest.

Percentage of rock fragments larger than 10 inches in diameter and 3 to 10 inches in diameter are indicated as a percentage of the total soil on a dry-weight basis. The percentages are estimates determined mainly by converting volume percentage in the field to weight percentage. Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

Percentage (of soil particles) passing designated sieves is the percentage of the soil fraction less than 3 inches in diameter based on an ovendry weight. The sieves, numbers 4, 10, 40, and 200 (USA Standard Series), have openings of 4.76, 2.00, 0.420, and 0.074 millimeters, respectively. Estimates are based on laboratory tests of soils sampled in the survey area and in nearby areas and on estimates made in the field. Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

Liquid limit and *plasticity index* (Atterberg limits) indicate the plasticity characteristics of a soil. The estimates are based on test data from the survey area or from nearby areas and on field examination. Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

References:

American Association of State Highway and Transportation Officials (AASHTO). 2004. Standard specifications for transportation materials and methods of sampling and testing. 24th edition.

American Society for Testing and Materials (ASTM). 2005. Standard classification of soils for engineering purposes. ASTM Standard D2487-00.

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Report—Engineering Properties

Absence of an entry indicates that the data were not estimated. The asterisk '*' denotes the representative texture; other possible textures follow the dash. The criteria for determining the hydrologic soil group for individual soil components is found in the National Engineering Handbook, Chapter 7 issued May 2007(http://directives.sc.egov.usda.gov/ OpenNonWebContent.aspx?content=17757.wba). Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

	Engineering Properties–Broadwater County Area, Montana													
Map unit symbol and	Pct. of	Hydrolo	Depth	USDA texture	Classi	fication	Pct Fra	agments	Percentage passing sieve number—					Plasticit
soil name	map unit	gic group			Unified	AASHTO	>10 inches	3-10 inches	4	10	40	200	limit	y index
			In				L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H
AoB—Amesha loam, 1 to 4 percent slopes														
Amesha	90	В	0-4	Loam	CL, CL- ML	A-4, A-6	0- 0- 0	0- 0- 0	95-98-1 00	90-95-1 00	70-80- 90	55-65- 75	25-30 -35	5-10-15
			4-49	Loam, sandy loam, silt loam	CL-ML, ML	A-4	0- 0- 0	0- 3- 5	95-98-1 00	90-95-1 00	70-80- 90	55-65- 75	20-25 -30	NP-5 -10
			49-74	Loam, fine sandy loam, gravelly sandy loam	CL-ML, ML, SC- SM, SM	A-2, A-4	0- 0- 0	0- 5- 10	65-83-1 00	55-78-1 00	45-65- 85	25-45- 65	20-25 -30	NP-5 -10
AoC—Amesha loam, 4 to 9 percent slopes														
Amesha	60	В	0-4	Loam	CL, CL- ML	A-4, A-6	0- 0- 0	0- 0- 0	95-98-1 00	90-95-1 00	70-80- 90	55-65- 75	25-30 -35	5-10-15
			4-49	Loam, sandy loam, silt loam	CL-ML, ML	A-4	0- 0- 0	0- 3- 5	95-98-1 00	90-95-1 00	70-80- 90	55-65- 75	20-25 -30	NP-5 -10
			49-74	Loam, fine sandy loam, gravelly sandy loam	CL-ML, ML, SC- SM, SM	A-2, A-4	0- 0- 0	0- 5- 10	65-83-1 00	55-78-1 00	45-65- 85	25-45- 65	20-25 -30	NP-5 -10



				Engineering Pro	operties–Br	oadwater C	ounty Are	a, Montar	a					
Map unit symbol and soil name	Pct. of	Hydrolo	Depth	USDA texture	Classi	fication	Pct Fra	igments	Percenta	age passi	ng sieve r	number—	Liquid limit	Plasticit y index
	map unit	gic group			Unified	AASHTO	>10 inches	3-10 inches	4	10	40	200		
			In				L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H
ChC—Chinook sandy loam, 4 to 9 percent slopes														
Chinook	95	A	0-8	Sandy loam	SM	A-2, A-4	0- 0- 0	0- 0- 0	80-90-1 00	75-88-1 00	55-65- 75	30-40- 50	15-20 -25	NP-3 -5
			8-14	Fine sandy loam, sandy loam	SM	A-2, A-4	0- 0- 0	0- 0- 0	80-90-1 00	75-88-1 00	55-70- 85	30-40- 50	15-20 -25	NP-3 -5
			14-34	Fine sandy loam, sandy loam	SM	A-2, A-4	0- 0- 0	0- 0- 0	80-90-1 00	75-88-1 00	55-70- 85	30-40- 50	15-20 -25	NP-3 -5
			34-60	Fine sandy loam, loamy fine sand, sandy loam	SM	A-2, A-4	0- 0- 0	0- 0- 0	80-90-1 00	75-88-1 00	60-70- 80	25-35- 45	15-20 -25	NP-3 -5



				Engineering Pro	operties–Br	oadwater Co	ounty Are	a, Montan	a					
Map unit symbol and	Pct. of	Hydrolo	Depth	USDA texture	Classi	fication	Pct Fra	agments	Percent	age passi	ng sieve i	number—		Plasticit y index
soil name	soil name map unit	gic group			Unified	AASHTO	>10 inches	3-10 inches	4	10	40	200		
			In				L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H
MwE—Musselshell- Crago channery loams, 15 to 35 percent slopes														
Musselshell	50	В	0-5	Channery loam	CL-ML, GC- GM, SC-SM	A-4	0- 0- 0	5-10- 15	65-75- 85	60-70- 80	45-55- 65	40-50- 60	25-28 -30	5-8 -10
			5-26	Loam, gravelly loam	CL-ML, GC- GM, SC-SM	A-4	0- 0- 0	0- 5- 10	60-80-1 00	55-78-1 00	50-65- 80	40-58- 75	25-28 -30	5-8 -10
			26-43	Gravelly loam, loam	CL-ML, GC- GM, GM, ML	A-4	0- 0- 0	0- 8- 15	65-83-1 00	60-80-1 00	45-63- 80	40-55- 70	15-20 -25	NP-5 -10



				Engineering Pro	operties–Br	oadwater Co	ounty Are	a, Montan	a					
Map unit symbol and	Pct. of	Hydrolo	Depth	USDA texture	USDA texture Classification		Pct Fragments		Percentage passing sieve number—				Liquid	Plasticit
soil name map unit	map unit	gic group			Unified	AASHTO	>10 inches	3-10 inches	4	10	40	200	limit	y index
			In				L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H
			43-60	Very gravelly sandy loam, very gravelly fine sandy loam, very gravelly loam	GC-GM, GM	A-1, A-2	0- 0- 0	10-13- 15	40-50- 60	30-43- 55	25-35- 45	10-20- 30	15-20 -25	NP-5 -10
Crago	40	В	0-4	Channery loam	CL-ML, GC- GM, GM, SC-SM	A-4	0- 0- 0	0- 4- 8	63-69- 76	45-59- 76	38-52- 72	27-38- 54	27-35 -43	9-14-18
			4-27	Gravelly loam, gravelly clay loam, very gravelly clay loam	GC, GC- GM	A-2, A-4, A-6	0- 0- 0	0- 6- 11	53-61- 72	29-48- 72	24-43- 71	18-33- 55	30-38 -45	13-19-2 5
			27-36	Extremely gravelly loam, very gravelly clay loam, extremely gravelly sandy loam	GC-GM, GM, GP-GM	A-1, A-2	0- 0- 0	0- 6- 10	44-51- 59	22-38- 59	16-30- 50	8-17- 29	27-38 -49	12-16-2 0
			36-60	Extremely gravelly loamy sand, extremely gravelly sandy loam, very gravelly sandy loam	GP, GP- GM, GM	A-1	0- 0- 0	0- 6- 10	49-57- 65	24-43- 65	17-35- 59	4-11- 23	0-27 -41	NP-6 -13



	Engineering Properties–Broadwater County Area, Montana													
Map unit symbol and	Pct. of	Hydrolo	Depth	USDA texture	Classi	fication	Pct Fra	gments	Percenta	age passi	ng sieve r	number—	Liquid	Plasticit
soil name	map unit	gic group			Unified	AASHTO	>10 inches	3-10 inches	4	10	40	200	limit	y index
			In				L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H
MxE—Musselshell- Crago cobbly loams, 8 to 20 percent slopes														
Musselshell	55	В	0-5	Cobbly loam	CL-ML	A-4	0- 0- 0	15-28- 40	85-90- 95	80-85- 90	60-70- 80	55-65- 75	25-28 -30	5-8 -10
			5-26	Loam, gravelly loam	CL-ML, GC- GM, SC-SM	A-4	0- 0- 0	0- 5- 10	60-80-1 00	55-78-1 00	50-65- 80	40-58- 75	25-28 -30	5-8 -10
			26-43	Gravelly loam, loam	CL-ML, GC- GM, GM, ML	A-4	0- 0- 0	0- 8- 15	65-83-1 00	60-80-1 00	45-63- 80	40-55- 70	15-20 -25	NP-5 -10



Engineering Properties–Broadwater County Area, Montana														
Map unit symbol and	Pct. of	Hydrolo	Depth	USDA texture	Classi	fication	Pct Fra	igments	Percent	age passi	ng sieve ı	number—	Liquid	Plastici
soil name	map unit	gic group			Unified	AASHTO	>10 inches	3-10 inches	4	10	40	200	limit	y index
			In				L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H	L-R-H
			43-60	Very gravelly sandy loam, very gravelly fine sandy loam, very gravelly loam	GC-GM, GM	A-1, A-2	0- 0- 0	10-13- 15	40-50- 60	30-43- 55	25-35- 45	10-20- 30	15-20 -25	NP-5 -10
Crago	30	В	0-4	Cobbly loam	CL-ML, ML	A-4	0- 0- 0	15-23- 30	75-80- 85	70-75- 80	60-65- 70	50-55- 60	20-25 -30	NP-5 -10
			4-27	Very stony loam, very cobbly clay loam, gravelly loam	CL, GC, GC- GM, SC-SM	A-2, A-4, A-6	0- 0- 0	10-28- 45	50-65- 80	45-60- 75	40-55- 70	30-45- 60	25-30 -35	5-10-15
			27-36	Very cobbly loam, extremely cobbly sandy loam, very gravelly clay loam	GC-GM, GM	A-1, A-2	0- 0- 0	25-40- 55	30-40- 50	25-35- 45	20-30- 40	15-25- 35	20-25 -30	NP-5 -10
			36-60	Very cobbly sandy loam, extremely cobbly loamy sand, very gravelly sandy loam	GM	A-1	0- 0- 0	25-40- 55	35-45- 55	25-35- 45	15-25- 35	10-18- 25	—	NP
Te—Thess silt loam														
Thess	80	В	0-5	Silt loam	CL, CL- ML	A-4, A-6	0- 0- 0	0- 0- 0	95-98-1 00	90-95-1 00	80-88- 95	60-70- 80	20-28 -35	5-10-15
			5-22	Loam, silt loam	CL, CL- ML	A-4, A-6	0- 0- 0	0- 3- 5	90-95-1 00	85-90- 95	80-88- 95	60-70- 80	20-28 -35	5-10-15
			22-60	Very gravelly sand, very gravelly loamy sand, extremely gravelly sand	GP, GP- GM	A-1	0- 0- 0	0- 8- 15	20-28- 35	15-23- 30	10-15- 20	0- 5- 10	—	NP



Data Source Information

Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 17, Sep 5, 2018



Physical Soil Properties

This table shows estimates of some physical characteristics and features that affect soil behavior. These estimates are given for the layers of each soil in the survey area. The estimates are based on field observations and on test data for these and similar soils.

Depth to the upper and lower boundaries of each layer is indicated.

Particle size is the effective diameter of a soil particle as measured by sedimentation, sieving, or micrometric methods. Particle sizes are expressed as classes with specific effective diameter class limits. The broad classes are sand, silt, and clay, ranging from the larger to the smaller.

Sand as a soil separate consists of mineral soil particles that are 0.05 millimeter to 2 millimeters in diameter. In this table, the estimated sand content of each soil layer is given as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter.

Silt as a soil separate consists of mineral soil particles that are 0.002 to 0.05 millimeter in diameter. In this table, the estimated silt content of each soil layer is given as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter.

Clay as a soil separate consists of mineral soil particles that are less than 0.002 millimeter in diameter. In this table, the estimated clay content of each soil layer is given as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter.

The content of sand, silt, and clay affects the physical behavior of a soil. Particle size is important for engineering and agronomic interpretations, for determination of soil hydrologic qualities, and for soil classification.

The amount and kind of clay affect the fertility and physical condition of the soil and the ability of the soil to adsorb cations and to retain moisture. They influence shrink-swell potential, saturated hydraulic conductivity (Ksat), plasticity, the ease of soil dispersion, and other soil properties. The amount and kind of clay in a soil also affect tillage and earthmoving operations.

Moist bulk density is the weight of soil (ovendry) per unit volume. Volume is measured when the soil is at field moisture capacity, that is, the moisture content at 1/3- or 1/10-bar (33kPa or 10kPa) moisture tension. Weight is determined after the soil is dried at 105 degrees C. In the table, the estimated moist bulk density of each soil horizon is expressed in grams per cubic centimeter of soil material that is less than 2 millimeters in diameter. Bulk density data are used to compute linear extensibility, shrink-swell potential, available water capacity, total pore space, and other soil properties. The moist bulk density of a soil indicates the pore space available for water and roots. Depending on soil texture, a bulk density of more than 1.4 can restrict water storage and root penetration. Moist bulk density is influenced by texture, kind of clay, content of organic matter, and soil structure.

Saturated hydraulic conductivity (Ksat) refers to the ease with which pores in a saturated soil transmit water. The estimates in the table are expressed in terms of micrometers per second. They are based on soil characteristics observed in the field, particularly structure, porosity, and texture. Saturated hydraulic conductivity (Ksat) is considered in the design of soil drainage systems and septic tank absorption fields.

Available water capacity refers to the quantity of water that the soil is capable of storing for use by plants. The capacity for water storage is given in inches of water per inch of soil for each soil layer. The capacity varies, depending on soil properties that affect retention of water. The most important properties are the content of organic matter, soil texture, bulk density, and soil structure. Available water capacity is an important factor in the choice of plants or crops to be grown and in the design and management of irrigation systems. Available water capacity is not an estimate of the quantity of water actually available to plants at any given time.

Linear extensibility refers to the change in length of an unconfined clod as moisture content is decreased from a moist to a dry state. It is an expression of the volume change between the water content of the clod at 1/3- or 1/10-bar tension (33kPa or 10kPa tension) and oven dryness. The volume change is reported in the table as percent change for the whole soil. The amount and type of clay minerals in the soil influence volume change.

Linear extensibility is used to determine the shrink-swell potential of soils. The shrink-swell potential is low if the soil has a linear extensibility of less than 3 percent; moderate if 3 to 6 percent; high if 6 to 9 percent; and very high if more than 9 percent. If the linear extensibility is more than 3, shrinking and swelling can cause damage to buildings, roads, and other structures and to plant roots. Special design commonly is needed.

Organic matter is the plant and animal residue in the soil at various stages of decomposition. In this table, the estimated content of organic matter is expressed as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter. The content of organic matter in a soil can be maintained by returning crop residue to the soil.

Organic matter has a positive effect on available water capacity, water infiltration, soil organism activity, and tilth. It is a source of nitrogen and other nutrients for crops and soil organisms.

Erosion factors are shown in the table as the K factor (Kw and Kf) and the T factor. Erosion factor K indicates the susceptibility of a soil to sheet and rill erosion by water. Factor K is one of six factors used in the Universal Soil Loss Equation (USLE) and the Revised Universal Soil Loss Equation (RUSLE) to predict the average annual rate of soil loss by sheet and rill erosion in tons per acre per year. The estimates are based primarily on percentage of silt, sand, and organic matter and on soil structure and Ksat. Values of K range from 0.02 to 0.69. Other factors being equal, the higher the value, the more susceptible the soil is to sheet and rill erosion by water.

Erosion factor Kw indicates the erodibility of the whole soil. The estimates are modified by the presence of rock fragments.

Erosion factor Kf indicates the erodibility of the fine-earth fraction, or the material less than 2 millimeters in size.

Erosion factor T is an estimate of the maximum average annual rate of soil erosion by wind and/or water that can occur without affecting crop productivity over a sustained period. The rate is in tons per acre per year.

Wind erodibility groups are made up of soils that have similar properties affecting their susceptibility to wind erosion in cultivated areas. The soils assigned to group 1 are the most susceptible to wind erosion, and those assigned to group 8 are the least susceptible. The groups are described in the "National Soil Survey Handbook."

Wind erodibility index is a numerical value indicating the susceptibility of soil to wind erosion, or the tons per acre per year that can be expected to be lost to wind erosion. There is a close correlation between wind erosion and the texture of the surface layer, the size and durability of surface clods, rock fragments, organic matter, and a calcareous reaction. Soil moisture and frozen soil layers also influence wind erosion.

Reference:

United States Department of Agriculture, Natural Resources Conservation Service. National soil survey handbook, title 430-VI. (http://soils.usda.gov)



Report—Physical Soil Properties

Three values are provided to identify the expected Low (L), Representative Value (R), and High (H).

	Physical Soil Properties-Broadwater County Area, Montana													
Map symbol and soil name	Depth	Sand	Silt	Clay	Moist bulk	Saturated hydraulic	Available water	Linear extensibility	Organic matter		Erosio factor		Wind erodibility	Wind erodibility
					density	conductivity	capacity			Kw	Kf	Т	group	index
	In	Pct	Pct	Pct	g/cc	micro m/sec	In/In	Pct	Pct					
AoB—Amesha loam, 1 to 4 percent slopes														
Amesha	0-4	-42-	-38-	15-20- 25	1.25-1.35 -1.45	4.00-9.00-14.00	0.16-0.18-0. 20	0.0- 1.5- 2.9	1.0- 2.0- 3.0	.28	.28	5	4L	86
	4-49	-45-	-41-	10-14- 18	1.30-1.43 -1.55	4.00-9.00-14.00	0.14-0.16-0. 17	0.0- 1.5- 2.9	0.5- 0.8- 1.0	.43	.43			
	49-74	-45-	-41-	10-14- 18	1.35-1.48 -1.60	4.00-9.00-14.00	0.12-0.14-0. 15	0.0- 1.5- 2.9	0.0- 0.3- 0.5	.43	.43			
AoC—Amesha loam, 4 to 9 percent slopes														
Amesha	0-4	-42-	-38-	15-20- 25	1.25-1.35 -1.45	4.00-9.00-14.00	0.16-0.18-0. 20	0.0- 1.5- 2.9	1.0- 2.0- 3.0	.28	.28	5	4L	86
	4-49	-45-	-41-	10-14- 18	1.30-1.43 -1.55	4.00-9.00-14.00	0.14-0.16-0. 17	0.0- 1.5- 2.9	0.5- 0.8- 1.0	.43	.43			
	49-74	-45-	-41-	10-14- 18	1.35-1.48 -1.60	4.00-9.00-14.00	0.12-0.14-0. 15	0.0- 1.5- 2.9	0.0- 0.3- 0.5	.43	.43			



	Physical Soil Properties–Broadwater County Area, Montana													
Map symbol and soil name	Depth	Sand	Silt	Clay	Moist bulk	Saturated hydraulic	Available water	Linear extensibility	Organic matter		Frosic factor		Wind erodibility	Wind erodibility
					density	conductivity	capacity			Kw	Kf	т	group	index
	In	Pct	Pct	Pct	g/cc	micro m/sec	In/In	Pct	Pct					
ChC—Chinook sandy loam, 4 to 9 percent slopes														
Chinook	0-8	-66-	-23-	5-12- 18	1.25-1.38 -1.50	14.00-28.00-42. 00	0.12-0.14-0. 15	0.0- 1.5- 2.9	1.0- 1.5- 2.0	.24	.24	5	3	86
	8-14	-66-	-23-	5-12- 18	1.40-1.50 -1.60	14.00-28.00-42. 00	0.12-0.14-0. 15	0.0- 1.5- 2.9	0.0- 0.5- 1.0	.28	.28			
	14-34	-66-	-23-	5-12- 18	1.40-1.50 -1.60	14.00-28.00-42. 00	0.12-0.14-0. 15	0.0- 1.5- 2.9	0.0- 0.5- 1.0	.28	.28			
	34-60	-67-	-23-	5-10- 15	1.40-1.50 -1.60	14.00-28.00-42. 00	0.11-0.12-0. 12	0.0- 1.5- 2.9	0.0- 0.5- 1.0	.28	.28			



				Pl	nysical Soil	Properties-Broa	adwater Coun	ty Area, Montana	ı					
Map symbol and soil name	Depth	Sand	Silt	Clay	Moist bulk	Saturated hydraulic	Available water	Linear extensibility	Organic matter	-	Erosio facto		Wind erodibility	Wind erodibility
					density	conductivity	capacity			Kw	Kf	т	group T	index
	In	Pct	Pct	Pct	g/cc	micro m/sec	In/In	Pct	Pct					
MwE— Musselshell- Crago channery loams, 15 to 35 percent slopes														
Musselshell	0-5	-39-	-37-	20-24- 27	1.15-1.25 -1.35	4.00-9.00-14.00	0.14-0.16-0. 18	0.0- 1.5- 2.9	1.0- 2.0- 3.0	.17	.32	2	5	56
	5-26	-43-	-39-	10-19- 27	1.40-1.50 -1.60	4.00-9.00-14.00	0.14-0.16-0. 18	0.0- 1.5- 2.9	0.5- 0.8- 1.0	.20	.37			
	26-43	-45-	-41-	10-14- 18	1.50-1.63 -1.75	4.00-9.00-14.00	0.14-0.16-0. 18	0.0- 1.5- 2.9	0.0- 0.3- 0.5	.24	.43			
	43-60	-67-	-19-	10-14- 18	1.50-1.63 -1.75	14.00-28.00-42. 00	0.06-0.08-0. 10	0.0- 1.5- 2.9	0.0- 0.3- 0.5	.05	.15			
Crago	0-4	-42-	-37-	15-21- 27	1.15-1.25 -1.35	4.00-9.00-14.00	0.10-0.11-0. 12	0.0- 1.5- 2.9	1.0- 2.0- 3.0	.17	.32	2	5	56
	4-27	-37-	-35-	20-28- 35	1.30-1.40 -1.50	4.00-9.00-14.00	0.07-0.08-0. 08	0.0- 1.5- 2.9	0.5- 0.8- 1.0	.10	.32			
	27-36	-62-	-14-	18-24- 30	1.30-1.43 -1.55	4.00-9.00-14.00	0.03-0.04-0. 04	0.0- 1.5- 2.9	0.0- 2.5- 5.0	.05	.17			
	36-60	-81-	- 9-	0-10- 20	1.45-1.58 -1.70	42.00-92.00-14 1.00	0.02-0.03-0. 03	0.0- 1.5- 2.9	0.0- 2.5- 5.0	.05	.10			



Map symbol and soil name	Depth	Sand	Silt	Clay	Moist bulk	Saturated hydraulic	Available water	Linear extensibility	Organic matter		rosic actor		Wind erodibility	Wind erodibility
					density	conductivity	capacity			Kw	Kf	т	group	index
	In	Pct	Pct	Pct	g/cc	micro m/sec	In/In	Pct	Pct					
MxE— Musselshell- Crago cobbly loams, 8 to 20 percent slopes														
Musselshell	0-5	-39-	-37-	20-24- 27	1.15-1.25 -1.35	4.00-9.00-14.00	0.14-0.16-0. 18	0.0- 1.5- 2.9	1.0- 2.0- 3.0	.17	.32	2	5	56
	5-26	-43-	-39-	10-19- 27	1.40-1.50 -1.60	4.00-9.00-14.00	0.14-0.16-0. 18	0.0- 1.5- 2.9	0.5- 0.8- 1.0	.20	.37			
	26-43	-45-	-41-	10-14- 18	1.50-1.63 -1.75	4.00-9.00-14.00	0.14-0.16-0. 18	0.0- 1.5- 2.9	0.0- 0.3- 0.5	.24	.43			
	43-60	-67-	-19-	10-14- 18	1.50-1.63 -1.75	14.00-28.00-42. 00	0.06-0.08-0. 10	0.0- 1.5- 2.9	0.0- 0.3- 0.5	.05	.15			
Crago	0-4	-42-	-37-	15-21- 27	1.30-1.40 -1.50	4.00-9.00-14.00	0.13-0.15-0. 16	0.0- 1.5- 2.9	1.0- 2.0- 3.0	.17	.32	2	5	56
	4-27	-37-	-37-	20-26- 35	1.40-1.50 -1.60	4.00-9.00-14.00	0.08-0.09-0. 10	0.0- 1.5- 2.9	0.0- 0.0- 1.0	.17	.32			
	27-36	-63-	-18-	15-19- 30	1.50-1.63 -1.75	4.00-9.00-14.00	0.04-0.05-0. 06	0.0- 1.5- 2.9	0.0- 0.3- 0.5	.05	.24			
	36-60	-84-	- 9-	0- 8- 15	1.50-1.60 -1.70	42.00-92.00-14 1.00	0.02-0.03-0. 04	0.0- 1.5- 2.9	0.0- 0.3- 0.5	.02	.15			
Te—Thess silt loam														
Thess	0-5	-26-	-52-	18-22- 25	1.10-1.20 -1.30	4.00-9.00-14.00	0.18-0.20-0. 22	0.0- 1.5- 2.9	1.0- 2.0- 3.0	.37	.37	3	4L	86
	5-22	-42-	-38-	15-20- 25	1.25-1.35 -1.45	4.00-9.00-14.00	0.16-0.18-0. 20	0.0- 1.5- 2.9	0.5- 0.8- 1.0	.37	.37			
	22-60	-96-	- 2-	0- 3- 5	1.50-1.60 -1.70	141.00-141.00- 141.00	0.02-0.03-0. 03	0.0- 1.5- 2.9	0.0- 0.3- 0.5	.02	.02			

Data Source Information

Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 17, Sep 5, 2018



Prime and other Important Farmlands

This table lists the map units in the survey area that are considered important farmlands. Important farmlands consist of prime farmland, unique farmland, and farmland of statewide or local importance. This list does not constitute a recommendation for a particular land use.

In an effort to identify the extent and location of important farmlands, the Natural Resources Conservation Service, in cooperation with other interested Federal, State, and local government organizations, has inventoried land that can be used for the production of the Nation's food supply.

Prime farmland is of major importance in meeting the Nation's short- and longrange needs for food and fiber. Because the supply of high-quality farmland is limited, the U.S. Department of Agriculture recognizes that responsible levels of government, as well as individuals, should encourage and facilitate the wise use of our Nation's prime farmland.

Prime farmland, as defined by the U.S. Department of Agriculture, is land that has the best combination of physical and chemical characteristics for producing food, feed, forage, fiber, and oilseed crops and is available for these uses. It could be cultivated land, pastureland, forestland, or other land, but it is not urban or built-up land or water areas. The soil quality, growing season, and moisture supply are those needed for the soil to economically produce sustained high yields of crops when proper management, including water management, and acceptable farming methods are applied. In general, prime farmland has an adequate and dependable supply of moisture from precipitation or irrigation, a favorable temperature and growing season, acceptable acidity or alkalinity, an acceptable salt and sodium content, and few or no rocks. The water supply is dependable and of adequate quality. Prime farmland is permeable to water and air. It is not excessively erodible or saturated with water for long periods, and it either is not frequently flooded during the growing season or is protected from flooding. Slope ranges mainly from 0 to 6 percent. More detailed information about the criteria for prime farmland is available at the local office of the Natural Resources Conservation Service.

For some of the soils identified in the table as prime farmland, measures that overcome a hazard or limitation, such as flooding, wetness, and droughtiness, are needed. Onsite evaluation is needed to determine whether or not the hazard or limitation has been overcome by corrective measures.

A recent trend in land use in some areas has been the loss of some prime farmland to industrial and urban uses. The loss of prime farmland to other uses puts pressure on marginal lands, which generally are more erodible, droughty, and less productive and cannot be easily cultivated.



Unique farmland is land other than prime farmland that is used for the production of specific high-value food and fiber crops, such as citrus, tree nuts, olives, cranberries, and other fruits and vegetables. It has the special combination of soil quality, growing season, moisture supply, temperature, humidity, air drainage, elevation, and aspect needed for the soil to economically produce sustainable high yields of these crops when properly managed. The water supply is dependable and of adequate quality. Nearness to markets is an additional consideration. Unique farmland is not based on national criteria. It commonly is in areas where there is a special microclimate, such as the wine country in California.

In some areas, land that does not meet the criteria for prime or unique farmland is considered to be *farmland of statewide importance* for the production of food, feed, fiber, forage, and oilseed crops. The criteria for defining and delineating farmland of statewide importance are determined by the appropriate State agencies. Generally, this land includes areas of soils that nearly meet the requirements for prime farmland and that economically produce high yields of crops when treated and managed according to acceptable farming methods. Some areas may produce as high a yield as prime farmland if conditions are favorable. Farmland of statewide importance may include tracts of land that have been designated for agriculture by State law.

In some areas that are not identified as having national or statewide importance, land is considered to be *farmland of local importance* for the production of food, feed, fiber, forage, and oilseed crops. This farmland is identified by the appropriate local agencies. Farmland of local importance may include tracts of land that have been designated for agriculture by local ordinance.

	Prime and other Important Farmlands–Broadwater	County Area, Montana
Map Symbol	Map Unit Name	Farmland Classification
AoB	Amesha loam, 1 to 4 percent slopes	Prime farmland if irrigated
AoC	Amesha loam, 4 to 9 percent slopes	Farmland of statewide importance
ChC	Chinook sandy loam, 4 to 9 percent slopes	Prime farmland if irrigated
MwE	Musselshell-Crago channery loams, 15 to 35 percent slopes	Not prime farmland
MxE	Musselshell-Crago cobbly loams, 8 to 20 percent slopes	Not prime farmland
Те	Thess silt loam	Prime farmland if irrigated

Report—Prime and other Important Farmlands

Data Source Information

Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 18, Sep 16, 2019

Water Features

This table gives estimates of various soil water features. The estimates are used in land use planning that involves engineering considerations.

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The four hydrologic soil groups are:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas.

Surface runoff refers to the loss of water from an area by flow over the land surface. Surface runoff classes are based on slope, climate, and vegetative cover. The concept indicates relative runoff for very specific conditions. It is assumed that the surface of the soil is bare and that the retention of surface water resulting from irregularities in the ground surface is minimal. The classes are negligible, very low, low, medium, high, and very high.

The *months* in the table indicate the portion of the year in which a water table, ponding, and/or flooding is most likely to be a concern.

Water table refers to a saturated zone in the soil. The water features table indicates, by month, depth to the top (*upper limit*) and base (*lower limit*) of the saturated zone in most years. Estimates of the upper and lower limits are based mainly on observations of the water table at selected sites and on evidence of a saturated zone, namely grayish colors or mottles (redoximorphic features) in the soil. A saturated zone that lasts for less than a month is not considered a water table. The kind of water table, apparent or perched, is given if a seasonal high water table exists in the soil. A water table is perched if free water is restricted from moving downward in the soil by a restrictive feature, in most cases a hardpan; there is a dry layer of soil underneath a wet layer. A water table is apparent if free water is present in all horizons from its upper boundary to below 2 meters or to the depth of observation. The water table kind listed is for the first major component in the map unit.

Ponding is standing water in a closed depression. Unless a drainage system is installed, the water is removed only by percolation, transpiration, or evaporation. The table indicates *surface water depth* and the *duration* and *frequency* of ponding. Duration is expressed as *very brief* if less than 2 days, *brief* if 2 to 7 days, *long* if 7 to 30 days, and *very long* if more than 30 days. Frequency is expressed as none, rare, occasional, and frequent. *None* means that ponding is not probable; *rare* that it is unlikely but possible under unusual weather conditions (the chance of ponding is nearly 0 percent to 5 percent in any year); *occasional* that it occurs, on the average, once or less in 2 years (the chance of ponding is 5 to 50 percent in any year); and *frequent* that it occurs, on the average, more than once in 2 years (the chance of ponding is more than 50 percent in any year).

Flooding is the temporary inundation of an area caused by overflowing streams, by runoff from adjacent slopes, or by tides. Water standing for short periods after rainfall or snowmelt is not considered flooding, and water standing in swamps and marshes is considered ponding rather than flooding.

Duration and *frequency* are estimated. Duration is expressed as *extremely brief* if 0.1 hour to 4 hours, *very brief* if 4 hours to 2 days, *brief* if 2 to 7 days, *long* if 7 to 30 days, and *very long* if more than 30 days. Frequency is expressed as none, very rare, rare, occasional, frequent, and very frequent. *None* means that flooding is not probable; *very rare* that it is very unlikely but possible under extremely unusual weather conditions (the chance of flooding is less than 1 percent in any year); *rare* that it is unlikely but possible under unusual weather conditions (the chance of flooding is 5 to 50 percent in any year); *frequent* that it is likely to occur often under normal weather conditions (the chance of flooding is 5 to 50 percent in any year); *frequent* that it is likely to occur often under normal weather conditions (the chance of flooding is more than 50 percent in any year); *and very frequent* that it is likely to occur very often under normal weather conditions (the chance of flooding is more than 50 percent in any year); *and very frequent* that it is likely to occur very often under normal weather conditions (the chance of flooding is more than 50 percent in any year); *and very frequent* that it is likely to occur very often under normal weather conditions (the chance of flooding is any year); *and very frequent* that it is likely to occur very often under normal weather conditions (the chance of flooding is more than 50 percent in all months of any year).

The information is based on evidence in the soil profile, namely thin strata of gravel, sand, silt, or clay deposited by floodwater; irregular decrease in organic matter content with increasing depth; and little or no horizon development.

Also considered are local information about the extent and levels of flooding and the relation of each soil on the landscape to historic floods. Information on the extent of flooding based on soil data is less specific than that provided by detailed engineering surveys that delineate flood-prone areas at specific flood frequency levels.



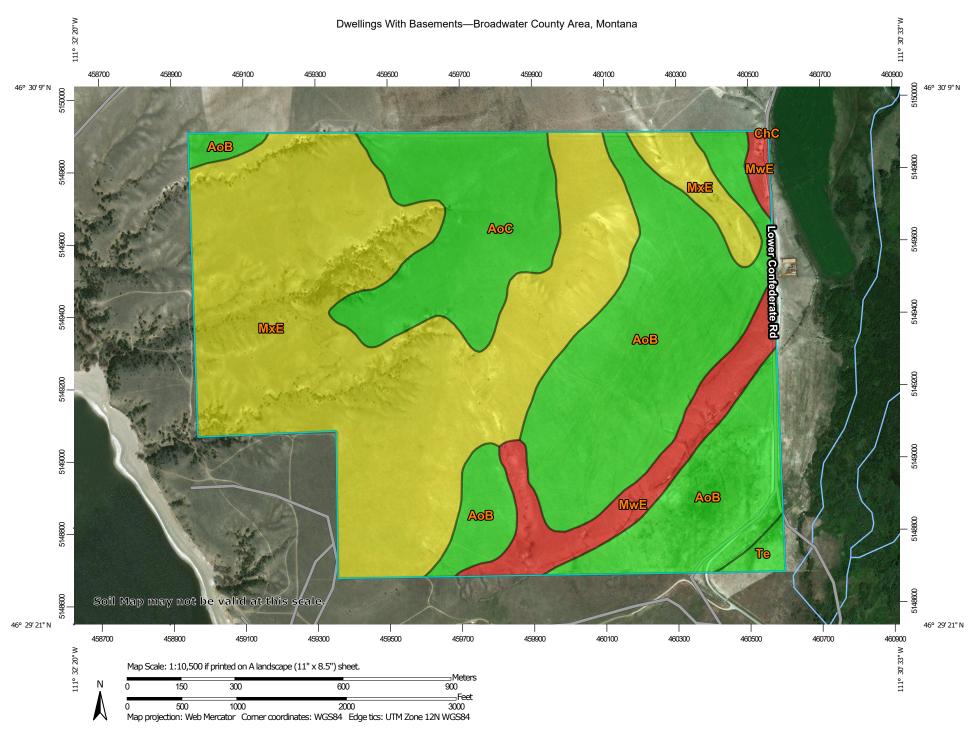
Report—Water Features

	-	-	-								
Map unit symbol and soil name	Hydrologic	Surface runoff	Most likely months		Water table			Ponding		Floo	ding
son name	group	runon	montais	Upper limit	Lower limit	Kind	Surface depth	Duration	Frequency	Duration	Frequency
				Ft	Ft		Ft				
AoB—Amesha loam, 1 to 4	percent slope	s									
Amesha	В		Jan-Dec	_	—	—	—	_	None	—	None
AoC—Amesha loam, 4 to 9	percent slope	S		•						•	•
Amesha	В		Jan-Dec	_	—	—	_	_	None	_	None
ChC—Chinook sandy loam	, 4 to 9 percen	it slopes		•						•	
Chinook	A		Jan-Dec	_	_	_	—	_	None	—	None
MwE—Musselshell-Crago	channery loam	s, 15 to 35 pe	rcent slopes								
Musselshell	В		Jan-Dec	_	—	—	—	-	None	—	None
Crago	В		Jan-Dec	_	—	—	—	_	None	_	None
MxE—Musselshell-Crago c	obbly loams, 8	to 20 percen	t slopes	•		·				•	
Musselshell	В		Jan-Dec	_	_	—	_	_	None	_	None
Crago	В		Jan-Dec	—	—	_	—	-	None	—	None
Te—Thess silt loam											
Thess	В		Jan-Dec	_	_	_		_	None	_	None

Data Source Information

Soil Survey Area: Broadwater County Area, Montana Survey Area Data: Version 17, Sep 5, 2018

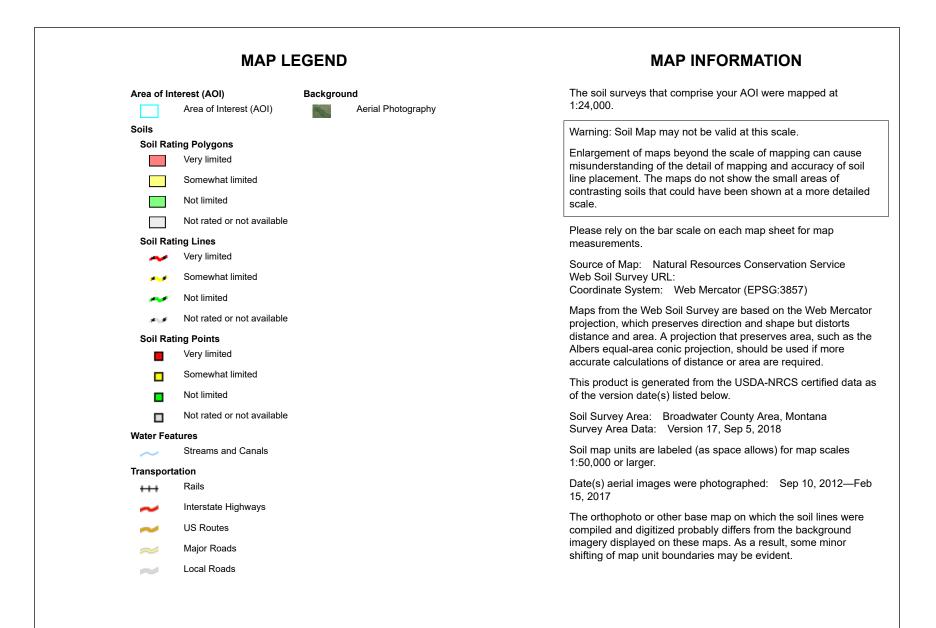




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Dwellings With Basements

Map unit symbol	Map unit name	Rating	Component name (percent)	Rating reasons (numeric values)	Acres in AOI	Percent of AOI
АоВ	Amesha loam, 1	Not limited	Amesha (90%)		146.3	32.3%
	to 4 percent slopes		Mussel (5%)			
			Musselshell (3%)			
			Amesha (2%)			
AoC	Amesha loam, 4	Not limited	Amesha (60%)		58.4	12.9%
	to 9 percent slopes		Amesha (15%)			
			Chinook (15%)			
			Crago (10%)			
ChC	Chinook sandy	Not limited	Chinook (95%)		0.0	0.0%
	loam, 4 to 9 percent slopes		Amesha (5%)			
MwE	Musselshell- Crago	Very limited	Musselshell (50%)	Slope (1.00)	31.7	7.0%
	channery loams, 15 to		Crago (40%)	Slope (1.00)		
	35 percent slopes		Cabbart (3%)	Depth to soft bedrock (1.00)		
				Slope (1.00)		
				Shrink-swell (0.50)		
MxE	Musselshell- Crago cobbly	Somewhat limited	Musselshell (55%)	Slope (0.96)	213.5	47.1%
	loams, 8 to 20 percent slopes		Crago (30%)	Slope (0.96)		
				Large stones (0.12)		
Те	Thess silt loam	Not limited	Thess (80%)		3.4	0.8%
			Amesha (5%)			
			Scravo (5%)			
Totals for Area	of Interest				453.4	100.0%

Rating	Acres in AOI	Percent of AOI
Somewhat limited	213.5	47.1%
Not limited	208.2	45.9%
Very limited	31.7	7.0%
Totals for Area of Interest	453.4	100.0%

USDA

Description

Dwellings are single-family houses of three stories or less. For dwellings with basements, the foundation is assumed to consist of spread footings of reinforced concrete built on undisturbed soil at a depth of about 7 feet.

The ratings for dwellings are based on the soil properties that affect the capacity of the soil to support a load without movement and on the properties that affect excavation and construction costs. The properties that affect the load-supporting capacity include depth to a water table, ponding, flooding, subsidence, linear extensibility (shrink-swell potential), and compressibility. Compressibility is inferred from the Unified classification of the soil. The properties that affect the ease and amount of excavation include depth to a water table, ponding, flooding, slope, depth to bedrock or a cemented pan, hardness of bedrock or a cemented pan, and the amount and size of rock fragments.

The ratings are both verbal and numerical. Rating class terms indicate the extent to which the soils are limited by all of the soil features that affect the specified use. "Not limited" indicates that the soil has features that are very favorable for the specified use. Good performance and very low maintenance can be expected. "Somewhat limited" indicates that the soil has features that are moderately favorable for the specified use. The limitations can be overcome or minimized by special planning, design, or installation. Fair performance and moderate maintenance can be expected. "Very limited" indicates that the soil has one or more features that are unfavorable for the specified use. The limitations generally cannot be overcome without major soil reclamation, special design, or expensive installation procedures. Poor performance and high maintenance can be expected.

Numerical ratings indicate the severity of individual limitations. The ratings are shown as decimal fractions ranging from 0.01 to 1.00. They indicate gradations between the point at which a soil feature has the greatest negative impact on the use (1.00) and the point at which the soil feature is not a limitation (0.00).

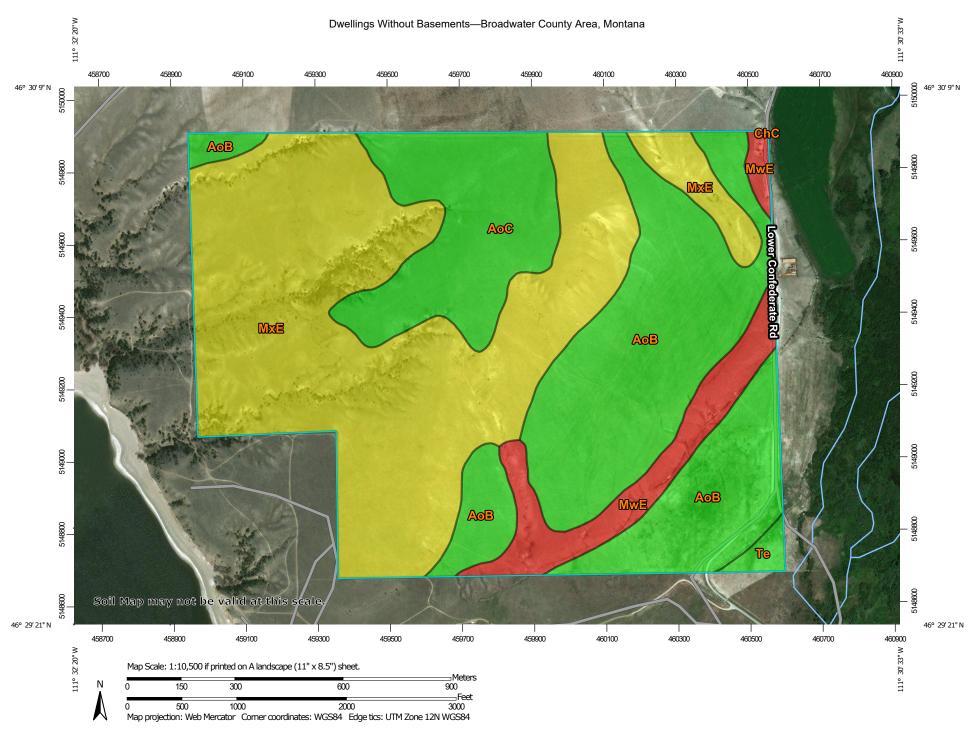
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Other components with different ratings may be present in each map unit. The ratings for all components, regardless of the map unit aggregated rating, can be viewed by generating the equivalent report from the Soil Reports tab in Web Soil Survey or from the Soil Data Mart site. Onsite investigation may be needed to validate these interpretations and to confirm the identity of the soil on a given site.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher





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MAF	P LEGEND	MAP INFORMATION
Area of Interest (AOI) Area of Interest (AOI)	Background Aerial Photography	The soil surveys that comprise your AOI were mapped at 1:24,000.
Soils	, on all motography	Maminu Onil Man merupat ka valid at this anala
Soil Rating Polygons		Warning: Soil Map may not be valid at this scale.
Very limited		Enlargement of maps beyond the scale of mapping can cau misunderstanding of the detail of mapping and accuracy of
Somewhat limited		line placement. The maps do not show the small areas of
Not limited		contrasting soils that could have been shown at a more det scale.
Not rated or not availa	able	Please rely on the bar scale on each map sheet for map
Soil Rating Lines		measurements.
Nery limited		Source of Map: Natural Resources Conservation Service
somewhat limited		Web Soil Survey URL:
Mot limited		Coordinate System: Web Mercator (EPSG:3857)
Not rated or not availa	able	Maps from the Web Soil Survey are based on the Web Mer projection, which preserves direction and shape but distorts
Soil Rating Points		distance and area. A projection that preserves area, such a
Very limited		Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.
Somewhat limited		
Not limited		This product is generated from the USDA-NRCS certified d of the version date(s) listed below.
Not rated or not available	able	Soil Survey Area: Broadwater County Area, Montana
Water Features		Survey Area Data: Version 17, Sep 5, 2018
Streams and Canals		Soil map units are labeled (as space allows) for map scales
Transportation		1:50,000 or larger.
+++ Rails		Date(s) aerial images were photographed: Sep 10, 2012-
nterstate Highways		15, 2017
JS Routes		The orthophoto or other base map on which the soil lines w compiled and digitized probably differs from the background
Major Roads		imagery displayed on these maps. As a result, some minor
Local Roads		shifting of map unit boundaries may be evident.



Dwellings Without Basements

Map unit symbol	Map unit name	Rating	Component name (percent)	Rating reasons (numeric values)	Acres in AOI	Percent of AOI
AoB	Amesha loam, 1	Not limited	Amesha (90%)		146.3	32.3%
	to 4 percent slopes		Mussel (5%)			
			Musselshell (3%)			
			Amesha (2%)			
AoC	Amesha loam, 4	Not limited	Amesha (60%)		58.4	12.9%
	to 9 percent slopes		Amesha (15%)			
			Chinook (15%)			
			Crago (10%)			
ChC	Chinook sandy	Not limited	Chinook (95%)		0.0	0.0%
	loam, 4 to 9 percent slopes		Amesha (5%)			
MwE	Musselshell- Crago	Very limited	Musselshell (50%)	Slope (1.00)	31.7	7.0%
	channery loams, 15 to		Crago (40%)	Slope (1.00)		
	35 percent slopes		Cabbart (3%)	Slope (1.00)		
	siopes			Depth to soft bedrock (0.50)		
				Shrink-swell (0.50)		
MxE	Musselshell- Crago cobbly	Somewhat limited	Musselshell (55%)	Slope (0.96)	213.5	47.1%
	loams, 8 to 20 percent slopes		Crago (30%)	Slope (0.96)		
				Large stones (0.12)		
Те	Thess silt loam	Not limited	Thess (80%)		3.4	0.8%
			Amesha (5%)			
			Scravo (5%)			
Totals for Area	of Interest				453.4	100.0%

Rating	Acres in AOI Percent of AOI	
Somewhat limited	213.5	47.1%
Not limited	208.2	45.9%
Very limited	31.7	7.0%
Totals for Area of Interest	453.4	100.0%

USDA

Description

Dwellings are single-family houses of three stories or less. For dwellings without basements, the foundation is assumed to consist of spread footings of reinforced concrete built on undisturbed soil at a depth of 2 feet or at the depth of maximum frost penetration, whichever is deeper.

The ratings for dwellings are based on the soil properties that affect the capacity of the soil to support a load without movement and on the properties that affect excavation and construction costs. The properties that affect the load-supporting capacity include depth to a water table, ponding, flooding, subsidence, linear extensibility (shrink-swell potential), and compressibility. Compressibility is inferred from the Unified classification of the soil. The properties that affect the ease and amount of excavation include depth to a water table, ponding, flooding, slope, depth to bedrock or a cemented pan, hardness of bedrock or a cemented pan, and the amount and size of rock fragments.

The ratings are both verbal and numerical. Rating class terms indicate the extent to which the soils are limited by all of the soil features that affect the specified use. "Not limited" indicates that the soil has features that are very favorable for the specified use. Good performance and very low maintenance can be expected. "Somewhat limited" indicates that the soil has features that are moderately favorable for the specified use. The limitations can be overcome or minimized by special planning, design, or installation. Fair performance and moderate maintenance can be expected. "Very limited" indicates that the soil has one or more features that are unfavorable for the specified use. The limitations generally cannot be overcome without major soil reclamation, special design, or expensive installation procedures. Poor performance and high maintenance can be expected.

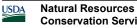
Numerical ratings indicate the severity of individual limitations. The ratings are shown as decimal fractions ranging from 0.01 to 1.00. They indicate gradations between the point at which a soil feature has the greatest negative impact on the use (1.00) and the point at which the soil feature is not a limitation (0.00).

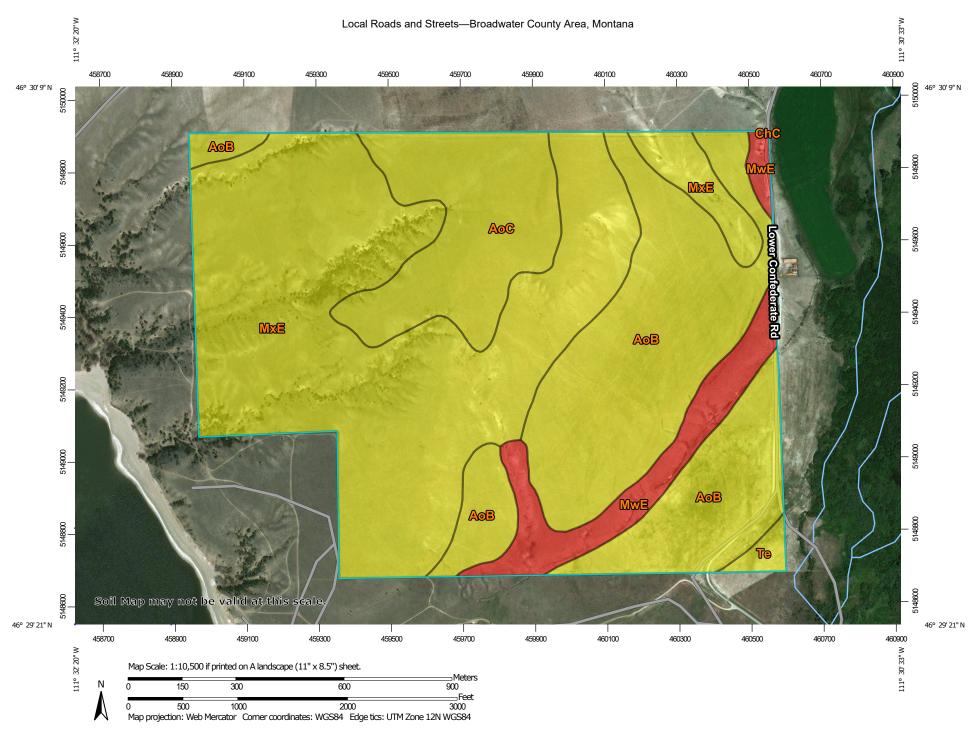
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Other components with different ratings may be present in each map unit. The ratings for all components, regardless of the map unit aggregated rating, can be viewed by generating the equivalent report from the Soil Reports tab in Web Soil Survey or from the Soil Data Mart site. Onsite investigation may be needed to validate these interpretations and to confirm the identity of the soil on a given site.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

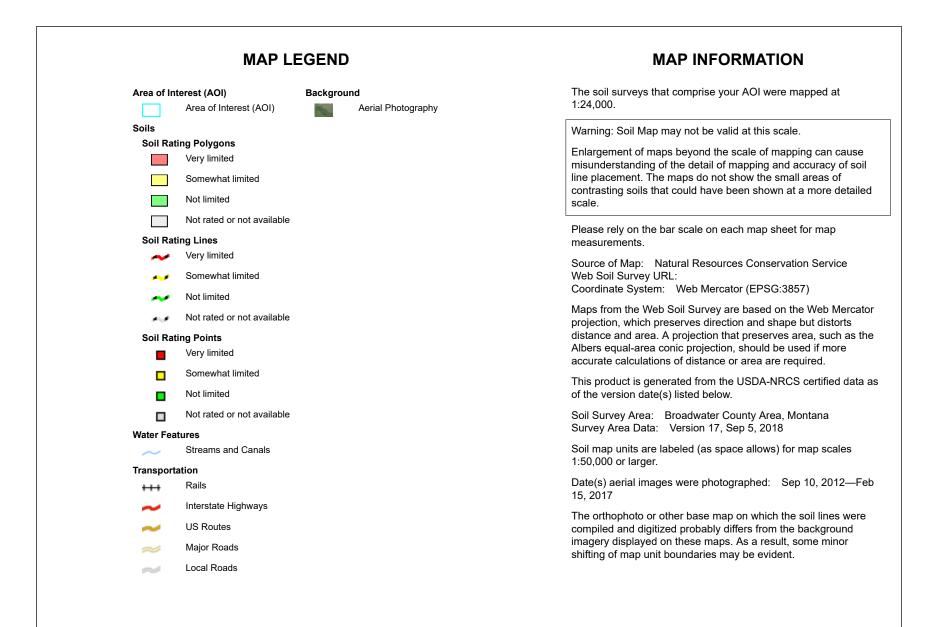




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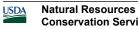


Local Roads and Streets

Map unit symbol	Map unit name	Rating	Component name (percent)	Rating reasons (numeric values)	Acres in AOI	Percent of AOI
AoB Amesha loam, 1 to 4 percent slopes	percent limited	Amesha (90%)	Frost action (0.50)	146.3	32.3%	
	slopes		Mussel (5%)	Frost action (0.50)		
		Musselshell (3%)	Frost action (0.50)			
		Amesha (2%)	Frost action (0.50)			
AoC	Amesha loam, 4 to 9 percent	esha loam, 4 9 percent opes	Amesha (60%)	Frost action (0.50)	58.4	12.9%
	siopes		Amesha (15%)	Frost action (0.50)		
			Chinook (15%)	Frost action (0.50)		
			Crago (10%)	Frost action (0.50)		
ChC	loam, 4 to 9 limited	Chinook (95%)	Frost action (0.50)	0.0	0.0%	
percent slopes		Amesha (5%)	Frost action (0.50)			
MwE	Musselshell-	Crago (50%) channery loams, 15 to 35 percent Slopes Crago (40%)		Slope (1.00)	31.7	7.0%
channery			Frost action (0.50)			
				Slope (1.00)		
				Frost action (0.50)		
			Cabbart (3%)	Depth to soft bedrock (1.00)		
			Slope (1.00)			
		Frost action (0.50)				
				Shrink-swell (0.50)		
loams, 8 to		Ausselshell- Crago cobbly loams, 8 to 20 percent slopes		Slope (0.96)	213.5	47.1%
	loams, 8 to 20		20	Frost action (0.50)		
		Crago (30%)	Slope (0.96)		1	
				Frost action (0.50)		

Map unit symbol	Map unit name	Rating	Component name (percent)	Rating reasons (numeric values)	Acres in AOI	Percent of AOI
				Large stones (0.12)		
			Thess (5%)	Frost action (0.50)		
			Thess (5%)	Frost action (0.50)		
			Sappington (5%)	Frost action (0.50)		
Те	Thess silt loam	Somewhat limited	Thess (80%)	Frost action (0.50)	3.4	0.8%
			Amesha (5%)	Frost action (0.50)		
Totals for Area of Interest					453.4	100.0%

Rating	Acres in AOI	Percent of AOI
Somewhat limited	421.8	93.0%
Very limited	31.7	7.0%
Totals for Area of Interest	453.4	100.0%



Description

Local roads and streets have an all-weather surface and carry automobile and light truck traffic all year. They have a subgrade of cut or fill soil material; a base of gravel, crushed rock, or soil material stabilized by lime or cement; and a surface of flexible material (asphalt), rigid material (concrete), or gravel with a binder. The ratings are based on the soil properties that affect the ease of excavation and grading and the traffic-supporting capacity. The properties that affect the ease of excavation and grading are depth to bedrock or a cemented pan, hardness of bedrock or a cemented pan, depth to a water table, ponding, flooding, the amount of large stones, and slope. The properties that affect the traffic-supporting capacity are soil strength (as inferred from the AASHTO group index number), subsidence, linear extensibility (shrink-swell potential), the potential for frost action, depth to a water table, and ponding.

The ratings are both verbal and numerical. Rating class terms indicate the extent to which the soils are limited by all of the soil features that affect the specified use. "Not limited" indicates that the soil has features that are very favorable for the specified use. Good performance and very low maintenance can be expected. "Somewhat limited" indicates that the soil has features that are moderately favorable for the specified use. The limitations can be overcome or minimized by special planning, design, or installation. Fair performance and moderate maintenance can be expected. "Very limited" indicates that the soil has one or more features that are unfavorable for the specified use. The limitations generally cannot be overcome without major soil reclamation, special design, or expensive installation procedures. Poor performance and high maintenance can be expected.

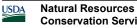
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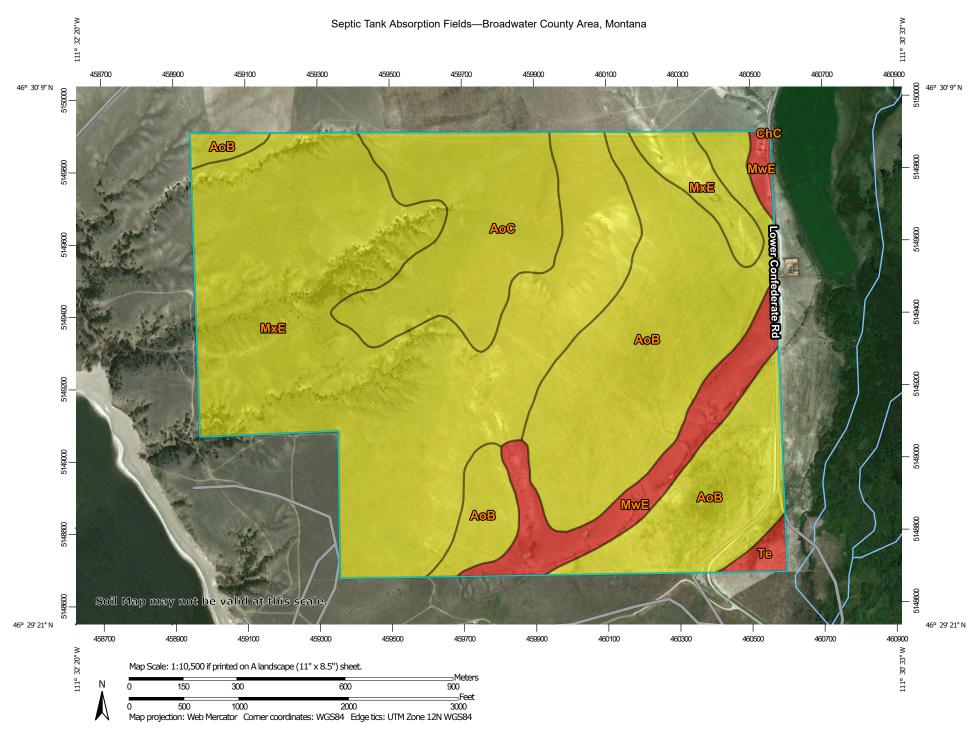
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Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

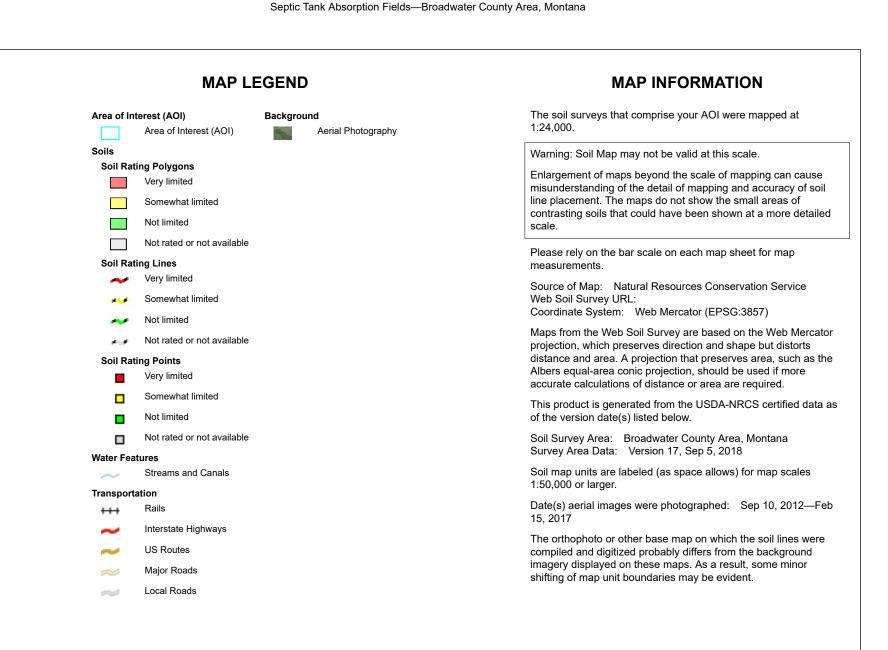




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Septic Tank Absorption Fields

Map unit symbol	Map unit name	Rating	Component name (percent)	Rating reasons (numeric values)	Acres in AOI	Percent of AOI
AoB Amesha loam, 1 to 4 percent slopes	to 4 percent limited	Amesha (90%)	Slow water movement (0.50)	146.3	32.3%	
			Mussel (5%)	Slow water movement (0.50)		
	Ν	Musselshell (3%)	Slow water movement (0.50)			
		Amesha (2%)	Amesha (2%)	Slow water movement (0.50)		
AoC	Amesha loam, 4 to 9 percent slopes	Somewhat limited	Amesha (60%)	Slow water movement (0.50)	58.4	12.9%
		Amesha (15%)	Slow water movement (0.50)			
		Crago (10%)	Slow water movement (0.50)			
ChC	Chinook sandy loam, 4 to 9 percent slopes	Not limited	Chinook (95%)		0.0	0.0%
MwE	Musselshell-	Ausselshell- Crago channery loams, 15 to 35 percent slopes	Musselshell (50%)	Slope (1.00)	31.7	7.0%
channery loams, 15 to	channery loams, 15 to			Slow water movement (0.50)		
			Crago (40%)	Slope (1.00)		
	Cabbart (3		Slow water movement (0.50)			
		Cabbart (3%)	Depth to bedrock (1.00)			
			Slope (1.00)			
		20	limited (55%)	Slope (0.96)	213.5	47.1%
	loams, 8 to 20 percent slopes			Slow water movement (0.50)		
			Crago (30%)	Slope (0.96)		
			Slow water movement (0.50)			

Map unit symbol	Map unit name	Rating	Component name (percent)	Rating reasons (numeric values)	Acres in AOI	Percent of AOI
				Large stones (0.12)		
			Thess (5%)	Slow water movement (0.50)		
			Thess (5%)	Slow water movement (0.50)		
			Sappington (5%)	Slow water movement (0.50)		
Те	Thess silt loam	Very limited	Thess (80%)	Filtering capacity (1.00)	3.4	0.8%
			Scravo (5%)	Filtering capacity (1.00)		
			Lothair (5%)	Slow water movement (1.00)		
				Slope (0.16)		
Totals for Area	of Interest		453.4	100.0%		

Rating	Acres in AOI	Percent of AOI
Somewhat limited	418.3	92.2%
Very limited	35.1	7.7%
Not limited	0.0	0.0%
Totals for Area of Interest	453.4	100.0%

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Description

Septic tank absorption fields are areas in which effluent from a septic tank is distributed into the soil through subsurface tiles or perforated pipe. Only that part of the soil between depths of 24 and 60 inches is evaluated. The ratings are based on the soil properties that affect absorption of the effluent, construction and maintenance of the system, and public health. Saturated hydraulic conductivity (Ksat), depth to a water table, ponding, depth to bedrock or a cemented pan, and flooding affect absorption of the effluent. Stones and boulders, ice, and bedrock or a cemented pan interfere with installation. Subsidence interferes with installation and maintenance. Excessive slope may cause lateral seepage and surfacing of the effluent in downslope areas.

Some soils are underlain by loose sand and gravel or fractured bedrock at a depth of less than 4 feet below the distribution lines. In these soils the absorption field may not adequately filter the effluent, particularly when the system is new. As a result, the ground water may become contaminated.

The ratings are both verbal and numerical. Rating class terms indicate the extent to which the soils are limited by all of the soil features that affect the specified use. "Not limited" indicates that the soil has features that are very favorable for the specified use. Good performance and very low maintenance can be expected. "Somewhat limited" indicates that the soil has features that are moderately favorable for the specified use. The limitations can be overcome or minimized by special planning, design, or installation. Fair performance and moderate maintenance can be expected. "Very limited" indicates that the soil has one or more features that are unfavorable for the specified use. The limitations generally cannot be overcome without major soil reclamation, special design, or expensive installation procedures. Poor performance and high maintenance can be expected.

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Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher





												Olverse project
Client: 71	Ranch						Location:	Test P	it 1			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 2%				
Date: 2/1	10/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed I	By:	MF										
	-			S	tructu	re		Bou				
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments
0" - 2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	m∨fr	G	I	1	f	Brown topsoil, moist with fine roots
2" - 36"	2.5YR 6/3	None	Silty Loam	1	sbk	f	m∨fr	G	W	1	vf	Light tan silt and sand with gravel up to 2" dia. Moist.
36" - 144"	2.5YR 6/2						mvfr	G	w	1	vf	Pitrun gravel w/ fines and cobbles up to 15" dia. Dry. Some orange type mottling - unclear if it was groundwater mottling
	End at 156". No G	Groundwater	r, bedrock, or lin	niting	layer er	ncoun	tered.	1	•		•	



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Client: 71	Ranch						Location:	Test Pi	t 2			
Project #:	19-072 71 Ranch -	- Major Sub	division				Slope:	± 2%				
Date: 2/1	10/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed I	•	MF										
	- j .			S	tructu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	T	Q	S	Comments
0" - 2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
2" - 45"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan silt and sand with gravel up to 2" dia. Moist.
45" - 144"	2.5YR 6/2	None	Sand/Gravel	1	sbk	f	mvfr	G	w	1	vf	Pitrun gravel w/ fines and cobbles up to 15" dia. Dry. Some orange type mottling - unclear if it was groundwater mottling
	End at 156". No G	niting	layer ei	ncoun	tered.		I		I			



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Client: 71	Ranch						Location:	Test P	t 3			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 2%				
Date: 2/1	10/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed I	-	MF							<u> </u>			
				s	tructu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
3" - 48"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan silt and sand with gravel up to 2" dia. Moist.
48" - 144"	2.5YR 6/2						mvfr	G	w	1	vf	Pitrun gravel w/ fines and cobbles up to 15" dia. Dry. Some orange type mottling - unclear if it was groundwater mottling
	End at 156". No G	iroundwate	r, bedrock, or lin	niting	l layer ei	ncoun	tered.	1	I	1		



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Client: 71	Ranch						Location:	Test Pi	t 4			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 3%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed I	By:	MF										
				s	tructu	re		Bou	ndary	R	oots	
Depth (in.)						S	Consistence	D	T	Q	S	Comments
0" -2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	2	f	Brown topsoil, moist with fine roots
2" - 12"	2.5YR 6/2	None	Silty Sand	1	sbk	f	mvfr	G	W	1	vf	Brown sandy silt with fine roots, dry.
12" - 32"	2.5YR 5/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt, with fewer fine roots, dry.
32" - 60"	2.5YR 4/2	None	Silty Loam with gravel	1	sbk	f	mvfr	G	W	1	vf	Tan silty sandy loam with gravel up to 4"
60" - 144"	Silty Sond with							G	W	1	vf	Very cobbly gravely sandy silt 30% fines. Dry
	End at 144". No G	niting I	layer ei	ncoun	tered.	•		•	•			



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Client: 71	Ranch						Location:	Test P	t 5			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	±4%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed I	-	MF							<u> </u>			
	-) -			S	tructu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	T	Q	S	Comments
0" -4"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	2	f	Brown topsoil, moist with fine roots
4" - 72"	2.5YR 4/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt w/ gravel up to 4". Roots and dry.
72" - 144"	2.5YR 3/2	None	Silt Loam	1	gr	m	mvfr	G	W	1	vf	Same material but with larger cobble up to 12". Dry
	End at 144". No G trenches.	Froundwate	r, bedrock, or lin	niting	layer e	ncoun	itered. Over 6' o	f Silt loa	m belov	v propo	sed	



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Client: 71	Ranch						Location:	Test P	it 6			
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	± 4%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	-	MF							•			
	-			S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	T	Q	S	Comments
0" -2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	2	f	Brown topsoil, moist with fine roots
2" - 144"	2.5YR 4/4	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt w/ gravel up to 4". Roots for first 2' and dry.
	End at 144". No C trenches.	niting	layer ei	ncour	itered. Over 6' of	f Silt Lo	am belo	w propo	osed			



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Client: 71	Ranch						Location:	Test P	t 7			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 3%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed		MF										
	-			S	Structu	re		Boundary Roots				
Depth (in.)	Color					S	Consistence	D	T	Q	S	Comments
0" -2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
2" - 144"	2.5YR 5/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan and sandy silt with roots down to 2' BGS. Dry
144" - 156"	2.5YR 6/4	None	Silty Fine Sand	1	sbk	f	mvfr	G	w	1	vf	Light tan and sandy silt w/ cobbles. Dry
		1										
	End at 156". No G proposed trenches		r, bedrock, or lin	niting	layer ei	ncoun	itered. Over 6' o	f Silt loa	m or fin	e sand	below	



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Client: 71	Ranch						Location:	Test Pi	t 8			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 5%				
Date: 2/0	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	S	Consistence	D	Т	Q	S	Comments			
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
3" - 144"	2.5YR 4/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt w/ some gravel. Some bigger gravels @ 144". Dry
	End at 144". No G trenches.	iroundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	f silt loa	m below	propos	sed	



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Client: 71	Ranch						Location:	Test Pi	t 9			
Project #:	19-072 71 Ranch -	- Major Sub	division				Slope:	± 5%				
Date: 2/	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments
0" -2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
2" - 150"	10YR 5/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt w/ gravel up to 4". Roots for first 2' and dry.
	End at 150". No G trenches.	Groundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' o	f Silt Loa	am belo	w propo	osed	



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Client: 71	Ranch						Location:	Test Pi	t 10			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 7%				
Date: 2/	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				8	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
3" - 144"	2.5YR 4/2	None	Silty Loam	1	sbk	f	m∨fr	G	W	1	vf	Light tan sandy silt w/ some gravel. Some bigger gravels @ 144". Dry
	End at 144". No G trenches.	Groundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' o	f Silt Loa	am belo	w propo	osed	



Client: 71	Ranch						Location:	Test Pi	t 11			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 8%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazing	g Opera	tion		
Reviewed	By:	MF										
				S	tructu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	T	Q	S	Comments
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
3" - 144"	10YR 5/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt w/ some gravel. Some bigger gravels @ 144". Dry
	End at 144". No G trenches	roundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	[:] silt loai	n below	propos	sed	



												0136 11-2
Client: 71	Ranch						Location:	Test Pi	t 12			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	±4%				
Date: 2/	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	T	Q	S	Comments
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
3" - 144"	10YR 6/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt w/ some gravel. Some bigger gravels @ 144". Dry
	End at 144". No G trenches.	iroundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	f silt loa	m below	propos	sed	



Client: 71	Ranch						Location:	Test Pi	t 13			
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	±8%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments
0" -5"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
5" - 120"	10YR 6/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light chalky sandy silt with some gravel, dry. Roots down to 2' bgs.
120" - 144"	2.5YR 7/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Same material but w/some cobbles up to 5" dia.
	End at 144". No C trenches.	Groundwater	l niting	l layer ei	l ncoun	I tered. Over 6' of	silt loa	l m below	propos	sed		



Client: 71	Ranch						Location:	Test Pi	t 14			Siverse projes
	19-072 71 Ranch -	Maior Sub	division				Slope:	± 8%				
	10/2020	Major Oub					Vegetation:	Native	Range			
Described		НТМ					Land Use:		g Opera	tion		
Reviewed	-	MF						Orazini	gopola			
	- j .			S	tructu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments
0" - 4"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
4" - 18"	2.5YR 5/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt, with fewer fine roots, dry.
18" - 24"	2.5YR 5/2	None	Fine Sandy Loam	2	bk	f	mvfr	С	S	1	vf	Layer of gravelly sand and loam w/ calcium deposits visible in layer. Dry
24" - 156"	2.5YR 5/2	None	Fine Sandy Loam	2	bk	f	mfr	С	S	1	vf	Sand with some loam w/ gravel and cobbles up to 5" dia., Dry.
	End at 156". No G proposed trenche		r, bedrock, or lin	niting	layer ei	ncour	tered. Over 6' o	f find sa	ndy loar	n belov	V	



Client: 71	Panch						Location:	Test Pi	+ 15			Siverse proje
	19-072 71 Ranch	Major Sub	division					± 10%	115			
	19-072 / T Ranch	- Major Sub					Slope:	-	Danaa			
							Vegetation:	Native	-			
Described	-	HTM					Land Use:	Grazin	g Opera	lion		
Reviewed I	By:	MF						1				
		-		-	tructu	-		Bou	ndary		oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments
0" - 2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Т	1	f	Brown topsoil, moist with fine roots
2" - 12"	2.5YR 5/2	None	Fine Sandy Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt, with fewer fine roots, dry. Calcium deposits visible
12" - 60"	2.5YR 5/2	None	Fine Sandy Loam	2	bk	f	mvfr	G	S	1	vf	Sandy silt w/ some gravel up to 1". Dry
60" - 72"	2.5YR 5/2	None	Gravel	2	bk	f	mfr	С	S	1	vf	Gravel seam - gravel up to 3" dia. Dry
72" - 156"	2.5YR 5/2	None	Sand	2	bk	f	mfr	С	S	1	vf	Sandy silt w/ some gravel up to 3" Dry.
	End at 156". No 0	Groundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered.					



Client: 71	Ranch						Location:	Test Pi	t 16			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 5%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	Ву:	HTM					Land Use:	Grazin	g Operat	tion		
Reviewed E	Зу:	MF										
				S	tructu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments
0" -4"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
4" - 24"	2.5YR 4/2	None	Sandy gravel	1	sbk	f	mvfr	G	W	1	vf	Tan/brown sand/pea gravel mix with some fines.
24" - 84"	2.5YR 5/2	None	Fine Sandy Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt, dry. Calcium deposits visible
84" - 120"	2.5YR 6/3	None	Sandy Gravel	1	sbk	f	mvfr	G	W	1	vf	Pitrun/gravel seam with gravel up to 3" dia. Dry
120" - 144"	2.5YR 6/3	None	Sandy Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt w/ gravel.
	End at 144". No G	Groundwate	r, bedrock, or lim	niting	layer er	ncoun	tered.					



Client: 71	Ranch						Location:	Test Pi	t 17			
Project #:	19-072 71 Ranch -	- Major Sub	division				Slope:	± 8%				
Date: 2/	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	T	Q	S	Comments
0" -2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
2" - 150"	2.5YR 5/2	None	Loam	1	sbk	f	m∨fr	G	W	1	vf	Light tan silty sand, dry and fine roots down to 3' bgs.
	End at 150". No G trenches.	Groundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' o	f loam b	elow pro	posed	<u> </u>	



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Client: 71	Ranch						Location:	Test Pi	t 18			
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	± 5%				
Date: 2/2	10/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
	•			S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Ť	Q	S	Comments
0" - 2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
2" - 48"	2.5YR 5/2	None	Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan silty sand, dry and fine roots down to 3' bgs.
48" - 156"	2.5YR 5/2	None	Loamy Sand	2	bk	f	mfr	С	S	1	vf	Sandy silt w/ fine gravel up to 0.5" dia. Dry
	End at 156". No C	Groundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered.	1	1	1	1	



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Client: 71	Ranch						Location:	Test Pi	t 19			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 8%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	T	Q	S	Comments
0" -2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
2" - 22"	2.5YR 3/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Brown sandy silt with fine roots. Dry
22" - 72"	2.5YR 5/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light chalky colored sandy silt w/ some gravel up to 1" dia. Dry
72" - 144"	2.5YR 5/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Darker light chalk w/ some gravel about 50% fines.
	End at 144". No G trenches.	Groundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	f Silty Lo	oam belo	ow prop	oosed	



011	Danak							Test	1.00			Overse proje
Client: 71							Location:	Test Pi	t 20			
	19-072 71 Ranch -	Major Sub	division				Slope:	± 3%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	T	Q	S	Comments
0" -10"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
10" - 96"	2.5YR 5/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Tan sandy silt w/ 40% gravel up to 1" dia. Dry
96" - 108"	2.5YR 5/3	None	Sand/gravel	1	sbk	f	mvfr	G	W	1	vf	Pitrun/gravel seam with gravel up to 3" dia. Dry
108" - 144"	2.5YR 6/3	None	Loamy Sand	1	sbk	f	mvfr	G	W	1	vf	Sandy silt/sand with some gravel up to 4" dia. Dry
	End at 144". No G trenches.	roundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered. 6' of Silty	Loam b	elow pro	oposed		



Client: 71	Danah						Location	Test Pi	+ 01			Siverse proje-
		M : 0					Location:		121			
	19-072 71 Ranch -	Major Sub	division				Slope:	± 5%				
Date: 2/*	10/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	tructu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Ť	Q	S	Comments
0" - 2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
2" - 48"	2.5YR 5/2	None	Sandy Loam	1	sbk	f	mvfr	G	W	1	vf	Sandy silt w/ small gravel up to 1" dia. Dry
48" - 54"	2.5YR 5/2	None	Sand/gravel	2	bk	f	mfr	С	S	1	vf	Gravel seam with gravel up to 2" dia. Dry
54" - 156"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Sandy silt w/ small gravel up to 1" dia. Dry
	End at 156". No G trenches.	Groundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	f Silty Lo	oam belo	ow prop	osed	



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Client: 71	Ranch						Location:	Test Pi	t 22			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 5%				
Date: 2/*	10/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	T	Q	S	Comments
0" - 5"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
5" - 18"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light graysilt sand w/ gravel up to 1" dia. Dry
18" - 46"	2.5YR 5/2	None	Sand/Gravel	2	bk	f	mvfl	С	S	1	vf	Fractured and weathered sandstone bedrock. Easy to dig through.
46" - 144"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light silty sand w/ some gravel up to 2" dia.
	End at 144". No G trenches.	Groundwate	r, bedrock, or lin	niting	layer ei	ncour	tered. Over 6' of	f Silty Lo	bam bel	ow prop	osed	



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Client: 71	Ranch						Location:	Test Pi	t 23						
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 5%							
Date: 2/	10/2020						Vegetation:	Vegetation: Native Range							
Described	By:	HTM					Land Use:	Grazing Operation							
Reviewed	-	MF													
	•			S	Structu	re		Boundary Roo			oots				
Depth (in.)						S	Consistence	D	Ť	Q	S	Comments			
0" -4"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots			
4" - 12"	2.5YR 5/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light chalky silty sand, powder. Dry			
12" - 48"	2.5YR 5/2	None	Coarse Sand	1	sbk	f	mvfr	G	W	1	vf	Sandy gravel with some loam/fines, loose brown/grey. Dry.			
48" - 144"	2.5YR 5/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt w/ some gravel up to 2" dia. Dry.			
	End at 144". No G trenches.	roundwater	r, bedrock, or lin	niting	layer ei	ncour	itered. Over 6' o	f Silty Lo	bam belo	ow prop	posed				



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Client: 71	Ranch						Location:	Test Pi	t 24			
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	± 5%				
Date: 2/2	10/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Boundary Roots				
Depth (in.)	Color	G SH S Consistence	D	Т	Q	S	Comments					
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
3" - 36"	2.5YR 6/3	None	Sandy Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt, Dry.
36" - 72"	2.5YR 6/4	None	Sand/Gravel	2	bk	f	mvfl	с	S	1	vf	Sandstone/fractured pieces w/ gravel. Non restrictive layer - similar to TP #22.
72" - 156"	2.5YR 6/3	None	Sand	1	sbk	f	mvfr	G	W	1	vf	Sand w/ some gravel up to 2" dia. Dry
	End at 144". No 0	Groundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered.		1	<u> </u>	I	



Client: 71	Ranch						Location:	Test Pi	t 24A			Superse proje
	19-072 71 Ranch	- Maior Sub	division				Slope:	± 2%	(20)			
	10/2020						Vegetation:	Native	Range			
Described		HTM					Land Use:					
Reviewed		MF							g Opera			
				Structure				Boundary F			oots	
Depth (in.)							Consistence	D	T	Q	S	Comments
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
3" - 48"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt, Dry.
48" - 156"	2.5YR 6/3	None	Sand	1	sbk	f	mvfr	G	W	1	vf	Sand w/ some gravel up to 2" dia. Dry
	End at 156". No G	Groundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered.	1	1	1	1	



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Client: 71	Ranch						Location:	Test P	t 25						
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	±4%							
Date: 2/	10/2020						Vegetation:	egetation: Native Range							
Described	By:	HTM					Land Use:	Grazin							
Reviewed	By:	MF													
				S	Structu	re		Boundary Roots							
Depth (in.)	n.)					S	Consistence		T	Q	S	Comments			
0" -3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots			
3" - 48"	2.5YR 5/3	None	Fine Sandy Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt, Dry.			
48" - 144"	2.5YR 6/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Lighter tan chalky silt/sand some gravel up to 2" dia. Dry			
	End at 144". No C trenches.	Groundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' o	f Silty L	oam bel	ow prop	bosed				



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Client: 71							Location:	Test Pi	t 26						
	19-072 71 Ranch	- Major Sub	division				Slope:	± 5%							
Date: 2/	10/2020						Vegetation:	tation: Native Range							
Described	By:	HTM					Land Use:	Grazing Operation							
Reviewed	By:	MF													
				Structure				Boundary Roo			oots				
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Ť	Q	S	Comments			
0" -3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots			
3" - 60"	2.5YR 5/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt, Dry.			
60" - 144"	2.5YR 6/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Lighter tan chalky silt/sand some gravel up to 2" dia. Dry			
	End at 144". No G trenches.	Groundwater	r, bedrock, or lin	niting	layer er	ncoun	Itered. Over 6' of	f Silty Lo	oam belo	ow prop	posed				



Client: 71	Ranch						Location:	Test Pi	t 27						
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	± 5%							
Date: 2/	10/2020						Vegetation:	getation: Native Range							
Described	By:	HTM					Land Use:	Grazin							
Reviewed	By:	MF													
				Structure				Boundary Roots			oots				
Depth (in.)	Color	Mottles	Texture	G	SH	s	Consistence	D	Т	Q	S	Comments			
0" -4"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	m∨fr	G	I	2	f	Brown topsoil, moist with fine roots			
4" - 60"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt, Dry.			
60" - 156"	2.5YR 6/3	None	Fine Sandy Loam	1	sbk	f	mvfr	G	w	1	vf	Sandy silt loam w/ some gravel up to 2" dia. Dry			
	End at 156". No G below proposed tro		r, bedrock, or lin	niting	layer er	ncoun	tered. Over 6' of	f Silt Lo	am or Fi	ne San	dy Loan	n			



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Client: 71	Ranch						Location:	Test Pi	t 28						
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	± 3%							
Date: 2/1	0/2020						Vegetation:	Native	Range						
Described	By:	HTM					Land Use:	Grazing Operation							
Reviewed I	By:	MF													
				S	tructu	re		Boundary			Roots				
Depth (in.)	Color	G SH S		Consistence	D	T	Q	S	Comments						
0" -4"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	m∨fr	G	Ι	2	f	Brown topsoil, moist with fine roots			
4" - 30"	2.5YR 6/3	None	Silty Loam	1	sbk	f	m∨fr	G	W	1	vf	Tan silt fairly loose, Dry			
30" - 54"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Darker tan silt and more dense. Dry			
54" - 120"	2.5YR 6/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light chalky silt sand, Dry			
120" - 156"	2.5YR 6/2	None	Silty Loam	1	sbk	f	m∨fr	G	W	1	vf	Darker tan silt and dense, Dry.			
	End at 156". No G trenches.	Groundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	f silty loa	am belo	w propo	osed				



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Client: 71	Ranch						Location:	Test Pi	t 29					
Project #:	19-072 71 Ranch -	- Major Sub	division				Slope:	± 5%						
Date: 2/1	10/2020						Vegetation: Native Range							
Described	By:	HTM					Land Use:	Grazin	g Opera	tion				
Reviewed	By:	MF												
	-			S	tructu	re		Boundary			Roots			
Depth (in.)	Color	S	Consistence	D	T	Q	S	Comments						
0" -4"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	2	f	Brown topsoil, moist with fine roots		
4" - 24"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Tan silt fairly loose, Dry		
24" - 60"	24" - 60" 2.5YR 6/2 None Silty Loam					f	mvfr	G	W	1	vf	Darker tan silt and more dense. Dry		
60" - 96"	2.5YR 6/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light chalky silt sand, Dry		
96" - 144"	2.5YR 6/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Darker tan silt and dense, Dry.		
	End at 156". No G trenches.	Groundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	f Silty Lo	oam belo	ow prop	osed			



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Client: 71							Location:	Test P	130					
	19-072 71 Ranch	- Major Sub	division				Slope:	± 8%						
Date: 2/	10/2020						Vegetation: Native Range							
Described	By:	HTM					Land Use:	Grazin	g Opera	tion				
Reviewed	Ву:	MF												
				S	Structu	re		Boundary Roots			oots			
Depth (in.)	Color	Texture	G	SH	S	Consistence	D	Ť	Q	S	Comments			
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	2	f	Brown topsoil, moist with fine roots		
3" - 18"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Darker sandy silt w/ calcium deposit visible. Dry		
18" - 156"	2.5YR 6/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light Tan Sandy Silt material with some gravel up to 3" dia. Dry		
	End at 156". No G trenches.	Groundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	f Silty Lo	pam belo	ow prop	posed			



Client: 71	Ranch						Location:	Test Pi	t 31						
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	± 10%							
Date: 2/2	10/2020			Vegetation: Native Range											
Described	By:	HTM					Land Use:	Grazing Operation							
Reviewed	Ву:	MF													
				S	Structu	re		Boundary			Roots				
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments			
0" - 2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	m∨fr	G	Ι	2	f	Brown topsoil, moist with fine roots			
2" - 18"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Darker sandy silt w/ calcium deposit visible. Dry			
18" - 156"	2.5YR 6/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt w/ some gravel. Gravel seam @ 52" Dry			
	End at 156". No G trenches.	l Groundwater	r, bedrock, or lin	niting	l layer ei	ncoun	tered. Over 6' of	f Silty Lo	bam belo	ow prop	bosed				



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Client: 71							Location:	Test Pi	t 32					
Project #:	19-072 71 Ranch	 Major Sub 	division				Slope:	± 10%						
Date: 2/2	10/2020						Vegetation:	Native	Range					
Described	By:	HTM					Land Use:	Grazing	g Opera	tion				
Reviewed	By:	MF												
				S	Structu	re		Boundary			Roots			
Depth (in.)	Color	Texture	G	SH	S	Consistence	D	Ť	Q	S	Comments			
0" -8"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	m∨fr	G	Ι	2	f	Brown topsoil, moist with fine roots		
8" - 30"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	2	f	Fine sandy silt w/ roots, Dry.		
30" - 156"	2.5YR 6/2	None	Sand	1	sbk	f	mvfr	G	W	1	vf	Orange/brown sand w/ pea gravel. Dry.		
	End at 156". No 0	Groundwate	, bedrock, or lin	niting	layer ei	ncoun	tered.	1		1	1			



Client: 71	Panch						Location:	Test Pi	+ 22			Siverse proje
		Major Sub	division					± 2%	1 33			
	19-072 71 Ranch	- Major Sub	aivision				Slope:					
	10/2020						Vegetation:		Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	Ву:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments
0" -5"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
5" - 24"	2.5YR 5/2	None	Silty Loam	1	sbk	f	mvfr	G	w	1	vf	Fine sandy silt w/ roots, Dry.
24" - 144"	2.5YR 6/2	None	Fine Sandy Loam	1	sbk	f	mvfr	G	w	1	vf	Sandier material w/ gravel w/ some pea gravel, Dry
	End at 144". No G proposed trenches		r, bedrock, or lin	niting	layer ei	ncoun	itered. Over 6' of	f Fine S	andy Lo	am bel	ow	



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Client: 71	Ranch						Location:	Test Pi	t 34			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 10%				
Date: 2/2	10/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	tructu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments
0" -4"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	I	1	f	Brown topsoil, moist with fine roots
4" - 48"	2.5YR 6/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan sandy silt, Dry with roots down to 2' bgs.
48" - 96"	2.5YR 5/3	None	Sand	1	sbk	f	mvfr	G	W	1	vf	Sand w/ some silt, Dry.
96" - 144"	2.5YR 4/2	None	Loamy Sand	1	sbk	f	mvfr	G	W	1	vf	Light Tan Sand with more silt, Dry
	End at 144". No G	iroundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered.	•	-		•	



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Client: 71	Ranch						Location:	Test Pi	t 35			
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	± 13%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Texture	G	SH	S	Consistence	D	Ť	Q	S	Comments	
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
3" - 60"	2.5YR 6/3	None	Fine Sandy Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan silty/sandy gravel up to 1" dia. Dry
60" - 144"				sbk	f	mvfr	G	W	1	vf	Cleaner sand w/ gravel up to 3" dia. Dry	
	End at 144". No G	Groundwater	, bedrock, or lin	niting	layer ei	ncoun	tered.	1			1	



-												C/3E F1-2
Client: 71	Ranch						Location:	Test Pi	t 36			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 12%				
Date: 2/0	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	n.)					S	Consistence	D	Т	Q	S	Comments
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	m∨fr	G	I	1	f	Brown topsoil, moist with fine roots
3" - 144"	2.5YR 6/3 None Silty Loam 1 sbk						m∨fr	G	W	1	vf	Light tan silty/sand with gravel up to 1" dia. Dry
	End at 144". No G trenches.	iroundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	f Silty Lo	bam belo	ow prop	osed	



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Client: 71	Ranch						Location:	Test Pi	t 37			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 8%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed		MF										
	-			S	tructu	re		Bou	ndary	R	oots	
Depth (in.)	.)				S	Consistence	D	T	Q	S	Comments	
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
3" - 144"	2.5YR 6/3 None Silty Loam 1 sbk						mvfr	G	W	1	vf	Light tan silty sand, Dry.
	End at 144". No G trenches.	roundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	Silty Lo	am belo	ow prop	osed	



												C/3E F1-2
Client: 71	Ranch						Location:	Test Pi	t 38			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 5%				
Date: 2/	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	n.)					S	Consistence	D	Т	Q	S	Comments
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	m∨fr	G	I	1	f	Brown topsoil, moist with fine roots
3" - 144"	" 2.5YR 6/3 None Silty Loam 1 sbk						m∨fr	G	W	1	vf	Light tan silty/sand with gravel up to 1" dia.
	End at 144". No G trenches.	iroundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	f Silty Lo	bam belo	ow prop	osed	



												C/3E F1-2
Client: 71	Ranch						Location:	Test Pi	t 39			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	± 10%				
Date: 2/	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	n.)					S	Consistence	D	Т	Q	S	Comments
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	m∨fr	G	I	1	f	Brown topsoil, moist with fine roots
3" - 144"	2.5YR 6/3	None	Silty Loam	1	sbk	f	m∨fr	G	W	1	vf	Light tan silty sand, Dry
	End at 144". No G trenches.	iroundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' of	f Silty Lo	oam belo	ow prop	osed	



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Client: 71	Ranch						Location:	Test Pi	t 40			
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	± 5%				
Date: 2/	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
	-			S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	n.)					S	Consistence	D	Т	Q	S	Comments
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
3" - 156"	- 156" 2.5YR 6/3 None Silty Loam 1 sbk					f	mvfr	G	W	1	vf	Sandy silt w/ some gravel. Cobbles near bottom. More gravel up to 3" dia. @ 72", Dry
	End at 156". No G trenches.	Groundwate	r, bedrock, or lin	niting	layer ei	ncoun	tered. Over 6' o	f Silty Lo	oam belo	ow prop	osed	



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Client: 71	Ranch						Location:	Test Pi	t 41A			
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	± 5%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed		MF										
	-			S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	(in.)					S	Consistence	D	T	Q	S	Comments
0" - 3"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	m∨fr	G	Ι	1	f	Brown topsoil, moist with fine roots
3" - 60"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan silty/sand with some gravel up to 1" dia. Dry
60" - 144"	2.5YR 6/2	None	Loamy Sand	1	sbk	f	mvfr	G	W	1	vf	Cleaner sand w/ gravel up to 2" dia. Dry
	End at 144". No 0	Groundwate	r, bedrock, or lin	niting	l layer ei	ncoun	tered.	1			I	



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Client: 71	Ranch						Location:	Test Pi	t 41B			
Project #:	19-072 71 Ranch	- Major Sub	division				Slope:	± 5%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
				S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	Color	Mottles	Texture	G	SH	S	Consistence	D	Т	Q	S	Comments
0" - 2"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
2" - 48"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan silty/sand with some gravel up to 1" dia. Dry
48" - 144"	2.5YR 6/2	None	Sand/Gravel	1	sbk	f	mvfr	G	W	1	vf	Pitrun type gravel w/ cobbles 6" increasing as depth increases
	End at 156". No G	Groundwater	, bedrock, or lin	niting	layer ei	ncoun	itered.	<u> </u>	I	<u> </u>	I	



r							1					Olverse proje
Client: 71	Ranch						Location:	Test Pi	t 41C			
Project #:	19-072 71 Ranch -	Major Sub	division				Slope:	±1%				
Date: 2/6	6/2020						Vegetation:	Native	Range			
Described	By:	HTM					Land Use:	Grazin	g Opera	tion		
Reviewed	By:	MF										
	-			S	Structu	re		Bou	ndary	R	oots	
Depth (in.)	(in.)					S	Consistence	D	Ť	Q	S	Comments
0" - 4"	2.5YR 4/3	None	Loamy Sand	1	sbk	f	mvfr	G	Ι	1	f	Brown topsoil, moist with fine roots
4" - 72"	2.5YR 6/3	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan powdery silt w/ sand tiny bit of gravel up to 1' dia. Dry
72" - 108"	2.5YR 4/2	None	Sand/Gravel	1	sbk	f	mvfr	G	W	1	vf	Cobbles and gravel and pitrun type material, Dry
108" - 156"	2.5YR 4/2	None	Silty Loam	1	sbk	f	mvfr	G	W	1	vf	Light tan powdery silt w/ sand tiny bit of gravel up to 4 dia.
	End at 156". No G trenches.	iroundwater	r, bedrock, or lin	niting	layer ei	ncoun	tered. 7' of Silty	Loam b	elow pro	oposed		

Appendix C

Well Information

- Horse Creek Hills Test Well Program and Summary

 Test Well Logs
- Horse Creek Hills Pump Test Well Log

 Pump Test Results and Graph

Test Well Program & Summary

This narrative provides for the summary, intent, and results of the Test Well Program & Summary for the Horse Creek Hills Subdivisions, which was used in the evaluation of the proposed wastewater treatment system evaluations of the Horse Creek Hills 1-4 subdivisions.

The proposed project is located approximately 0.25 miles east of Canyon Ferry Reservoir at the location where Lower Confederate Road reaches the lake. The legal description of the approximately 435-acre is Section 31, Township 9 North, Range 2 East, Principal Meridian Montana, Broadwater County, Montana. The subject property is currently used for cattle grazing purposes. The current projects are proposing to develop the subject property into a 41-lot major subdivision.

Three test wells were drilled in the project area to provide for site specific data for evaluation of the proposed wastewater absorption areas to assess site specific groundwater depths, groundwater flow gradient, hydraulic conductivity, and background nitrate concentrations in the first 15 ft of the first aquifer. We sampled nitrates and conductivity on the three TWs for data to be used in our non-degradation analysis.

Additionally, a production well was drilled on Lot #13 to be used for pump testing analysis. This well was drilled to a depth beyond the first 15-ft of the first aquifer. The well was pump tested on January 30th, 2020. The pump testing occurred at a rate of 15 gallons-per-minute for a duration of 8 hours. A pressure transducer was placed in the pump testing well to analyze water depths while pumping. Another pressure transducer was placed in Test Well #1 while the pump test was ran to evaluate any potential drawdown in the aquifer from the pump test. Test Well #1 did not see any abnormal fluctuation of static water level during the pump test of the production well.

Per the attached site plan, the following Test Wells were drilled, as described below. Included are some summary notes.

TW #1 - (GWIC Id: 304166)

TW #1 was installed on November 26, 2019 by H&L Drilling on Lot #7 for testing, sampling and monitoring purposes only (not intended for potable use). Allied Engineering measured the static water level at 82.42 ft below ground surface – at an elevation of 3795.66 feet above sea level. A background nitrate sample was taken by the driller at first water and was found to 0.50 mg/l. A pump test was performed for approximately 1 hrs at a pumping rate of 8.5 gpm. The well was completed on November 26, 2019. Hydraulic Conductivity was found to be 97.06 ft/day (calculations included in the Non-Degradation Report).

TW #2 - (GWIC Id: 304169)

TW #2 was installed on November 26, 2019 by H&L Drilling on Lot #25 for testing, sampling and monitoring purposes only (not intended for potable use). Allied Engineering measured the static water level at 91.06 ft below ground surface – at an elevation of 3794.24 feet above sea level. A background nitrate sample was taken by the driller at first water and was found to 1.30 mg/l. A pump test was performed for approximately 1 hrs at a pumping rate of 9 gpm. The well

was completed on November 26, 2019. Hydraulic Conductivity was found to be 137.87 ft/day (calculations included in the Non-Degradation Report).

TW #3 - (GWIC Id: 304167)

TW #3 was installed on November 26, 2019 by H&L Drilling on Lot #37 for testing, sampling and monitoring purposes only (not intended for potable use). Allied Engineering measured the static water level at 169.57 ft below ground surface – at an elevation of 3801.60 feet above sea level. A background nitrate sample was taken by the driller at first water and was found to 0.97 mg/l. A pump test was performed for approximately 1 hrs at a pumping rate of 11 gpm. The well was completed on November 26, 2019. Hydraulic Conductivity was found to be 87.59 ft/day (calculations included in the Non-Degradation Report).

Pumping Well #1 - (GWIC Id: 304170)

Pumping Well #1 was installed on November 26, 2019 by H&L Drilling on Lot #13 for testing, sampling and monitoring purposes and future potable usage. The pumping well was drilled beyond the first 15 feet of the aquifer to be used to pump test and find if the aquifer had adequate water supply. A pump test was performed for approximately 8.08 hrs at a pumping rate of 15 gpm. The static level of the well recovered in less than 8 hours as shown on the pump testing graph in Appendix C. The pump test was conducted on January 30th of 2020. Hydraulic Conductivity was found to be 79.60 ft/day (calculations included in the Non-Degradation Report).

<u>Summary</u>

The groundwater mapping was based measurements conducted on the three (3) test wells that were drilled into the first aquifer. The depth to first water was recorded for each well and the well heads and existing ground surface were surveyed. A groundwater surface was developed based on the field measurements, and the hydraulic gradient was subsequently determined to be 0.0021 ft/ft with a direction of South 38 degrees, 34 minutes, and 40 Seconds West.

We obtained background nitrate samples from the first aquifer in each the test wells. The background nitrates for TW #1-3 were determined to be 0.50 mg/L, 1.30 mg/L and 0.97 mg/L respectively. For the purpose of this application, we have the three values as outlined in the non-degradation manual and used a background nitrate level of 0.923 mg/L for this application. Hydraulic Conductivity for the TWs #1-3 was found to be 97.06 ft/day, 137.87 ft/day, and 87.59 ft/day, respectively using the Razack and Huntley Method. Those three values were averaged with the results of the 8 hour pump test on Pumping Well #1 that had an estimated hydraulic conductivity of 79.60 ft/day using the Razack & Huntley Method. The average value was 100.5 ft/day was used in the Non-Degradation report.

This well log reports the activities of a licensed Montana well driller, serves as the official record of work done within the borehole and casing, and describes the amount of water encountered. This report was completed online by the driller. Acquiring water rights is the well owner's responsibility and is NOT accomplished by the filing of this report.

Site Name: 71 RANCH LP GWIC Id: 304166

Section 1: Well Owner(s) 1) GALT, ERROL (MAIL) 106 71 RANCH RD MARTINSDALE MT 59053

Section 2: Location

Township	Range	Section	Quarter Se	ections
09N	02E	31	SE1/4 NE1/4	SW1/4
	County		Geoc	ode
BROADWATER				
Latitude	Longitude)	Geomethod	Datum
Addition			Block	Lot
HORSE CREEK H	HILLS			4R

Section 3: Proposed Use of Water

TEST WELL (1)

Section 4: Type of Work

Drilling Method: ROTARY

Section 5: Well Completion Date

Date well completed: Monday, November 25, 2019

Section 6: Well Construction Details Meta Data Fields

1. Was borehole completed as a well? YES 2. Was well abandoned?

Borehole dimensions

From	То	Diameter				
0	108	6				
Casin	g					
From	То	Diameter	Wall Thicknes	Pressu s Rating	re Joint	Туре
-2	108	6	0.250		WELDED	A53B STEEL
Comp	letio	n (Perf/Sc	reen)		B	
From	То		# of Openings	Size of Openings	Description	
93	108	6	23	6"X5/16"	TORCH OR	PLASMA CUTS
Annula	ar S	pace (Seal	/Grout/Pac	ker)	3	
From	To	Descriptio	Cont. Fed?			
0	93	BENTONIT	EY			

Section 7: Well Test Data

Total Depth: 108 Static Water Level: 84 Water Temperature:

Air Test *

<u>8.5</u> gpm with drill stem set at <u>108</u> feet for <u>1</u> hours. Time of recovery <u>0.07</u> hours. Recovery water level <u>84</u> feet.

* During the well test the discharge rate shall be as uniform as possible. This rate may or may not be the sustainable yield of the well. Sustainable yield does not include the reservoir of the well casing.

Section 8: Remarks

TW-1

Section 9: Well Log

From	То	Description
0	8	SILTY CLAY
8	17	SILTY SAND/GRAVEL
17	24	SANDY CLAY
24	50	SAND
50		SAND/GRAVEL
78		CLAY
93	105	GRAVEL/SAND
105	108	GRAVEL/CLAY

Driller Certification

All work performed and reported in this well log is in compliance with the Montana well construction standards. This report is true to the best of my knowledge.

This well log reports the activities of a licensed Montana well driller, serves as the official record of work done within the borehole and casing, and describes the amount of water encountered. This report was completed online by the driller. Acquiring water rights is the well owner's responsibility and is NOT accomplished by the filing of this report.

Site Name: 71 RANCH LP GWIC Id: 304169

Section 1: Well Owner(s) 1) GALT, ERROL (MAIL) 106 71 RANCH RD MARTINSDALE MT 59053

Section 2: Location

Township 09N	Range 02E	Section 31	Quarter S		
	County		Geocode		
BROADWATER					
Latitude	Longitud	e	Geomethod	Datum	
Addition			Block	Lot	
HORSE CREEK H	HLLS			18R	

Section 3: Proposed Use of Water TEST WELL (1)

Section 4: Type of Work

Drilling Method: ROTARY

Section 5: Well Completion Date

Date well completed: Thursday, November 21, 2019

Section 6: Well Construction Details Meta Data Fields

Was borehole completed as a well? YES
 Was well abandoned?

Borehole dimensions

From	То	Diameter	-						
0	135	6							
Casin	g								
From	То	Diameter	Wal Thio	-		ssure ing	Joint		Туре
-2	135	6	0.25	50			WELD	ED	A53B ST
Comp	letio	n (Perf/Sc	reen)					
From	То	Diamete	~ I	# of Openir	igs	Size Oper	of nings	D	escription
120	13	56		23		6"X5/16"		SAW SLOT	
Annul	ar S	pace (Seal	/Gro	ut/Pac	ker)				
From	То	Descriptio		ont. ed?					
0	120	BENTON	TEY						

Section 7: Well Test Data

Total Depth: 135 Static Water Level: 93 Water Temperature:

Air Test *

 $\underline{9}$ gpm with drill stem set at <u>135</u> feet for <u>1</u> hours. Time of recovery <u>0.12</u> hours. Recovery water level <u>93</u> feet.

* During the well test the discharge rate shall be as uniform as possible. This rate may or may not be the sustainable yield of the well. Sustainable yield does not include the reservoir of the well casing.

Section 8: Remarks

TW-2

Driller Certification

EEL

S

All work performed and reported in this well log is in compliance with the Montana well construction standards. This report is true to the best of my knowledge.

This well log reports the activities of a licensed Montana well driller, serves as the official record of work done within the borehole and casing, and describes the amount of water encountered. This report was completed online by the driller. Acquiring water rights is the well owner's responsibility and is NOT accomplished by the filing of this report.

Site Name: 71 RANCH LP GWIC Id: 304167

Section 1: Well Owner(s) 1) GALT, ERROL (MAIL) 106 71 RANCH RD MARTINSDALE MT 59053

Section 2: Location

Township	Range	Section	Quarter S	ections
09N	02E	31	SE1/4 NE1/4 SW1/4	
	County		Geod	code
BROADWATER				
Latitude	Longitud	le	Geomethod	Datum
Addition			Block	Lot
HORSE CREEK H	HILLS			39R

Section 3: Proposed Use of Water

TEST WELL (1)

Section 4: Type of Work

Drilling Method: ROTARY

Section 5: Well Completion Date

Date well completed: Tuesday, November 19, 2019

Section 6: Well Construction Details Meta Data Fields

1. Was borehole completed as a well? YES 2. Was well abandoned?

Borehole dimensions

From	То	Diameter							
0	200	6	1						
Casin	g								
From	То	Diameter	1.00	/all hicknes	S	Pressu Rating	re	Joint	Туре
-2	200	6	0.	250				WELDED	A53B STEEL
Comp	letio	n (Perf/Sc	reel	n)					
From	То	Diameter		# of Size Openings Ope		ze of penings	D	escription	
185	200	6	23		6		Т	ORCH OR P	PLASMA CUTS
Annul	ar Sj	oace (Seal	/Gr	out/Pac	ke	r)			
From	То	Descriptio		Cont. Fed?					
0	185	BENTONI	TE	Y					

Section 7: Well Test Data

Total Depth: 200 Static Water Level: 173 Water Temperature:

Air Test *

<u>11</u> gpm with drill stem set at <u>200</u> feet for <u>1</u> hours. Time of recovery <u>0.06</u> hours. Recovery water level <u>173</u> feet.

* During the well test the discharge rate shall be as uniform as possible. This rate may or may not be the sustainable yield of the well. Sustainable yield does not include the reservoir of the well casing.

Section 8: Remarks

TW-3

Section 9: Well Log

From	То	Description
0	28	SILTY TAN CLAY
28	42	GRAVEL/SAND
42	118	CLAY/GRAVEL/SAND
118	155	SAND/GRAVEL
155	164	HARD CLAY
164	185	SAND/GRAVEL/CLAY
185	200	SAND/GRAVEL

Driller Certification

All work performed and reported in this well log is in compliance with the Montana well construction standards. This report is true to the best of my knowledge.

CONSTRUCTION SPECIFICATIONS

Initial Static Water Level: 83.	Q Number of Pumpi	ing Stens:	IWI	
Depth to pump intake:	, Number of Pump	ing Steps:		
Water measurement device:	Jell Probe	anna Maria an Anna Anna Anna Anna Anna Anna Anna		
Total Well Depth: 108	, , , , , , , , , , , , , , , , , , , ,	Driller's Production Estimate	8.5 GI	SM
Total Well Depth: Casing Diameter:La"		Driller's Production Estimate Depth to screen interval:		
Notes: Drawdown = Initial stati Initial Static Water Level:		r level Pumping Water Level: 100	,	
STEP ONE	Date 01/21/2020	Start Time 11: DD A.M		
50% of design production		1		
Time Since	Actual Time Since Start	Depth to Pumping Water	Drawdown	Pumping Rate
Start (minutes)	(minutes)	Level (ft.)	(ft.)	(gpm)
1				
2				
3				
4		0	Y	
5	11:05	87		6
6				
8				
9				
10	11:10	89		8
11				
12				
13				
14				
15	11:15	89.6		9
17				0
19 2D	11:20	89.7		9
23	11.20	01.1		
25	11:25	89.7		9
27			1. 10	
29				
30	11:30	89.7		9
35	11:35	B9.8		9
40	11:40	89.8		q
45 50	11:45	B9.8		
55		1210-00		
60	12:00	89.8		9
70			(1961) - F. K.	
80				
90				
100				
115 130				
145				
145				
180				
210				
240				
270				
300				
Field Notes:				
Field Notes.				

PUMPING TEST DATA SHEET

USDA-NRCS-Montana

RECOVERY TEST	Date 01/21/2020	Start Time 12:01 PM	End Time <u>12:40</u>
Time Since Start (minutes)	Actual Time Since Start (minutes)	Depth to Water Level (ft.)	Residual Drawdown (ft.)
1	12:01	Ble.B	
2	12:02	85.7	
3	12:03	85.2	
4	12:04	85.1	
5	12:05	85	
6			
7			
8			
9	12:10	B4.8 1/2	
10	12.10	64.8/2	
11			
12			
<u> </u>	12:15	84.8	
13	14.12	0-1.0	
19			
20	12:20	B4.71/2	
23	12.20	0-1. 16	
25	12:25	84.7	
27	1 500 . 500		
29			
30	12:30	84.6 1/2	
35			
40	12:40	B4.(e	
45			
50			
55			
60			
70			
80			
90			
100			
115			
130			
145			
160			
<u>180</u> 210			
240			
240			
300			
Anno 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997			

RECOVERY TEST DATA SHEET JW1

USDA-NRCS-Montana

PUMPING TEST DATA SHEET 1W2

Initial Static Water Level: 93 Depth to pump intake: 125	, Number of Pump	ing Steps:		
Water measurement device:	all trake			
Water measurement device: Total Well Depth: Casing Diameter:	GIT FUEL	Driller's Production Estimate	9	
Casing Diameter:		Depth to screen interval:		
	2 D			
Notes: Drawdown = Initial stati Initial Static Water Level: 9	c water level - pumping wate 3, 8	r level Pumping Water Level: 125 Start Time 1:00 PM		
STEP ONE	$\frac{3.8}{\text{Date }01/21/2020}$	Start Time 1:00 PM		
50% of design production				
Time Since Start (minutes)	Actual Time Since Start (minutes)	Depth to Pumping Water Level (ft.)	Drawdown (ft.)	Pumping Rate (gpm)
1	1.01	95.9		ID
2	1:02	96.2		ID
3	1:03	96.4		10
4	1:04	9 le. le		10
5	1:05	96.7		10
6				
7				
8				
9	. 1			
10	1:10	96.9		10
11				
12	22			
13				
14	11/12	09.0		10
15	1:15	97.0		10
17				
19 2D	1:20	97.0		10
23	1.40	11.0		
25	1:25	97.0	The later of the second s	10
27				
29		1 (CA210)		
30	1'.30	97.5		10
35				
40				
45	1:45	97.5		10
50				
55	And a Another and		AV	
60	2:00	97.5		10
70				
80				
90				
100				
113				
145				
145				
180				
210				
240				
270				
300				
Field Notes:				

Actual Time Since Start	Depth to Water Level (ft.)	D 1 ID I
(minutes)		Residual Drawdown (ft.)
2'01	95.1	
2:02	94.6	
2:03	94.31/z	
2'04	94.2	
2'05	94.1	
2		
2:10	93.9	
	5	
2:15	93.9	
2'20	93.9	
	12.1	
2'25	93.9	
		-
2120	929	
6:20	1	
		1
		-
	2!25	2:10 2:10 2:15 93.9 2:20 93.9 2:25 93.9

RECOVERY TEST DATA SHEET $\top w^2$

USDA-NRCS-Montana

CONSTRUCTION SPECIFICATIONS

PUMPING TEST DATA SHEET 1W3

Vater measurement device: We	1) Probe			
Vater measurement device: <u>We</u> otal Well Depth: <u>200</u> Casing Diameter: <u>12</u>		Driller's Production Estimate:		
		Depth to screen interval:		
Notes: Drawdown = Initial stati	c water level - numping wate	r lavel		
Notes: Drawdown = Initial stati Initial Static Water Level:	2.5	umping Water Level: 190		
STEP ONE	$\frac{12.5}{\text{Date } D1/21/2020}$	Start Time 2:30 PM		
50% of design production				
Fime Since	Actual Time Since Start	Depth to Pumping Water	Drawdown	Pumping Rate
Start (minutes)	(minutes)	Level (ft.)	(ft.)	(gpm)
1	2:31	178.8		10
2	2:32	179.6		10
3	2:33	180		JD
4	2:34	180.2		10
5	2:35	180.3		10
7				
8				
9				
10	2:40	180.8		10
		1.00.0		
12				
13				
14	0/1-			
15	2:45	181.1		10
<u>17</u> 19				
20	2:50	101016		
23	A.50	181.21/2		10
25	2:55	181.21/2		10
27		101.2/2		10
29				
30	3:00	181.21/2		10
35				
40	0.115			
<u> </u>	3:15	181.4		10
55				
60	3:30	181.4		15
70	0.00	101.7		10
80				
90				
100				
115				
130 145				
145				
180				
210				
240				
270				
300				

RECOVERY TEST	Date_01/21/2020	Start Time <u>3:31</u>	End Time
Time Since Start (minutes)	Actual Time Since Start (minutes)	Depth to Water Level (ft.)	Residual Drawdown (ft.)
1	3:31 3:32 3:33 3:34 3:35	177.2	
2	3'32	175	
3	3:33	173.8	
4	3'34	173.2	
5	3:35	173	
6			
7			
8			
9			
10	3.4D	172.6	
11			
12			
13			
13			
15	3:45	172.5	
17			
19			
21			
23			
25			
27			
29			
30			
35			
40			
45			y, 2012 10 yr
50			
55			
60			
70			
80			
90			
100			
115			
130			
145			
160			
180			
210			
240			
270			
300	ante de contra atén		
	- Initial Statia Watar I av	rel – Measured Water Level.	

RECOVERY TEST DATA SHEET $\neg w \beta$

USDA-NRCS-Montana

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Site Name: 71 RANCH LP GWIC Id: 304170

Section 1: Well Owner(s) 1) GALT, ERROL (MAIL) 106 71 RANCH RD MARTINSDALE MT 59053

Section 2: Location

Township 09N	Range 02E County	Section 31	Quarter S SE¼ NE½ Geoo	4 SW1/4
BROADWATER Latitude	Longitude		Geomethod	Datum
Addition HORSE CREEK H	ILLS		Block	Lot 14R

Section 3: Proposed Use of Water DOMESTIC (1)

Section 4: Type of Work

Drilling Method: ROTARY

Section 5: Well Completion Date

Date well completed: Friday, November 22, 2019

Section 6: Well Construction Details Meta Data Fields

1. Was borehole completed as a well? YES 2. Was well abandoned?

Borehole dimensions

From	То	Diameter	r						
0	180) 6	5						
Casin	g		-						
From	То	Diamete	Wall r Thicknes	Pressu ss Rating		Joint	Туре		
-2	180	6	0.250			WELDED	A53B STEEL		
Comp	letio	n (Perf/Sc	reen)						
From	То	Diameter	# of Openings	Size of Openings	Description				
165	180		23		TORCH OR PLASMA CUTS				
Annul	ar S	oace (Seal	/Grout/Pac	ker)			21011/10010		
From		Descriptio	Cont.	(10) No. (*)					
0	165	BENTONT	IE Y						

Section 7: Well Test Data

Total Depth: 180 Static Water Level: 143 Water Temperature:

Air Test *

18 gpm with drill stem set at 180 feet for 1 hours. Time of recovery 0.05 hours. Recovery water level 143 feet.

* During the well test the discharge rate shall be as uniform as possible. This rate may or may not be the sustainable yield of the well. Sustainable yield does not include the reservoir of the well casing.

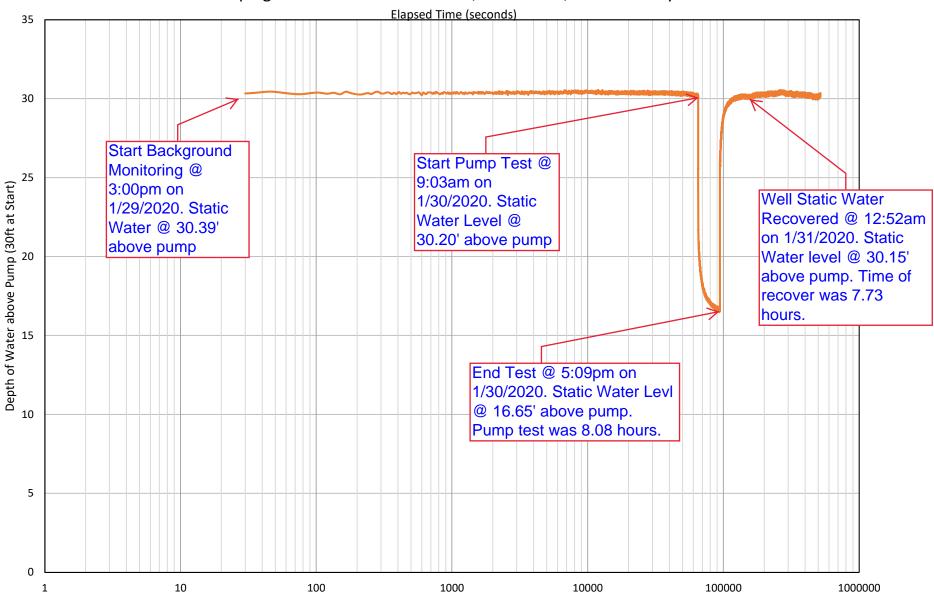
Section 8: Remarks PW-1

Section 9: Well Log

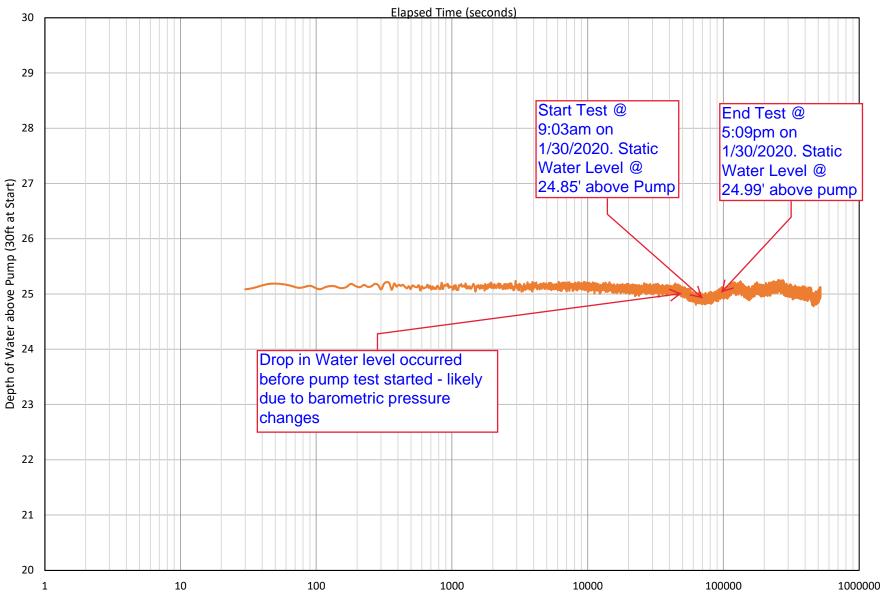
From	То	Description
0	42	SILT/SAND/CLAY/GRAVEL
42	55	FINE SAND
55		CLAY
100	112	SAND/GRAVEL
112	165	CLAY/SAND/GRAVEL
165	180	GRAVEL/SAND
\rightarrow		

Driller Certification

All work performed and reported in this well log is in compliance with the Montana well construction standards. This report is true to the best of my knowledge.



Pumping Well #1 Static Water Level, Drawdown, and Recovery



Observation Well #1 Static Water Level, Drawdown, and Recovery

Appendix D

Non-degradation Analysis

- Nitrate Sensitivity Analysis
 - Hydraulic Conductivity Calculations
 - Background Nitrate Results
- Nitrate Sensitivity Analysis for Cumulative Effects (Spreadsheet Calculations)
 - Adjacent to State Waters Calculations
 - Stream Stats Data for Canyon Ferry Flow
- Phosphorous Breakthrough Analysis
 - Phosphorous Breakthrough Analysis (Spreadsheet Calculations)
- Categorical Exemptions Appendix P of Non-degradation

MONTANA DEPARTMENT OF ENVIRONMENTAL QUALITY NITRATE SENSITIVITY ANALYSIS

Project:	Horse Creek Hills Subdivisions 1-4
Project Number:	19-072
Lot:	38 - Worst-Case-Scenario of Drainfield Width Perp. To GW Flow
Location:	Broadwater County, Montana



	DESCRIPTION	VALUE	
K	Hydraulic Conductivity	100.53	
1	Hydraulic Gradient	0.0021	,
D	Mixing Zone Thickness (usually constant)	30.0	
L	Mixing Zone Length (see ARM 17.30.517(1)(d)(viii)	200	
Ŷ	Width of Drainfield Perpendicular to Ground Water Flow	33.0	ft
Ng	Background Nitrate (as Nitrogen) Concentration	0.923	ma/L
Nr	Nitrate (as Nitrogen) Concentration in Precipitation (usually constant)		mg/L
Ne	Nitrate (as Nitrogen) Concentration in Effluent	50.00	
#I	Number of Single Family Homes on the Drainfield	1.00	÷
QI	Quantity of Effluent per Single Family Home	26.70	ft3/day
Р	Precipitation		in/year
V	Percent of Precipitation Recharging Ground Water (usually constant)	0.2	•
EQUATIONS			
W	Width of Mixing Zone Perpendicular to Ground Water Flow	68	ft
	= (0.175)(L)+(Y)		
Am	Cross Sectional Area of Aquifer Mixing Zone = (D)(W)	2040	ft2
As	Surface Area of Mixing Zone = (L)(W)	13600	ft2
Qg	Ground Water Flow Rate = (K)(I)(Am)	434.7707	ft3/day
Qr	Recharge Flow Rate = (As)(P/12/365)(V)	8.694064	ft3/day
Qe	Effluent Flow Rate = (#I)(QI)	26.7	ft3/day
SOLUTION			
Nt	Nitrate (as Nitrogen) Concentration at End of Mixing Zone	<u>3.71</u>	mg/L
	=((Ng)(Qg)+(Nr)(Qr)+(Ne)(Qe)) / ((Qg)+(Qr)+(Qe))		

REV. 03/2005

Conductivity

HYDRAULIC	CONDUCTIVITY	ANALYSIS
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Project: Project Number: Location:

Horse Creek Hills Subdivisions 1-4 19-072 Broadwater County, Montana



	RAZACK & HUNTLEY METHOD														
Well Owner Name	GWIC ID V	Nell Loo	cation			Bottom of Well Casing (ft)	Water Level After Pumping (ft)	Static Water Level Before Pumping (ft)	Yield (gpm)	Length of Test (hours)	Length of Perforated Casing (ft)		Transmissivity T (gpd/ft)	b ¹	Hydraulic Conductivity (ft/day)
Pump Well 1 Test Well #1 Test Well #2 Test Well #3	304170 304166 304169 304167	CBD CBD CBD CBD	Sec. Sec.	31 31	I T 09N R 02E I T 09N R 02E I T 09N R 02E I T 09N R 02E I T 09N R 02E	108 135	157 89.8 97.5 181.4		15 8.5 9 11	8.08 1 1 1	15 15 15 15	5.9 5 3.7	1193.94 1455.95 2068.02 1313.86		79.60 97.06 137.87 87.59
¹ Aquifer thickness (b) = static wa If well is perforated, b = depth c For short duration pump tests (a)	of perforations		0	fora	ted wells, b = 10	ft								Average	e 100.5



Case Narrative

On January 21, 2020, three water samples identified as "Horse Creek" were received by our laboratory for analysis. The chain of custody indicated the samples were to be analyzed for Specific Conductivity and Nitrate + Nitrite as N. The samples were received cool, intact and hand delivered.

Results are sumarized on the following page. Quality control data are available upon request.

Should you have any questions regarding this analysis feel free to give us a call at 449-6282

We appreciate the fact that you have chosen us as your analytical lab.

Sincerely yours,

D'S 29

Chris Erickson Laboratory Manager



Client: H & L Drilling

Date Reported: 22-Jan-20

Sample ID: Horse Creek TW1 Project ID: None Given Site ID: None Given

Chain of Custody #: 10971

Laboratory ID: 27A239 Sample Matrix: Water Date / Time Sampled: 21-Jan-20 @ 12:10 Date / Time Received: 22-Jan-20 @ 08:40

				Analyz	ed	Method Reference	
Parameter	AR	MCL	SCL	Date/Time	Ву		
Nitrate + Nitrite as N, mg/L	0.50	10	NR	22-Jan-20 @ 13:28	CE	EPA 300.0	
Specific Conductivity, umho/cm	522	NR	NR	22-Jan-20 @ 11:23	CE	EPA 120.1	

Comments:

 AR - Analytical Result
 NR - Not Regulated

 MCL - Maximum Contaminant Limit for Drinking Water Standards
 SCL - Secondary Contaminant Limit for Drinking Water Standards

References:

Methods for Chemical Analysis of Water and Wastes, US EPA, 600/4-79-020 Method 9223 B - QT, Colilert 18, Standard Methods for the Examination of Water and Wastewater.

Reviewed by: CE



Client: H & L Drilling

Date Reported: 22-Jan-20

Sample ID: Horse Creek TW2 Project ID: None Given Site ID: None Given

Laboratory ID: 27A240 Sample Matrix: Water Chain of Custody #: 10971

Date / Time Sampled: 21-Jan-20 @ 14:00 Date / Time Received: 22-Jan-20 @ 08:40

				Analyz	ed	Method	
Parameter	AR	MCL	SCL	Date/Time	Ву	Reference	
Nitrate + Nitrite as N, mg/L	1.30	10	NR	22-Jan-20 @ 13:39	CE	EPA 300.0	
Specific Conductivity, umho/cm	380	NR	NR	22-Jan-20 @ 11:23	CE	EPA 120.1	

Comments:

AR - Analytical ResultNR - Not RegulatedMCL - Maximum Contaminant Limit for Drinking Water StandardsSCL - Secondary Contaminant Limit for Drinking Water Standards

References:

Methods for Chemical Analysis of Water and Wastes, US EPA, 600/4-79-020 Method 9223 B - QT, Colilert 18, Standard Methods for the Examination of Water and Wastewater.

Reviewed by: CE



Client: H & L Drilling

Date Reported: 22-Jan-20

Sample ID: Horse Creek TW3 Project ID: None Given Site ID: None Given

Chain of Custody #: 10971

Laboratory ID: 27A241 Sample Matrix: Water Date / Time Sampled: 21-Jan-20 @ 15:30 Date / Time Received: 22-Jan-20 @ 08:40

				Analyz	ed	Method	
Parameter	AR	MCL	SCL	Date/Time	Ву	Reference	
Nitrate + Nitrite as N, mg/L	0.97	10	NR	22-Jan-20 @ 13:49	CE	EPA 300.0	
Specific Conductivity, umho/cm	607	NR	NR	22-Jan-20 @ 11:23	CE	EPA 120.1	

Comments:

AR - Analytical Result

NR - Not Regulated

MCL - Maximum Contaminant Limit for Drinking Water Standards

SCL - Secondary Contaminant Limit for Drinking Water Standards

References:

Methods for Chemical Analysis of Water and Wastes, US EPA, 600/4-79-020 Method 9223 B - QT, Colilert 18, Standard Methods for the Examination of Water and Wastewater.

Reviewed by: CE

								An	oendix 1	F									
					MONT		FPART						VTL						
										ANALY									
								_ •		/									
SITE NAM	E:				division	s 1-4													
COUNTY:		Broadv	vater co	ounty															
NOTES:																			
BY:	НТМ																		
DATE:	04/02/20				1														
					1														
Nitrate at e	nd of mixing	zone(s)	with no	cumula	tive effec	ts													
Variable	(K)	(I)	(D)	(L)	(Y)	(Ng)	(Nr)	(Ne)	(#I)	(QI)	(P)	(V)	(W)	(Am)	(As)	(Qg)	(Qr)	(Qe)	Nt
	Hydr.	Hydr.	Mix zone	Down grad.	Drain- field	Back- ground	Nitrate	Effluent Nitrate	# of single	Effluent per	Annual	Percent	Down- grad.	Mix zone	Mix. zone surface	Ground water	Recharge	Effluent	Resulting
	cond.	grad.	thick	distance	width	nitrate	precip	conc.	family	drain.	precip.	precip.	width	area	area	flow	flow	flow	nitrate (N)
LOT #	(ft/day)	(ft/ft)	(feet)	(feet)	(feet)	(mg/l)	(mg/l)	(mg/l)	homes	(ft3/day)	(in/yr)	recharge	(feet)	(ft²)	(ft²)	(ft3/day)	(ft3/day)	(ft3/day)	(mg/l)
Lot 16 of HCH Pr. 2	100.50	0.002	30.0	200	92.5	0.92	1.0	50.0	1.0	26.70	16.0	0.2	127.50	3825.00	25500.00	814.95	18.63	26.70	2.45
Lot 15 of HCH Pr. 2	100.50	0.002	30.0	200	80.3	2.02	1.0	50.0	1.0	26.70	16.0	0.2	115.30	3459.00	23060.00	736.97	16.85	26.70	3.64
2																			
LOT #	nd of mixing	zones w	lith cum	ulative	errects														
Lot 16 of HCH Pr.	100.50	0.002	30.0	466	92.5	0.92	1.0	50.0	1.0	26.70	16.0	0.2	174.05	5221.50	81107.30	1112.49	59.26	26.70	2.02
2 Lot 15 of HCH Pr.																			
2	100.50	0.002	30.0	200	80.3	2.02	1.0	50.0	1.0	26.70	0.00	0.00	115.30	3459.00	23060.00	736.97	0.00	26.70	3.70
0																			
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0																			
0																			
0					1	1												REV. 03/2	20005
NOTES:																			
	= fill in values			VOU															
Hydr. cond. =	= these cells	are calcu			c Conduct	vitv													
Hydr. grad. =			1	Hydraulio	c Gradient														
Mix zone thic											tant at 15 f		d of loot	-1.1	de en la el evile "		- # + -		
Down grad. o Drainfield wid			L Y				M 17.30.5 cular to Gre			a may also	De the dis	lance to en	iu or last n	nixing zone v	hen calculating	cumulative	ellects.		
Background	nitrate =		Ng	Backgrou	und Nitrate	e (as Nitro	gen) Conc	entration											
Nitrate in pre											t at 1.0 mg/		wal 1-: 10) for low-1 d					
Effluent Nitra # single fami) for level 1b) ijusted to equ	ual total effluent	from drainfie	eld)		
Effluent per o	drain. =		Q/	Quantity	of Effluen	t from drai	nfield (ave	rage rate	varies de	pending o	n number	of bedroom	is)	,			'		
Annual preci					ocal Precip			aug 147 -	or (et 0.0								
Down grad. v	ip recharge = width =		V W				narging Gro												
Mix zone are	a =		Am	Cross Se	ectional Ar	ea of Aqui	ifer Mixing				(<u>-/ · (· /</u>								
Mix zone sur					Area of Mi														
Ground wate Recharge flo			Qg Qr		Nater Flov		K)(I)(Am) P/12/365)('	0											
Effluent flow			Qr Qe		e Flow Rate			v)											
Resulting nit			Nt	Nitrate (a	as Nitroge	n) Concen	tration at E) + (Qr) + (Q					
	1			(or nitra	te concen	tration to u	use as bac	kground	nitrate for	next dowr	ngradient d	rainfield wh	nen detern	nining cumul	ative effects)				

Appendix Q

TRIGGER VALUE CALCULATION FOR ADJACENT TO SURFACE WATER DILUTION ANALYSIS

"An analysis of the effect of the proposed drainfield system on the quality of any adjacent surface water is required by ARM 17.36.312 and 17.30.715(1c). The increase in the nutrient concentration in the surface water cannot exceed the trigger value (T.V. of 0.01 mg/L nitrate and 0.001 mg/L phosphorous as set forth in Circular DEQ 7."

DILUTION EQUATION: (QD)(CD) + (QL)(CL) < T.V. = non-significant QD + QL

Note: Effluent flow rate (QD) must be multiplied by the number of drainfields in the subdivision.

NITRATE CALCULATION:

	40.00	
QD =	26.70	ft³/d
CD =		mg/L
QL =	301.00	ft³/s
CL =	0.00	mg/L

Number of drainfields in subdivision

Effluent flow rate from drainfield in cubic feet per day (commonly 200 gpd or 26.7 ft³/d for a 2 - 5 bedroom home) Nitrate concentration in mg/L (50 mg/L nitrate-N for standard drainfield, 24 mg/L for Level 2 wastewater treatment system) Flow rate in ft³/s into (or out of) surface water determined by stream gauge (usually the 14-day, 5-year low flow or 14Q5) Nitrate concentration (in mg/L) in surface water; can typically assume zero since increase, not total, is important

0.0020533 mg/L = final result, must be < 0.01 mg/L to be considered nonsignificant nitrate increase

PHOSPHOROUS CALCULATION:

	40	
QD =	26.7	
CD =	10.6	mg/L
QL =	301	ft³/s
CL =	0	mg/L

Number of drainfields in subdivision

Effluent flow rate from drainfield in cubic feet per day, (commonly 200 gpd or 26.7 ft³/d for a 2 - 5 bedroom home)

. Phosphorous concentration in mg/L (commonly 10.6 mg/L) in effluent

Flow rate in ft³/s into (or out of) surface water determined by stream gauge (usually the 14-day, 5-year low flow or 14Q5)

Phosphorous concentration (in mg/L) in surface water; can typically assume zero since increase, not total, is important

0.0004353 mg/L = final result, must be < 0.001 mg/L to be considered nonsignificant for phosphorous increase

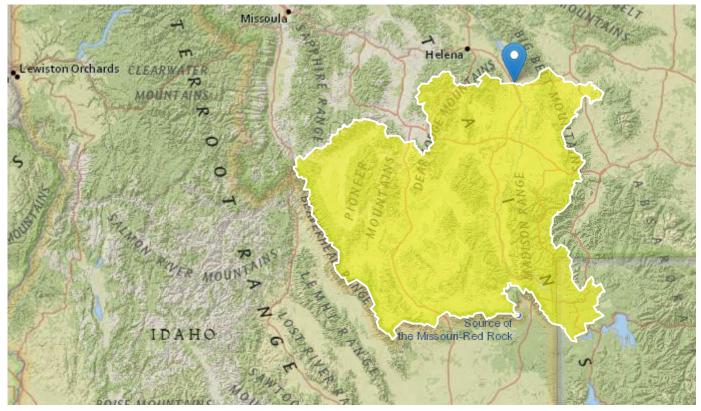
StreamStats Report for Horse Creek Hills Subdivision

 Region ID:
 MT

 Workspace ID:
 MT20200303215848128000

 Clicked Point (Latitude, Longitude):
 46.34053, -111.52323

 Time:
 2020-03-03 14:59:07 -0700



Basin Characteristics				
Parameter Code	Parameter Description	Value	Unit	
CONTDA	Area that contributes flow to a point on a stream	15294.7	square miles	
EL6000	Percent of area above 6000 ft	68.3	percent	
PRECIP	Mean Annual Precipitation	21.76	inches	
SLOP50_30M	Percent area with slopes greater than 50 percent from 30-meter DEM.	7.4	percent	

Peak-Flow Statistics Parameters [14 Percent (2210 square miles) UpYellow CentMount Region BasinC 2015 5019F]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
CONTDA	Contributing Drainage Area	15294.7	square miles	0.39	2040
EL6000	Percent above 6000 ft	68.3	percent	0	100

Peak-Flow Statistics Parameters [86 Percent (13100 square miles) SW Region BasinC 2015 5019F]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
CONTDA	Contributing Drainage Area	15294.7	square miles	0.42	2480
EL6000	Percent above 6000 ft	68.3	percent	0	100

Peak-Flow Statistics Disclaimers[14 Percent (2210 square miles) UpYellow CentMount Region BasinC 2015 5019F]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors

Peak-Flow Statistics Flow Report [14 Percent (2210 square miles) UpYellow CentMount Region BasinC 2015 5019F]

Statistic	Value	Unit
1.5 Year Peak Flood	21800	ft^3/s
2 Year Peak Flood	24400	ft^3/s
2 33 Year Peak Flood	25800	ft^3/s
5 Year Peak Flood	33600	ft^3/s
10 Year Peak Flood	41600	ft^3/s
25 Year Peak Flood	52200	ft^3/s
50 Year Peak Flood	59500	ft^3/s
100 Year Peak Flood	65800	ft^3/s
200 Year Peak Flood	72200	ft^3/s
500 Year Peak Flood	80300	ft^3/s

Peak-Flow Statistics Disclaimers[86 Percent (13100 square miles) SW Region BasinC 2015 5019F]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors

Peak-Flow Statistics Flow Report [86 Percent (13100 square miles) SW Region BasinC 2015 5019F]

StreamStats

StreamStat	5	
Statistic	Value	Unit
1.5 Year Peak Flood	27500	ft^3/s
2 Year Peak Flood	29000	ft^3/s
2 33 Year Peak Flood	29000	ft^3/s
5 Year Peak Flood	30800	ft^3/s
10 Year Peak Flood	32300	ft^3/s
25 Year Peak Flood	34400	ft^3/s
50 Year Peak Flood	35600	ft^3/s
100 Year Peak Flood	37100	ft^3/s
200 Year Peak Flood	38700	ft^3/s
500 Year Peak Flood	40700	ft^3/s
Peak-Flow Statistics Flow Reporting Averaged		
Peak-Flow Statistics Flow Report[Area-Averaged]		
Peak-Flow Statistics Flow Report[Area-Averaged] Statistic	Value	Unit
	Value 26700	Unit ft^3/s
Statistic		
Statistic 1.5 Year Peak Flood	26700	ft^3/s
Statistic 1.5 Year Peak Flood 2 Year Peak Flood	26700 28400	ft^3/s ft^3/s
Statistic1.5 Year Peak Flood2 Year Peak Flood2 33 Year Peak Flood	26700 28400 28600	ft^3/s ft^3/s ft^3/s
Statistic1.5 Year Peak Flood2 Year Peak Flood2 33 Year Peak Flood5 Year Peak Flood	26700 28400 28600 31200	ft^3/s ft^3/s ft^3/s ft^3/s
Statistic1.5 Year Peak Flood2 Year Peak Flood2 33 Year Peak Flood5 Year Peak Flood10 Year Peak Flood	26700 28400 28600 31200 33600	ft^3/s ft^3/s ft^3/s ft^3/s ft^3/s
Statistic1.5 Year Peak Flood2 Year Peak Flood2 33 Year Peak Flood5 Year Peak Flood10 Year Peak Flood25 Year Peak Flood	26700 28400 28600 31200 33600 36900	ft^3/s ft^3/s ft^3/s ft^3/s ft^3/s ft^3/s
Statistic1.5 Year Peak Flood2 Year Peak Flood2 33 Year Peak Flood5 Year Peak Flood10 Year Peak Flood25 Year Peak Flood50 Year Peak Flood	26700 28400 28600 31200 33600 36900 39000	ft^3/s ft^3/s ft^3/s ft^3/s ft^3/s ft^3/s ft^3/s

Peak-Flow Statistics Citations

Sando, Roy, Sando, S.K., McCarthy, P.M., and Dutton, D.M.,2016, Methods for estimating peak-flow frequencies at ungaged sites in Montana based on data through water year 2011: U.S. Geological Survey Scientific Investigations Report 2015-5019-F, 30 p. (https://doi.org/10.3133/sir20155019)

Low-Flow Statistics Parameters [14 Percent (2210 square miles) UpYellow CentMt Region LowFlow GLS 2015 50196]

StreamStats

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
CONTDA	Contributing Drainage Area	15294.7	square miles	28.1	2620
PRECIP	Mean Annual Precipitation	21.76	inches	16.4	38.9

Low-Flow Statistics Parameters [86 Percent (13100 square miles) SW Region LowFlow GLS 2015 5019G]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
CONTDA	Contributing Drainage Area	15294.7	square miles	24.4	2480
SLOP50_30M	Slopes_gt_50pct_from_30m_DEM	7.4	percent	0.96	22.6

Low-Flow Statistics Disclaimers[14 Percent (2210 square miles) UpYellow CentMt Region LowFlow GLS 2015 50196]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors

Low-Flow Statistics Flow Report [14 Percent (2210 square miles) UpYellow CentMt Region LowFlow GLS 2015 50196]

Statistic	Value	Unit
7 Day 10 Year Low Flow	240	ft^3/s

Low-Flow Statistics Disclaimers [86 Percent (13100 square miles) SW Region LowFlow GLS 2015 5019G]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors

Low-Flow Statistics Flow Report [86 Percent (13100 square miles) SW Region LowFlow GLS 2015 5019G]

Statistic	Value	Unit
7 Day 10 Year Low Flow	7910	ft^3/s
Low-Flow Statistics Flow Report[Area-Averaged]		
Statistic	Value	Unit
7 Day 10 Year Low Flow	6800	ft^3/s

Low-Flow Statistics Citations

McCarthy, P.M., Sando, Roy, Sando, S.K., and Dutton, D.M.,2016, Methods for estimating streamflow characteristics at ungaged sites in western Montana based on data through

water year 2009: U.S. Geological Survey Scientific Investigations Report 2015-5019-G, 19 p. (https://doi.org/10.3133/sir20155019)

Seasonal Flow Statistics Parameters[14 Percent (2210 square miles) UpYellow CentMt Region LowFlow GLS 2015 5019G]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
CONTDA	Contributing Drainage Area	15294.7	square miles	28.1	2620
PRECIP	Mean Annual Precipitation	21.76	inches	16.4	38.9

Seasonal Flow Statistics Parameters [86 Percent (13100 square miles) SW Region LowFlow GLS 2015 50196]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
CONTDA	Contributing Drainage Area	15294.7	square miles	24.4	2480
PRECIP	Mean Annual Precipitation	21.76	inches	16.7	37.1

Seasonal Flow Statistics Disclaimers[14 Percent (2210 square miles) UpYellow CentMt Region LowFlow GLS 2015 50196]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors

Seasonal Flow Statistics Flow Report [14 Percent (2210 square miles) UpYellow CentMt Region LowFlow GLS 2015 50196]

Statistic	Value	Unit
Jul_to_Oct_14_Day_5_Yr_Low_Flow	301	ft^3/s

Seasonal Flow Statistics Disclaimers [86 Percent (13100 square miles) SW Region LowFlow GLS 2015 50196]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors

Seasonal Flow Statistics Flow Report [86 Percent (13100 square miles) SW Region LowFlow GLS 2015 50196]

Statistic	Value	Unit
Jul_to_Oct_14_Day_5_Yr_Low_Flow	1030	ft^3/s
Seasonal Flow Statistics Flow Report[Area-Averaged]		
Statistic	Value	Unit
Jul_to_Oct_14_Day_5_Yr_Low_Flow	926	ft^3/s

Seasonal Flow Statistics Citations

McCarthy, P.M., Sando, Roy, Sando, S.K., and Dutton, D.M.,2016, Methods for estimating streamflow characteristics at ungaged sites in western Montana based on data through water year 2009: U.S. Geological Survey Scientific Investigations Report 2015–5019–G, 19 p. (https://doi.org/10.3133/sir20155019)

Annual Flow Statistics Parameters [14 Percent (2210 square miles) UpYellow CentMt Region Annual MeanDur 2015 50196]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
CONTDA	Contributing Drainage Area	15294.7	square miles	28.1	2620
PRECIP	Mean Annual Precipitation	21.76	inches	16.4	38.9

Annual Flow Statistics Parameters [86 Percent (13100 square miles) SW Region Annual MeanDur 2015 50196]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
CONTDA	Contributing Drainage Area	15294.7	square miles	24.4	2480
PRECIP	Mean Annual Precipitation	21.76	inches	16.7	37.1

Annual Flow Statistics Disclaimers[14 Percent (2210 square miles) UpYellow CentMt Region Annual MeanDur 2015 50196]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors

Annual Flow Statistics Flow Report [14 Percent (2210 square miles) UpYellow CentMt Region Annual MeanDur 2015 50196]

Statistic	Value	Unit
Median Annual Flow	2220	ft^3/s
Mean Annual Flow	3300	ft^3/s

Annual Flow Statistics Disclaimers [86 Percent (13100 square miles) SW Region Annual MeanDur 2015 5019G]

One or more of the parameters is outside the suggested range. Estimates were extrapolated with unknown errors

Annual Flow Statistics Flow Report [86 Percent (13100 square miles) SW Region Annual MeanDur 2015 50196]

Statistic	Value	Unit
Median Annual Flow	1230	ft^3/s
Mean Annual Flow	4280	ft^3/s

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StreamStats

Annual Flow Statistics Flow Report[Area-Averaged]

Statistic	Value	Unit
Median Annual Flow	1380	ft^3/s
Mean Annual Flow	4140	ft^3/s

Annual Flow Statistics Citations

McCarthy, P.M., Sando, Roy, Sando, S.K., and Dutton, D.M.,2016, Methods for estimating streamflow characteristics at ungaged sites in western Montana based on data through water year 2009: U.S. Geological Survey Scientific Investigations Report 2015–5019–G, 19 p. (https://doi.org/10.3133/sir20155019)

USGS Data Disclaimer: Unless otherwise stated, all data, metadata and related materials are considered to satisfy the quality standards relative to the purpose for which the data were collected. Although these data and associated metadata have been reviewed for accuracy and completeness and approved for release by the U.S. Geological Survey (USGS), no warranty expressed or implied is made regarding the display or utility of the data for other purposes, nor on all computer systems, nor shall the act of distribution constitute any such warranty.

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Application Version: 4.3.11

MONTANA DEPARTMENT OF ENVIRONMENTAL QUALITY PHOSPHOROUS BREAKTHROUGH ANALYSIS

Project:Horse Creek Hills Subdivisions 1-4Project Number:19-072Lot1 - 41Location:Broadwater County, Montana



VARIABLE	S DESCRIPTION	VALUE UNITS
_g	Length of Primary Drainfield as Measured Perpendicular to Ground	33.0 ft
	Water Flow	
	Length of Primary Drainfield's Long Axis	75.0 ft
/	Width of Primary Drainfield's Short Axis	23.0 ft
	Depth to Limiting Layer from Bottom of Drainfield Laterals*	<mark>9.0</mark> ft
	Distance from Drainfield to Surface Water	466 ft
	Phosphorous Mixing Depth in Ground Water (0.5 ft for coarse soils,	1.0 ft
е	1.0 ft for fine soils)**	
W	Soil Weight (usually constant)	100.0 lb/ft3
а	Phosphorous Adsorption Capacity of Soil (usually constant)	200.0 ppm
I	Number of Single Family Homes on the Drainfield	1.00
	re and a second s	
<u> </u>	Phosphorous Load per Single Family Home (constant)	6.44 lbs/yr
(Conversion Factor for ppm to percentage (constant)	1.0E+06
		1.02.00
Pt	Total Phosphorous Load = (PI)(#I)	6.44 lbs/yr
V1	Soil Weight under Drainfield = (L)(W)(B)(Sw)	1552500.0 lbs
V2	Soil Weight from Drainfield to Surface Water	3437915.0 lbs
	= [(Lg)(D) + (0.0875)(D)(D)](T)(Sw)	
	Total Phosphorous Adsorption by Soils = (W1 + W2)[(Pa)/(X)]	998.1 lbs
OLUTION		
вт	Breakthrough Time to Surface Water = P / Pt	<u>155.0</u> years
BY:		
ATE:	April 2, 2020	
OTES:	* Depth to limiting layer is typically based on depth to a limiting layer (such as clay,	
	bedrock or water) in a test pit or bottom of a dry test pit minus two feet to account for	
	burial depth of standard drainfield laterals.	
	** Material type is usually based on test pit. A soil that can be described as loam	

** Material type is usually based on test pit. A soil that can be described as loam (e.g. gravelly loam, sandy loam, etc.) or finer according to the USDA soil texture classification system is considered a "fine" soil.

REV. 12/2007

Appendix P

<u>`SUMMARY OF REQUIREMENTS FOR NONDEGRADATION "EXEMPTIONS" IN ARM 17.30.716</u> FISCAL YEAR 2015 VERSION⁽¹⁾

NOTE: This is not part of the official rule – it is an informational summary. To ensure compliance with all requirements of the rule, refer to the rule.

REQUIREMENTS	CATEGORY #1	CATEGORY #2	CATEGORY #3	CATEGORY #4 ⁽¹⁾	CATEGORY #5
General Requirements [ARM 17.30.716(2)(a)]					
Distance between absorption trench and impacted	≥1,000 feet (500 if	≥500 feet	≥500 feet	≥400 feet (200 if	≥1,000 feet (500 if
downgradient high-quality surface water	trench is pressure- dosed)			trench is pressure- dosed)	trench is pressure- dosed)
Perc rate ⁽²⁾ and soil requirement if absorption trench (AT) is not pressure-dosed (if AT is pressured-dosed, these requirements don't apply).	Perc. rate between 16 and 50 min/inch; AND 6 feet of VFS, SCL, CL, or SiCL soil	NOT APPLICABLE	NOT APPLICABLE	Perc. rate between 16 and 50 min/inch; AND 6 feet of VFS, SCL, CL, or SiCL soil	Perc. rate between 16 and 50 min/inch; AND 6 feet of VFS, SCL, CL, or SiCL soil
SWTS designed for ≤ 2 single-family residences, or non-industrial design flow ≤ 700 gal. per day	APPLICABLE	APPLICABLE	APPLICABLE	APPLICABLE	APPLICABLE
SWTS is on the lot being served and there is only one SWTS on the lot	APPLICABLE	APPLICABLE	APPLICABLE	APPLICABLE	APPLICABLE
SWTS meets current requirements in DEQ-4 and ARM 17.36 sub-chapter 3	APPLICABLE	APPLICABLE	APPLICABLE	APPLICABLE	APPLICABLE
Background nitrate concentration limit (does not apply to lots ≥20 acres when the absorption trench is greater than 500 feet from the downgradient property boundary)	<2 mg/L	<2 mg/L	<2 mg/L	<2 mg/L	<2 mg/L
Specific Requirements [ARM 17.30.716(2)(b)]	ARM 17.36.716(2)(b)(i)	ARM 17.36.716(2)(b)(ii)	ARM 17.36.716(2)(b)(iii)	ARM 17.36.716(2)(b)(iv)	ARM 17.36.716(2)(b)(v)
Lot size	≥2 acres	≥2 acres	≥1 acre	NOT APPLICABLE	≥2 acres
Percolation rate ⁽²⁾⁽³⁾	\geq 16 min/inch	\geq 6 min/inch	\geq 6 min/inch	NOT APPLICABLE	NOT APPLICABLE
Soil type required beneath the absorption trench (minimum thickness of 6 feet)	VFS, SCL or finer material	MS, SL or finer material	MS, SL or finer material	NOT APPLICABLE	NOT APPLICABLE
Depth to bedrock and ground water below ground surface	≥8 feet (<i>seasonally</i> high ground water)	≥12 feet (<i>seasonally</i> high ground water)	≥100 feet	NOT APPLICABLE	NOT APPLICABLE
Depth to limiting layer below ground surface	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	>6 feet
Pressure-dosing of absorption trench required	NOT APPLICABLE	APPLICABLE	APPLICABLE	NOT APPLICABLE	NOT APPLICABLE
Number of lots in subdivision	NOT APPLICABLE	NOT APPLICABLE	≤ 5	NOT APPLICABLE	NOT APPLICABLE
Distance from subdivision boundaries to any neighboring existing/approved SWTSs	NOT APPLICABLE	NOT APPLICABLE	≥ 500 feet	NOT APPLICABLE	NOT APPLICABLE
Number of subdivision lots created in the county over last 10 fiscal years	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	<150 ⁽⁴⁾	NOT APPLICABLE
Distance between lot and any town with a population > 500	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	>1 mile	NOT APPLICABLE
Depth of absorption trench below ground surface	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	≤18 inches
Level II SWTS required	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	NOT APPLICABLE	APPLICABLE
Well Setback [ARM 17.30.716(3)]					
Separation between a provisional mixing zone and any existing/approved drinking water supply well		≥100 feet	≥100 feet	≥100 feet	≥100 feet

S:

EVIATIONS:

SWTS =	SUBSURFACE WASTE
VFS =	VERY FINE SAND
SCL =	SANDY CLAY LOAM
CL =	CLAY LOAM
SiCL =	SILTY CLAY LOAM
MS =	MEDIUM SAND
SL =	SANDY LOAM

/2008

Requirements for category 4 include a maximum number of lots subdivided over previous 10 years. Therefore, this table will be updated at the beginning of each fiscal year. Percolation rates are only necessary when a percolation test has been conducted on the lot. If colation test has been conducted, the soil type will be used to determine compliance with the rule. The symbol "≥" indicates a percolation rate equal to or greater (i.e. slower) than the value

For fiscal year 2015, the counties that meet this requirement are: Big Horn, Blaine, Carter, au, Custer, Daniels, Dawson, Deer Lodge, Fallon, Garfield, Glacier, Golden Valley, Hill, Judith Liberty, McCone, Meagher, Musselshell, Petroleum, Phillips, Pondera, Powder River, Prairie, relt, Rosebud, Sheridan, Sweetgrass, Teton, Toole, Treasure, Wheatland, Wibaux.

STEWATER TREATMENT SYSTEM

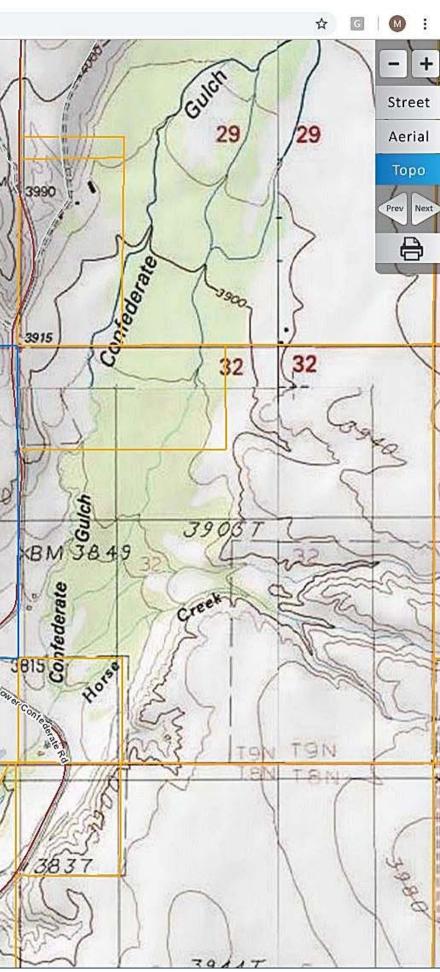
Appendix E

Existing Information

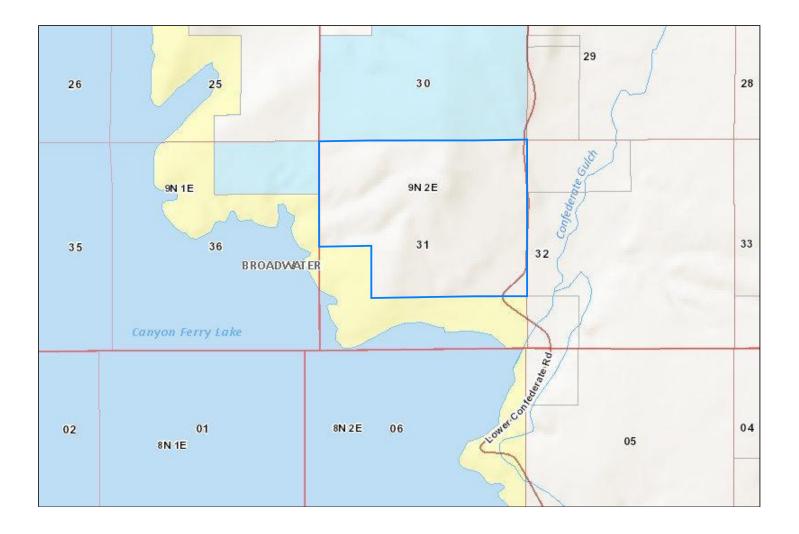
- Montana Cadastral Information
- Bureau of Land Management Survey
- DRAFT Horse Creek Hills Subdivision 2 Plat
- DRAFT Horse Creek Hills Subdivision 1-4 Plat
- DNRC Well Appropriations Letter
- DNRC Sage Grouse Habitat Inquiry
- FEMA Map Panel Index (Panel 3007C0225C)

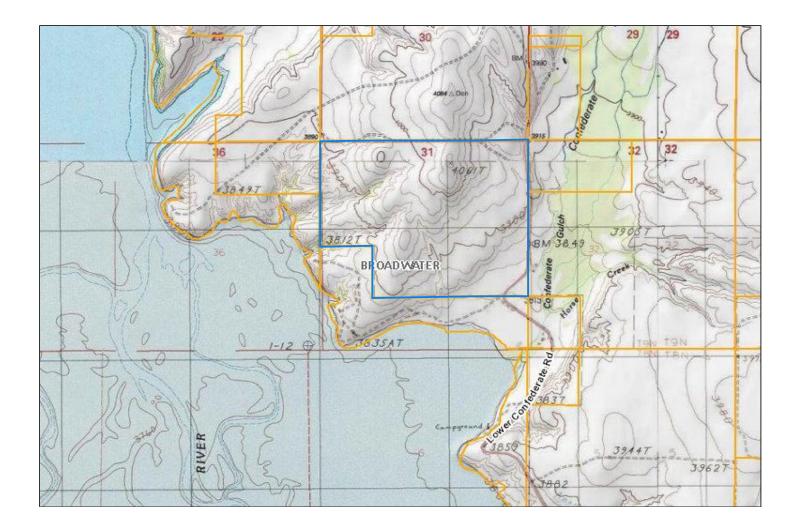
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	Property Record Card	× V A B B B B B C C C C C C C C C C C C C C
	Tax Year 2019 T	
Montana	Print	
Montana Cadastral		
Cauastral	Summary	
~		30
SEARCH	Primary Information	
	Property Category: RP Subcategory: Agricultural and Timber Properties	
曼 data	Geocode: 43-1792-31-1-01-01-0000 Assessment Code: 0007000251 Primary Owner: PropertyAddress:	PORT I WET I WIT
	71 RANCH LP	
—	40 71 RANCH RD COS Parcel:	
TOOLS	MARTINSDALE, MT 59053-8705	4084 △ Don
	NOTE: See the Owner tab for all owner information Certificate of Survey:	
LEGEND	Subdivision:	
	Legal Description:	
	S31, T09 N, R02 E, N2;N2SE4;NE4SW4	
	Last Modified: 4/14/2019 3:52:24 AM General Property Information	3890
	Neighborhood: 243.001 Property Type: VAC_R - Vacant Land - Rural	JAN GOLD PICON 31 ALLIN
	Living Units: 0 Levy District: 43-1050-70UT	L'astabello A STOUL
	Zoning: Ownership %: 100	Participation and a participation of the second sec
	Linked Property:	A DEFICE POLICIAN IN
	No linked properties exist for this property Exemptions:	
	No exemptions exist for this property	349T
	Condo Ownership:	A AND MARTERAL AND A
	General: 0 Limited: 0	
	Property Factors	BROADWATER A
	Topography: 8 Fronting: 0 - None	- Classification . My
	Utilities: 0 Parking Type: Access: 0 Parking Quantity:	38/21 0 8/11
	Location: 0 - Rural Land Parking Proximity:	
	Land Summary	
	Land Type Acres Value	
	Grazing 435.000 00.00	
	Fallow 0.000 00.00 Irrigated 0.000 00.00	
	Continuous Crop 0.000 00.00	S S S S S S S S S S S S S S S S S S S
	Wild Hay 0.000 00.00	
	Farmsite 0.000 00.00	
	ROW 0.000 00.00 NonQual Land 0.000 00.00	
	Total Ag Land 435.000 00.00	
	Total Forest Land 0.000 00.00	1-12 C 3835AT
	Total Market Land 0.000 00.00	V 1-12 P 00000 A1
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	Quiners	
	Owners	
	Appraisals	
	Market Land Info	
DISCLAUMED	Dwellings	
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~	Commercial	((Campground)
HELP	Ag/Forest Land	0 9/15 0.3mi
	Page 190	9 9.15 0.3mi
DEQP	aye rav	









Property Record Card

Summary

Property Category: RP Subcategory: Agricultural and Timber Properties Geocode: 43-1792-31-1-01-01-0000 Assessment Code: 0007000251 Primary Owner: PropertyAddress: 71 RANCH LP 40 71 RANCH RD 40 71 RANCH RD COS Parcel: MARTINSDALE, MT 59053-8705 NOTE: See the Owner tab for all owner information Certificate of Survey: Subclivision: Legal Description: S31, T09 N, R02 E, N2;N2SE4;NE4SW4 Last Modified: 4/14/2019 3:52:24 AM General Property Information Neighborhood: 243.001 Property Type: VAC_R - Vacant Land - Rural Living Units: 0 Levy District: 43-1050-70UT Zoning: Ownership %: 100 Linked Property: No linked properties exist for this property Exemptions: No exemptions exist for this property Condo Ownership: General: 0 Limited: 0 Eronting: 0 - None Property Factors Fronting: 0 - None Utilities: 0 Parking Type: Arease: 0 Parking Type:		
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Access: 0 Barking Quantity		
Access: 0 Parking Quantity:		
Location: 0 - Rural Land Parking Proximity:		
Land Summary		
Land Type <u>Acres</u> <u>Value</u>		
Grazing 435.000 00.00		
Fallow 0.000 00.00		
Irrigated 0.000 00.00		
Continuous Crop 0.000 00.00		
Wild Hay 0.000 00.00		
Farmsite 0.000 00.00		
ROW 0.000 00.00		
NonQual Land 0.000 00.00		
Total Ag Land 435.000 00.00		
Total Forest Land0.00000.00		
Total Market Land0.00000.00		
Deed Information: DEQ Page 194		

DEQ Page 194 http://svc.mt.gov/msl/MTCadastral/PrintPropertyRecordCard/GetPropertyRecordCardData?Geocode=43179231101010000&year=2019 Deed Date Book Page Recorded Date Document Number Document Type

Owners

Party #1			
Default Information:	71 RANCH LP		
	40 71 RANCH RD		
Ownership %:	100		
Primary Owner:	"Yes"		
Interest Type:	Conversion		
Last Modified:	12/8/2015 4:31:37 PM		
Other Names			Other Addresses
Name		Туре	

Appraisals

Appraisal History No data available for the parcel selected

Market Land

Market Land Info	
No market land info	exists for this parcel

Dwellings

Existing Dwellings

No dwellings exist for this parcel

Other Buildings/Improvements

Outbuilding/Yard Improvements

No other buildings or yard improvements exist for this parcel

Commercial

Existing Commercial Buildings

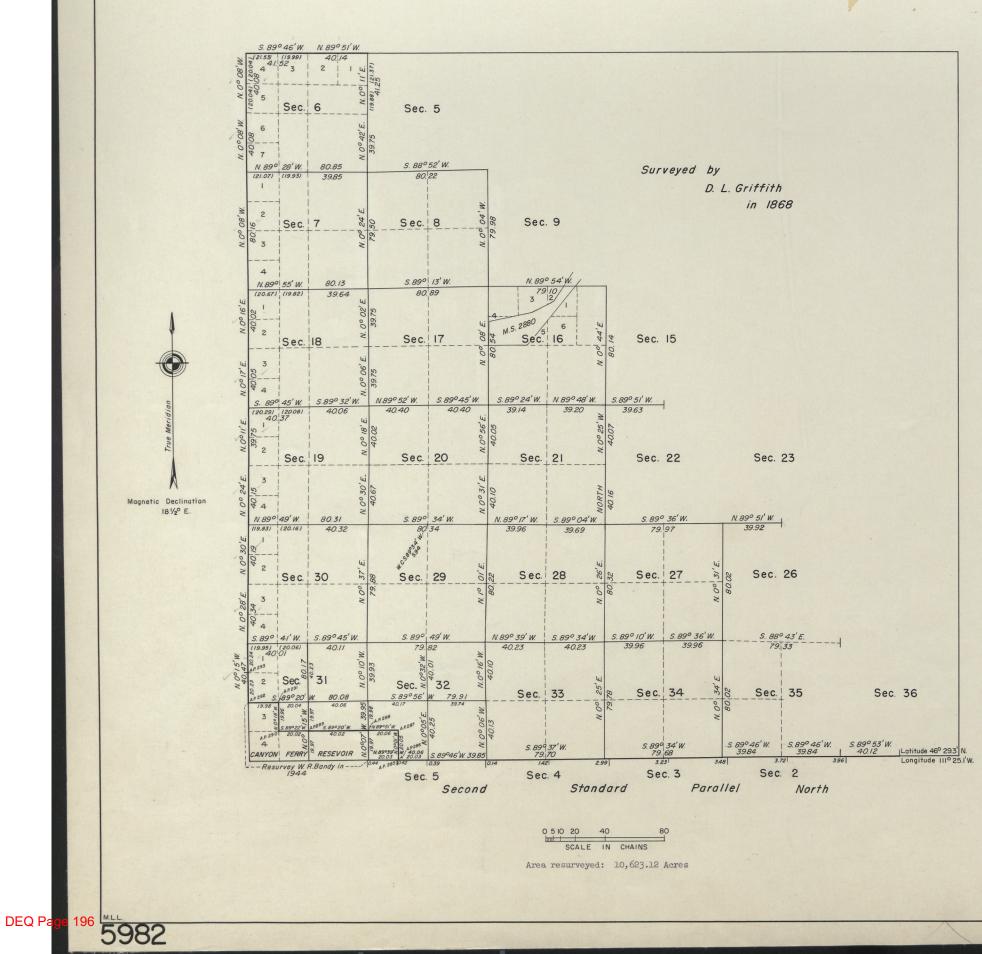
No commercial buildings exist for this parcel

Ag/Forest Land

Ag/Forest Land

No ag/forest land exists for this parcel

TOWNSHIP 9 NORTH, RANGE 2 EAST OF THE PRINCIPAL MERIDIAN, MONTANA DEPENDENT RESURVEY



The lottings and areas are as shown on the plat approved February 22, 1869. The history of previous surveys and resurveys is contained in the field note record. Portions of the north and west boundaries were resurveyed concurrently with this group.

These surveys were executed by Henry U. Lang, beginning July 12, 1961, and completed September 5, 1961, pur-suant to Special Instructions dated June 16, 1961, and Supplemental Special Instructions dated June 30, 1961, for Group No. 525, Montana.

This plat is strictly conformable to the approved field notes, and the survey, having been correctly ex-ecuted in accordance with the requirements of law and the regulations of this Bureau, is hereby accepted.

ORIGINAL

This plat represents a retracement and reestablishment of a portion of the Second Standard Parallel North through Range 2 East and a portion of the subdivision-al lines designed to restore the corners in their true original locations according to the best available evidence and the survey of a partial subdivision of sec-tions 31 and 32 and that portion of the Canyon Ferry Reservoir Boundary in Township 9 North, Range 2 East, Principal Meridian, Montana.

For topography of the area resurveyed, see U. S. Geo-logical Survey "Duck Creek Pass", "Townsend", and "Fort Logan" quadrangles.

UNITED STATES DEPARTMENT OF THE INTERIOR BUREAU OF LAND MANAGEMENT Washington, D. C. November 22, 1963

For the Director

Chief, Division of Engineering

.9N. R.2.E

PRELIMINARY PLAT MAP of HORSE CREEK HILLS 1 SUBDIVISION LOCATED IN SECTION 31. TOWNSHIP 9 NORTH, RANGE 2 EAST. PRINCIPAL MERIDIAN MONTANA, BROADWATER COUNTY, MONTANA OWNER: 71 RANCH LP PURPOSE: TO CREATE 12 TRACTS

CERTIFICATION OF DEDICATION

CONSENT OF MORTGAGEES

I/We, the undersigned property owner(s), do hereby certify that I/We have caused to be surveyed, subdivided and platted into lots, blocks, streets, alleys, as shown be the plat hereto annexed, the following described land in Broadwater County, to-wit:

LEGAL DESCRIPTION

A tract of land being the North One-Half, the North One-Half of the Southeast One -Quarter, and the Northeast One-Quarter of the Southwest One-Quarter of Section 31, Township 9 North, Range 2 East, Principal Meridian Montana, Broadwater County, Montana and being more particularly described as follows:

Beginning at the Northeast Corner of Section 31; thence South 01"19'49" West, a distance of 3,953.22 feet along the eastern section line of said Section 31 to a 1/16th Corner of Section 31; thence North 89'10'42" West, a distance of 2,641.57 feet along the eastern section line of said Section 31 to a

1/16th Corner of Section 31;

1/16th Corner of Section 31; thence North 89'09'25" West, a distance of 1,321.17 feet to a 1/16th Corner of Section 31; thence North 01'11'14" East, a distance of 1,317.54 feet to a 1/16th Corner of Section 31; thence North 01'14'10" East, a distance of 1,318.39 feet to the west One-Quarter Corner of Section 31; thence North 01'14'10" East, a distance of 1,3135.07 feet along the western section line of sid Section 31 to a 1/16th Comer of Section 31; thence North 0114'32" East, a distance of 1,335.42 feet along the western section line of said Section 31 to the

Northwest Section Corner of said Section 31; thence South 88'49'43" East, a distance of 2,640.43 feet along the northern section line of said Section 31 to the northern One-Quarter Corner of said Section 31; thence South 88'45'28" East, a distance of 2,647.88 feet along the northern section line of said Section 31 to the Northwest Section corner of said Section 31;

Said tract of land being 435 acres, along with and subject to any existing easements.

The above described tract of land is to be known and designated as HORSE CREEK HILLS 1 SUBDIVISION and the lands included in all streets, avenues, alleys, and parks or public squares shown on said plat are hereby granted and donated to the use of the public forever.

GRANT OF PUBLIC UTILITY EASEMENT

): ss

The undersigned hereby grants unto each and every person or firm, wheter public or privte, providing or offering to provide telephone, internet, electric power, gas, cable television, water or sewer service to the public, the right to the joint use of an easement for the construction, maintenance, repair and removal of their lines and other facilities in, over, under, and across each area designated on this plat as "Utility Easement" to have and to hold

CERTIFICATE OF WAIVER

I/We, the undersigned property owners of HORSE CREEK HILLS 1 SUBDIVISION do hereby waive the right to protest creation of a rural improvements district for improvements to Lower Confederate Road and the internal primary and secondary access subdivision roads. In so doing, we do not waive any right to protest, and/or appeal assessment formula which may be proposed if we believe it to be inequitable. This waiver shall be binding upon the heirs, assigns and purchasers of all tracts within this subdivision.

__, 20 Dated this _____ day of ____

State of Montana)

County of Gallatin

On this _____ day of _____, 20____, before me, the undersigned, a Natary Public for the State of ______, personally appeared ______, known to me to be the ______ of the Corporation executed the within instrument, and acknowledged to me that such Corporation executed the same. IN WINESS WHEREOF, I have hereunto set my hand and affixed my Notarial Seal the day and year first above written.

Notary	Public	for	the	State	of	
(Printe	d Nam	e)				
Residin	a at					

Residing at		,	
My commission	expires		

CERTIFICATION OF COMPLETION OF IMPROVEMENTS

I, 71 Ranch LP, and I, Mark Fasting, a registered professional engineer licensed to practice in the State of Montana hereby certify that the public improvements, required as a condition of approval of HORSE CREEK HILLS 1 SUBDIVISION, have been installed in conformance with the approved specifications and plans, or have been bonded concerdent to the instrumentation and plans. according to the improvements agreement.

71 Ranch LP

___, 20____ (Date)

Mark A. Fastina, P.E. Montana Registration No. 12071PE

____, 20____ (Date)

We, the undersigned mortgagees, do hereby join in and consent to the described plat, releasing our respective liens, claims or encumbrances as to any portion of said lands now being platted into roads, avenues, parks or other public uses and dedicated to the use of the public forever.

____, 20____ DATED this _____ day of _____

Lending Institution

BY:

State of Montana)

): ss County of Gallatin)

On this _____ day of _____, 20____, before me, the undersigned, a Notary Public for the State of ______, personally appeared ______, known to me to be the ______, of the Corporation executed the within instrument, and acknowledged to me that such

Corporation executed the same. IN WITNESS WHEREOF, I have hereunto set my hand and affixed my Notarial Seal the day and year first above

Notary Public for the State of _____ (Printed Name) Residing at _____ My commission expires _____

CERTIFICATE OF COUNTY COMMISSIONERS

I, the Chairman of the Board of County Commissioners, Gallatin County, Montana, do hereby certify that the accompanying plat has been duly examined and have found the same to conform to the law, approve it, and hereby accept the dedication to public use.

DATED this _____ day of _____

Chairman, Board of County Commissioners

CERTIFICATE OF COUNTY TREASURER

I, _______Treasurer of Broadwater County, Montana, pursuant to Section 76-3-611(1)(b) MCA, that all real property taxes assessed and levied on the land described below encompassed by the proposed HORSE CREEK HILLS 1 SUBDIVISION have been paid.

DATED this _____ day of _____, 20_____,

Treasurer of Gallatin County

CERTIFICATE OF CLERK AND RECORDER

I, _____, Clerk and Recorder of Broadwater County, Montana, do hereby certify that the foregoing instrument was filed in my office at ______ o'clock (AM or PM) this _____ day of ______ and recorded as HORSE CREEK HILLS 1 SUBDIVISION, Records of the Clerk and Recorder, Broadwater County, Montana.

Clerk and Recorder

CERTIFICATE OF SURVEYOR

I, the undersigned, Gregory L. Finck, a Professional Land Surveyor, do hereby certify that I have performed the survey shown on the attached plat of HORSE CREEK HILLS 1 SUBDIVISION; that such survey was made on ______ 20____; that said survey is true and complete as shown and that the monuments found and set are of the character and occupy the positions shown thereon.

Dated this _____ day of _____ _____, 20_____

Gregory L. Finck, P.L.S. Montana Registration No. 13174 LS



VICINITY MAP





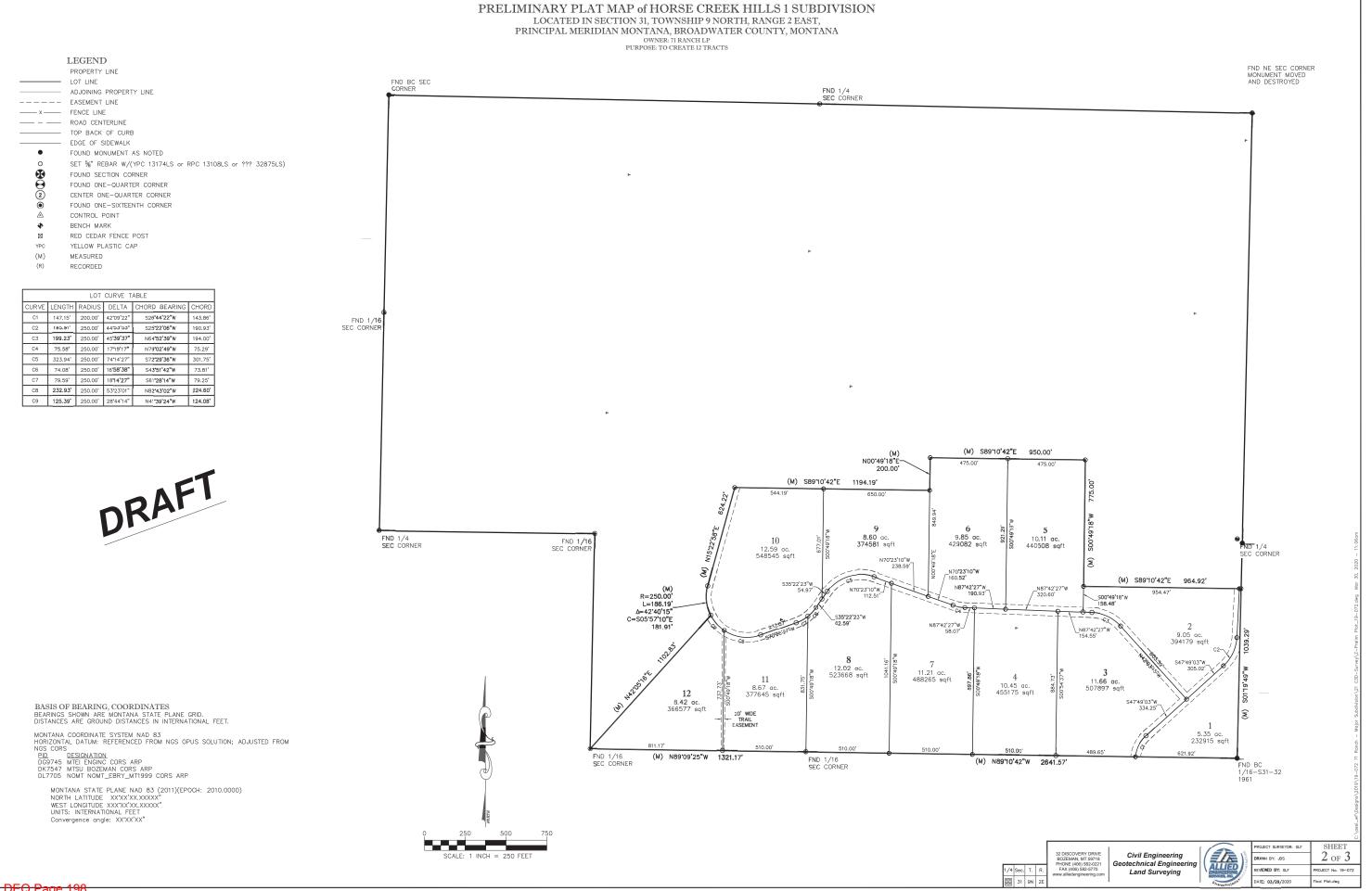
MAN, MT 59718 PHONE (406) 582-022 FAX (406) 582-5770

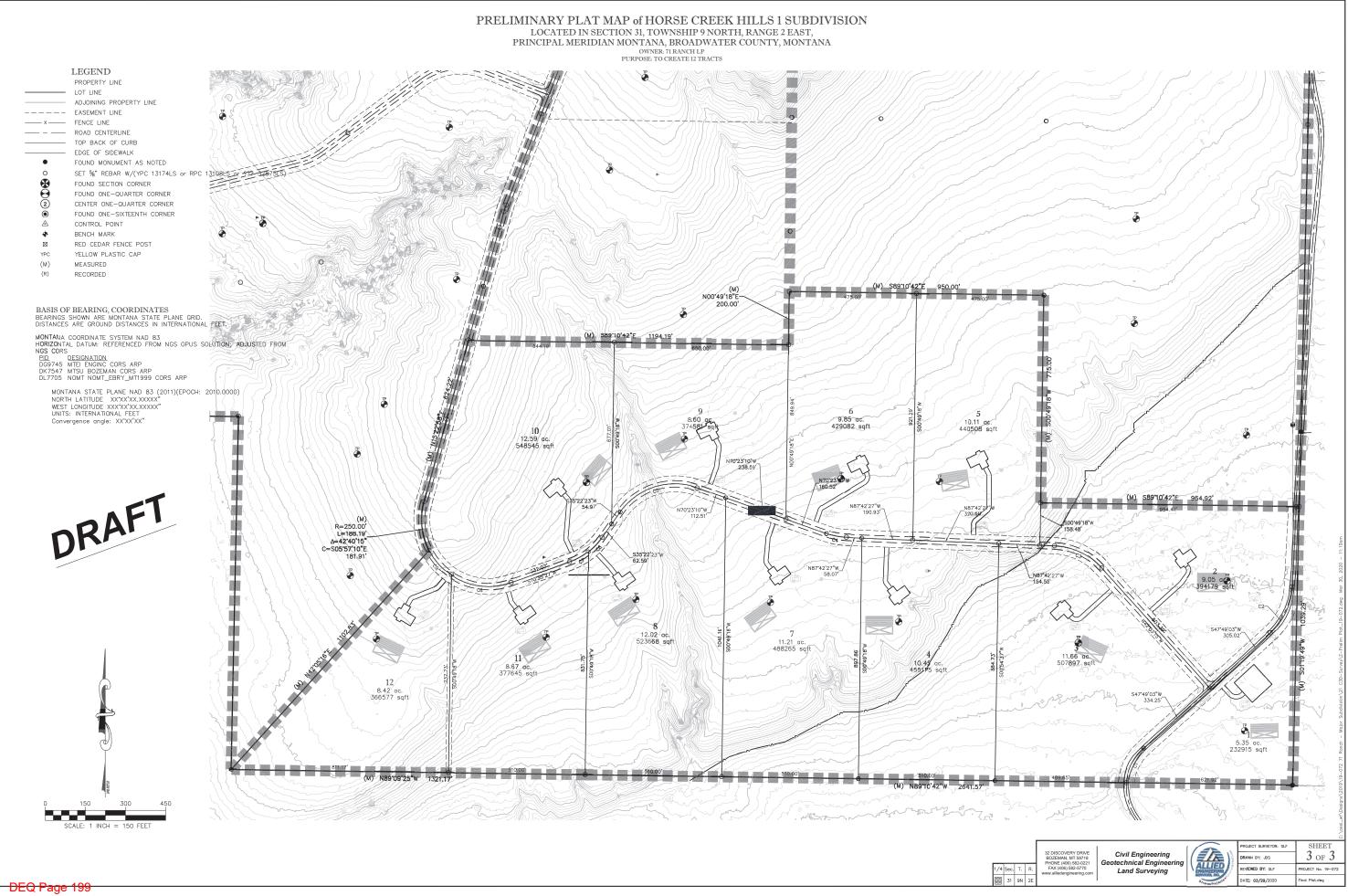
Civil Engineering Geotechnical Engineering Land Surveying



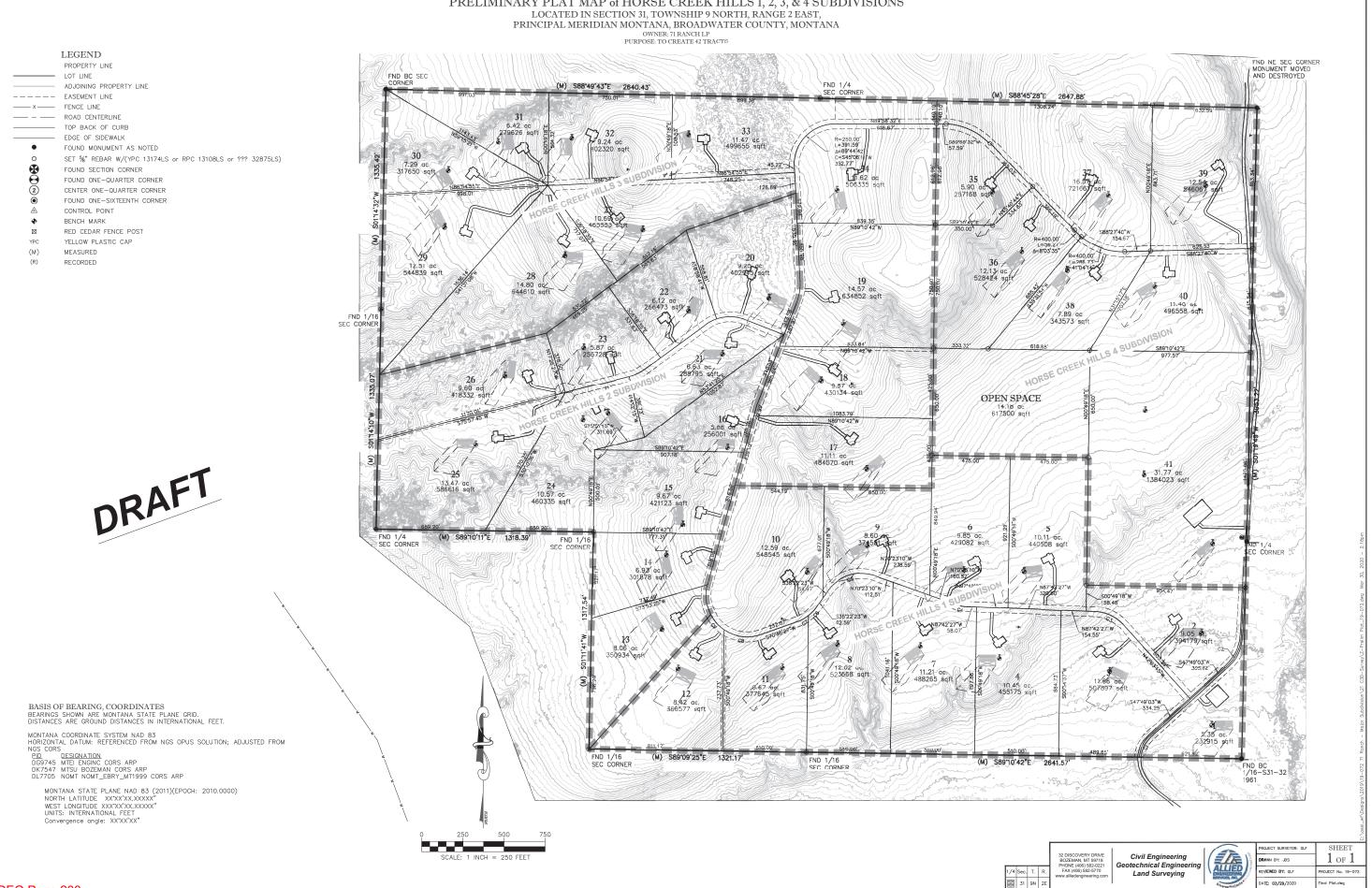
PROJECT SURVEYOR: GLF SHEET DRAWN BY: JDS 2 of 3 REVIEWED BY: GLF PROJECT No. 19-072 DATE: 03/29/2020 l Plat.dwg

LOCATED IN SECTION 31, TOWNSHIP 9 NORTH, RANGE 2 EAST, PRINCIPAL MERIDIAN MONTANA, BROADWATER COUNTY, MONTANA OWNER: 71 RANCH LP PURPOSE: TO CREATE 12 TRACTS





PRELIMINARY PLAT MAP of HORSE CREEK HILLS 1, 2, 3, & 4 SUBDIVISIONS LOCATED IN SECTION 31, TOWNSHIP 9 NORTH, RANGE 2 EAST, PRINCIPAL MERIDIAN MONTANA, BROADWATER COUNTY, MONTANA



DEPARTMENT OF NATURAL RESOURCES AND CONSERVATION Water Resources Division



STEVE BULLOCK

PHONE: (406) 444-6999 FAX: (406) 444-9317 http://www.dnrc.mt.gov

1424 9TH AVENUE PO BOX 201601 HELENA, MONTANA 59620-1601

February 4, 2020

Hunter Morrical Allied Engineering Services, Inc. 32 Discovery Dr. Bozeman, MT 59718

Re: Horse Creek Hills Subdivision, Phase 1, Broadwater County, HRO 20-4

Dear Mr. Morrical:

The purpose of this letter is to respond to your request for DNRC review of water right permit exceptions under MCA 85-2-306(3)(a)(iii) for the proposed DEQ review in accordance with ARM 17.36.103(1)(s). The proposed project is to split an existing ±435-acre tract, into individual lots in four phases. The project is located in Section 31, T9N, R2E, Broadwater County. The proposed project for Phase 1 is for one domestic dwelling each on eleven lots (0.28 AF x 11 lots = **3.08 AF**) and one commercial lot with water usage estimated to be **0.35 AF** (see submitted calculations). Lawn and garden irrigation would be approximately 0.219 acres on each lot (0.219 acres x 12 lots = 2.62 acres x 2.5 AF/season = **6.57 AF**). The total combined volumetric use for the proposed ten lot project is 10 AF.

Based on the information received January 31, 2020, the proposed appropriation does fit the current rules and laws pertaining to the filing of an exempt water right using a DNRC Form 602, Notice of Completion of Groundwater Development. The proposed appropriation is considered a combined appropriation because the proposed split of the 435 acre tract has not been approved or recorded with Broadwater County prior to October 17, 2014. As noted on Form 602, the appropriations combined, will not exceed a flow rate of 35 GPM or an annual volume of 10 AF in combination, or a water right permit must be applied for on DNRC Form 600, prior to putting the water to a beneficial use. DNRC Form 602, Notice of Completion of Groundwater Development, is to be filed within 60 days of the water being put to a beneficial use.

In <u>Clark Fork Coalition, et. al. v. DNRC, et. al.</u>, 2016 MT 229, 384 Mont. 503, 380 P.3d 771, the Montana Supreme Court concluded that the definition of "combined appropriation" in Admin. R. Mont. 36.12.101(13) was invalid. The Court reinstated the Department's 1987 Rule defining "combined appropriation" as: "An appropriation of water from the same source aquifer by means of two or more

groundwater developments, the purpose of which, in the department's judgment, could have been accomplished by a single appropriation. Groundwater developments need not be physically connected nor have a common distribution system to be considered a "combined appropriation." They can be separate developed springs or wells to separate parts of a project or development. Such wells and springs need not be developed simultaneously. They can be developed gradually or in increments. The amount of water appropriated from the entire project or development from these groundwater developments in the same source aquifer is the "combined appropriation."

Under this Rule, the Department interprets subdivisions that are pending before the Department of Environmental Quality for approval on October 17, 2014 or filed after that date to be a single project that can be accomplished by a single appropriation. Consequently all wells in such a subdivision will be considered a "combined appropriation" for the purposes of Mont. Code Ann. 85-2-306. The only exception to this interpretation is that a subdivision which has received preliminary plat approval prior to October 17, 2014 will not be considered a project under the "combined appropriation" 1987 Rule; individual lots will still be evaluated under the 1987 Rule at the time of an application to the Department. 2015 Mont. Laws § 1, Ch. 221.

This letter does not serve as a pre-approval for a water right nor does it provide a pre-approval to utilize up to 10 AF of water in the future. This letter only evaluates the amount of water proposed under the current project.

Thank you,

Sustern Wofford Kristeen Wofford

DNRC Water Resources Helena Regional Office

Cc: DEQ, Leata English via email

Montana Sage Grouse Habitat Conservation Map

Use this map to view and explore types of sage grouse habitat designated as core (blue), general (green), connectivity (light-blue) habitats or BLM priority areas. To zoom into an area, hold the Shift key and draw a rectangle. Anyone proposing new activities in sage grouse habitat must submit a project application for consultation.

If your project is close to designated sage grouse habitat or BLM Priority area, or if you are unsure your project is within designated sage grouse habitat or BLM Priority area, please submit your project for review as permitting agencies will be checking to see if your project is located within these designated sage grouse habitats. If your permitting agency requires evidence that your project is outside of designated sage grouse habitat, we recommend that you log in and start a project application and take a screenshot of your project's location.



NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The **community map repository** should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Siliwater Elevations tables contained within the Flood Insurance Study (FIS) Report that accompanies this FIRM. Users should be aware that BFEs are intended for flood insurance rating purposes only and should not used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS Report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Sullwater Elevations table in the Flood Insurance Study Report for this jurisdiction. Elevations shown in the Summary of Sullwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study Report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study Report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercafor (UTM) zone 12. The horizontal datum was NAD 83, GRS 1980 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slipht positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey vebsite at <u>http://www.nss.noaa.gov</u> or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, Maryland 20910-3282 (301) 713-3242

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713- 3242, or visit its website at <u>http://www.ngs.noaa.gov</u>.

Base map information shown on this FIRM was derived from NAIP Orthophotograph produced with a one meter ground resolution from photography dated 2009.

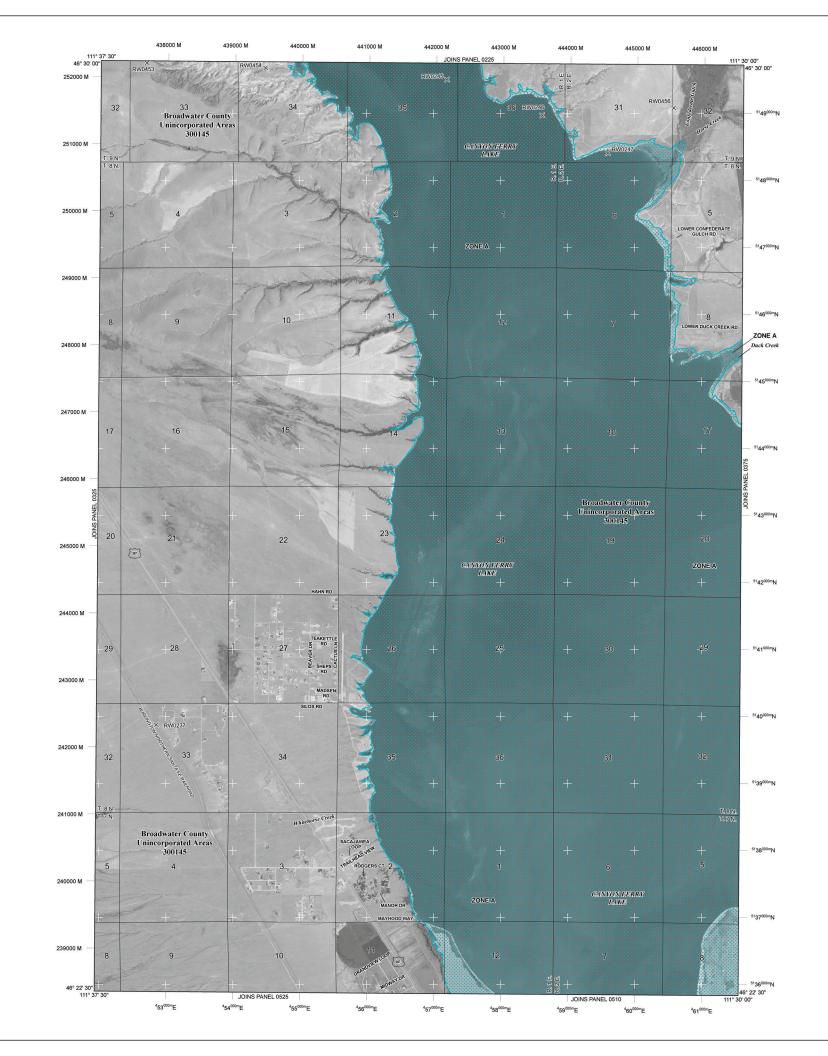
This map reflects more detailed and up-to-date **stream channel configurations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables for multiple streams in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

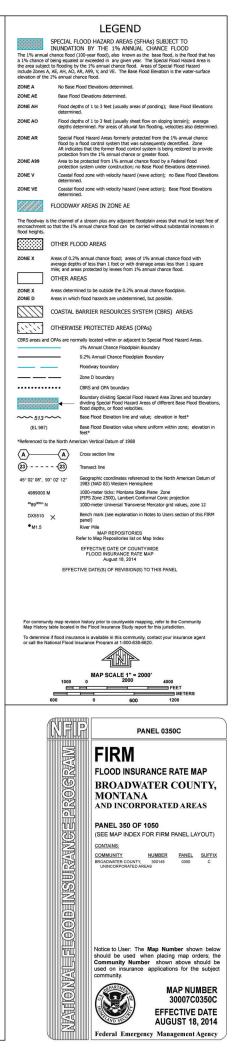
Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flock Insurance Program dates for each community as well as a listing of the panels on which each community is located.

For information on available products associated with this FIRM visit the Map Service Center (MSC) website at <u>http://mscfema.gov</u>, Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. Many of these products can be ordered or obtained directly from the MSC website.

If you have **questions about this map**, how to order products, or the National Flood Insurance Program in general, please call the **FEMA Map Information exchange (FMIX) at 1477-FEMA-MAP** (1-877-362-2627) or visit the FEMA website at <u>http://www.fema.gov/business/nfip</u>.





BROADWATER COUNTY Blanning Department Office 406-266-9211 Fax 406-266-3674 515 BROADWAY TOWNSEND, MONTANA 59644

March 23, 2020

Hunter Morrical, E.I. Allied Engineering 32 Discovery Drive Bozeman, MT 59718

Dear Mr. Morrical:

Per your request, WWC Engineering (Broadwater County Contract Floodplain Administrator) has completed a review to determine if the proposed subdivision to be constructed is within the FEMA designated floodplain. The proposed subdivision is located on a parcel owned by the 71 Ranch LP, with a parcel ID #43179231101010000, in the N 1/2, Section 31, Township 9 North, Range 2 East. Per our review, the proposed subdivision does not require a floodplain permit from Broadwater County. If you have any questions or need additional information please do not hesitate to contact us.

Sincerely,

Gary Vert, P.E., CFM Broadwater County Floodplain Administrator (406) 443-3962 Office gvert@wwcengineering.com

Appendix F

Storm Drainage Calculations

- Storm Drainage Report Horse Creek Hills 1-4 Subdivisions
- Storm Drainage Plans
- Storm Drainage Maintenance Plan

Storm Drainage Report:

Horse Creek Hills Subdivisions 1,2,3, & 4 Broadwater County, MT



Project #19-072

April, 2020

Prepared By:

Allied Engineering Services, Inc.



Horse Creek Hills Subdivisions 1-4 Storm Drainage Report April 2020

INTRODUCTION

This report presents the necessary information for MDEQ Subdivision review required per Circular MDEQ-8. Located off Lower Confederate Road, the project is just east of Canyon Ferry Reservoir. The project is to subdivide a single lot into 39 residential lots and two commercial lots. Horse Creek Hills Subdivision #1 will consist of 11 residential lots and 1 commercial lot. Horse Creek Hills Subdivision #2 will consist of 11 residential lots. Horse Creek Hills Subdivision #3 will consist of 11 residential lots. Horse Creek Hills Subdivision #4 will consist of 6 residential lots and 1 commercial lot. All residential and commercial lots will be served by on-site wastewater and water. This report has been addressed to encompass all four subdivisions within the overall development. The overall stormwater management plan for the development is to ensure that all increased runoff from the 2-year, 24-hour storm due to road and infrastructure is captured before it leaves the property. Additionally, the development is designed so that existing runoff patterns will be maintained. Stormwater conveyance structures have been designed to convey the 10-year, 24-hour event without roads and driveways being overtopped. Finally, the 100-year, 24-hour event will not inundate homes and drainfields due to the existing topography of the site and the strategic placement of homes and drainfields.

Existing conditions at the site are native grassland range that has been historically used for grazing purposes. Additionally, there are dry wash gullies on the site that hold true to existing drainage patterns. General topography of the site can be seen on the storm drainage plans included in Appendix 4 (F). The site has slopes that range from 1-75% in some areas. Slopes generally drain towards dry wash gullies that ultimately go in the direction of Canyon Ferry Reservoir. Soils for the site are primarily labeled by the NRCS as hydrologic soil group B. Group B soils have moderately low runoff potential when saturated. This is true for the existing topsoil layer on-site, which varies in thickness from 0 to 6 inches. During the site investigation, silty loam with high infiltration capabilities where found below the topsoil layer. This soil profile is common amongst the test pits excavated within the subdivision. Overall, 43 test pits were excavated within the development – all confirming the above.

The essential storm drainage management plan is for ten retention facilities to be constructed throughout the site to account for the increase in runoff due to road and utility construction only. All individual lot owners will also need to construct a generically sized retention pond and place it on the downstream side of their development to retain the excess stormwater runoff due to home and driveway construction.

PRE-DEVEOPMENT HYDROLOGY

The peak flows and volumes for the required storm events were computed using the MDEQ spreadsheets for DEQ-8 Standard Plans. Additionally, the DEQ-8 IDF spreadsheet was used for calculating intensity data and for sizing on-site culverts. The existing ground was classified as undeveloped area since it has been used for grazing purposes historically. In addition to site visits an aerial drone survey was performed on the site that is included to show pre-development land use conditions. Post development land use will include residential lots, commercial lots, roads, storm ponds, and open space lots. The open space is assumed to have native grasses maintained and will require minimal irrigation to remain established. Rational Method Coefficients for the different land uses are estimated below.

Land Use	Coefficient (C)
Paved/hard Surfaces	0.90
Gravel Surfaces	0.80
Lawn/Landscaping	0.10
Unimproved Areas	0.20

Table 1 – Rational Method Co-Efficient (C)

Horse Creek Hills Subdivisions 1-4 Storm Drainage Report April 2020

Pre-development basins were delineated into seven (7) different basins labeled Drainage Basin 1, 2, 3, 4, 5, 6, and 7. The drainage basins Existing 6 and 7 are both basins that have off-site drainage that has been accounted for. Existing drainage basins have historical runoff patterns and directions that will not be altered by this development. The overall layout of the drainage basins is shown on page WW2.0 (see Appendix 4). The development generally will not alter existing drainage paths or patterns; thus the post development basins were analyzed to be the same as the pre-development basins.

Drainage Basin	Primary Land Use	Primary Land Use Area (acre)	
Existing 1	Undeveloped Land	61.10	0.20
Existing 2	Undeveloped Land	60.50	0.20
Existing 3	Undeveloped Land	70.00	0.20
Existing 4	Undeveloped Land	79.70	0.20
Existing 5	Undeveloped Land	90.40	0.20
Existing 6	Undeveloped Land	76.30	0.20
Existing 7	Undeveloped Land	87.60	0.20

Table 2 – Pre-Development Drainage Basins

Drainage Basin	Design Storm	Peak Run-Off (cfs)	Volume (Cu. Ft.)
DB 1	2-YR 24-HR	4.19	55,004
DB 2	2-YR 24-HR	4.15	54,465
DB 3	2-YR 24-HR	4.79	62,830
DB 4	2-YR 24-HR	5.46	71,713
DB 5	2-YR 24-HR	6.20	83,346
DB 6	2-YR 24-HR	5.23	68,688
DB 7	2-YR 24-HR	6.00	78,877

All analysis was performed using MDEQ spreadsheets available online. The IDF curve used to calculate intensities for peak runoff was found using the IDF spreadsheet from MDEQ. The intensity values used for calculating required retention pond volumes were found in Appendix A from DEQ-8 Circular.

POST-DEVELOPMENT HYDROLOGY

Post-Development conditions for the four proposed subdivisions are going to be residential lots between 5 to 15 acres in size, as well as two commercial lots between 5 and 32 acres in size. The site has been designed so that increased runoff due to road construction will be retained on site and that existing drainage basins are not altered. Run-off will be captured by roadside swales and channelized ten different ponds throughout the site – as seen in the Stormwater plans in Appendix 4. Ponds will generally overtop during events larger than the 2-year, 24-hour event and runoff will flow into existing drainage paths without inundating houses or drainfields. Soil types on the site are primarily Fine Sandy Loam, loam, or coarser, thus infiltration in the ponds can be expected to be 0.7 inches per hour – per DEQ Circular 8. After 72 hours, infiltration levels can be expected to be 4.2 feet or greater. Because the max depth of each

retention pond is 3-ft, infiltration should ensure that stormwater is not retained in the retention ponds for longer than 72 hours. Evaporation was not considered to contribute to stormwater loss after storm events.

Post-Development 10-YR, 24-HR peak flow rates for culvert sizing were calculated using the MDEQ IDF spreadsheet calculations attached in Appendix 3. All culverts and swales on site were designed to convey the flow rates calculated. Many culverts and most of the swales on the property will be able to convey the 100-year, 24-hour event as these structures were oversized to account for snow melt potential in conjunction with frozen ground. According to MDEQ-8 standard plan requirements the controlling factor for storm water treatment is now the Initial Storm Water Facility (ISWF) volume. The ISWF for all drainage basins did not exceed they increased runoff volume from the rational method calculation. To satisfy the Standard Plan the 10-YR 24-HR event will be evaluated to make sure roadways and driveways are not overtopped. Also, a general narrative and calculations will be given to demonstrate that drainfields and buildings are not flooded during the 100-YR 24-HR storm.

Drainage Basin	Design Storm	Peak Run-Off (cfs)	Volume (Cu. Ft.)	Increased Volume (Cu. Ft.)
DB 1	2-YR 24-HR	4.19	55,004	0
DB 2	2-YR 24-HR	4.71	61,869	7,404
DB 3	2-YR 24-HR	5.15	67,567	4,738
DB 4	2-YR 24-HR	6.21	81,584	9,871
DB 5	2-YR 24-HR	6.89	90,454	9,108
DB 6	2-YR 24-HR	5.23	68,688	0
DB 7	2-YR 24-HR	6.51	85,432	6,555

 Table 4 - Post-Development Total Run-Off Values

The total drainage basin area evaluated is 525.6 acres. Of this area, 435 acres is on-site drainage area, and 90.6 acres is offsite drainage area. A total of 12 acres of impervious area will be added due to road infrastructure. It was conservatively assumed that the roads will be paved for the post development runoff calculations. This volume does not include the impervious area on the residential lots, as residential and commercial lots will be responsible to retain the excess stormwater in individual retention ponds. See below for description of individual lot impervious area run-off capture pond sizing.

Typical Residential Lot Pond Sizing

As described above each lot will be required to capture the first half inch run-off from all impervious area, or the amount of excess stormwater generated during the 2-year, 24-hour event. To estimate the pond size needed for these lots, a typical residential lot was analyzed as having a 3,500-sf house footprint and a 600-ft long driveway being 16-ft wide. Additionally, no lawn/landscaping area was accounted for, as many of the lots will consist of zero scaping given the location. For the commercial lots, the same pond has been shown for conceptual purposes; however, if impervious area for the commercial lots is expected to exceed 13,100-sf, the lot owner will be responsible to size and build a larger retention facility. See table below for the typical lot layout with estimates for proposed driveway area and building size.

Table 5 - Typical Residential Lot Layout

Land Use	Area (sq. ft.)	Coefficient
Driveway	9,600	0.9
House	3,500	0.9

A typical lot will have a total impervious area of 13,100 Sq. Ft. To capture the 2-year, 24-hour stormwater volume of 948 cu. ft. The volume of the first half inch of stormwater is 546 cu. ft., thus the stormwater pond size is enough. Assuming 3:1 side slope and 2.0 feet deep the pond will have a total footprint of 16-ft by 31-ft. The total volume of this pond will hold cu. ft. Each lot owner will need to construct this pond on the downstream side of there lot and grade drainage from the impervious areas to drain to it.

Basin	Land Use	Area (sq. ft.)	Volume Required (cu. Ft.)
All Subdivision Roads	Impervious Area	522,720	37,676
Individual Lots	Impervious Area	13,100	948

 Table 6 – Summary of Initial Storm Water Facilities Required

POST-DEVELOPMENT HYDRAULICS

The project storm ponds are designed to retain the stormwater increase from the 2-year, 24 hour storm event. Utilizing a linear pond configuration, the ponds will have a trapezoidal shape with 3:1 side slopes. Once full, the ponds will overtop and flow into existing drainage paths without inundating roads, homes, or drainfields.

1 able 7 = Ketention 1 onus			- I I		
Pond	Drainage Basin	Top Dimensions (Length x Width)	Pond Depth (ft.)	Storage Volume (Cu. Ft.)	Side Slopes (H:V)
Strawberry Roan Trail Pond – Sta. 92+00	DB-1 & DB-2	39 ft x 79 ft	2.75	8,293	3:1
Strawberry Roan Trail Pond – Sta. 68+00	DB-3	34 ft x 59 ft	2.75	5,389	3:1
Strawberry Roan Trail Pond – Sta. 46+00	DB-4	29 ft x 59 ft	3.0	5,214	3:1
Strawberry Roan Trail Pond – Sta. 35+00	DB-5	29 ft x 59 ft	2.75	4,588	3:1
Strawberry Roan Trail Pond – Sta. 4+00	DB-7	39 ft x 69 ft	2.75	7,241	3:1
Appaloosa Trail Pond – Cul-de-Sac North	DB-4	24 ft x 44 ft	2.75	2,828	3:1
Appaloosa Trail Pond – Cul-de-Sac South	DB-4	24 ft x 44 ft	2.75	2,828	3:1
Buckskin Trail Pond – Sta. 6+00	DB-5	24 ft x 44 ft	2.75	2,828	3:1
Buckskin Trail Pond – Cul-de-Sac North	DB-5	19 ft x 29 ft	2.75	1,480	3:1
Buckskin Trail Pond – Cul-de-Sac South	DB-5	19 ft x 29 ft	2.75	1,480	3:1
Typical Lot Pond	All	19 ft x 34 ft	2.0	1,016	3:1

 Table 7 – Retention Ponds Overview

Stormwater conveyance for the site is primarily by roadside swales and pond swales which are a 12-ft wide triangular swale, with 3:1 side slope making it approximately 2 feet deep – shown in detail 1 on stormwater plan sheet WW4.7. These swales can convey approximately 48-cfs each side of the road at bank full at with 0.5% slope and assuming grass sides.

Subdivision Culvert Overview

Individual lots in project #1 will be responsible for installing a 18-in minimum diameter culvert at each driveway, as that project is on the downstream side of most of the drainage and more stormwater will need to be conveyed through driveway culverts. The 18-in cmp culvert was sized by analyzing the culvert at Sta. 89+00 of Strawberry Roan trail, where a large amount of stormwater from drainage basin #2 will be conveyed. The 18-in culvert at roughly 2% will have capacity to convey the required 7.88 cfs without overtopping the roadway, thus all culverts in project #1 under driveways should be 18-in to conservatively pass the 10-year, 24-hour event – these calculations are shown in Appendix 3. This culvert was also used as the control culvert for all typical culvert road crossings in subdivisions 1-4, as it has the largest drainage area to convey in the subdivision. All other individual driveway culverts in subdivisions #2-4 shall be 15-in diameter cmp culverts. Calculations shown in Appendix 3 show that a 15-in cmp for a worst-case scenario driveway crossing will convey the 10-year, 24-hour event. All typical road culvert crossings are shown as 18-in cmp culverts. All culverts that convey water under the road in existing drainage gullies were sized to be 36-in. The culvert crossing at Strawberry Roan Trail Sta. 3+25 was used as the control culvert for sizing gully drainage, as it has the largest area to convey in the development. Storm swales and culverts are described in Appendix 3 and MDEQ provided spreadsheets show their capacity to handle the design storms for the project. Culverts were sized to account for the increase flow due to increase in impervious area from residential homes and driveways. This is conservative, as lots should retain increased stormwater within individual retention ponds. All storm water conveyance infrastructure will handle the 10-YR 24-HR storm event without any overtopping. During the 100-YR storm the conveyance system will generally overtop some driveway culverts and the intersection of Strawberry Roan Trail and Lower Confederate Road on Lots #1 & 3. The overflow will continue to flow to existing drainage paths that end up flowing to Canyon Ferry Reservoir.

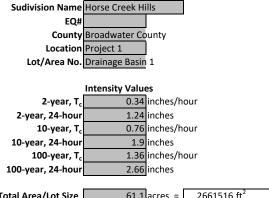
CONCLUSION

The retention facilities on-site have been designed to retain excess runoff from pre to post development during 2-year 24-hour storm. Conveyance structures have been designed to convey the entire runoff flow from the site during the 10-year, 24-hour storm. The site has been designed so that during the 100-year, 24-hour event, no buildings or drainfields are inundated during the event. All residential lots will construct their own ponds to capture the increased runoff for the individual lot. The 10-year storm will safely flow through the project without any overtopping of roads. During the 100-year event a small amount of ponding will occur at the downstream end of the subdivision, (South End) however no buildings or drainfields will be inundated. Stormwater will infiltrate and be completely gone after no more than 72 hours after the last storm event.

Appendix 1 – Drainage Basins - Pre and Post Analysis

Appendix G: Standard Storm Drainage Plan





Rational Method Co-Efficients (C)			
0.9	Paved/hard surfaces		
0.8	Gravel surfaces		
0.1	Lawn/landscaping		
0.2 Unimproved areas			
Q=C*i*A			

61.1 acres = Total Area/Lot Size 2661516 ft²

Initial Stormwater Facility Volume (0.5" x Impervious Area) =	0 ft ³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)	
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	61.1 acres	2661516 ft ²	Q= 4.189 ft ³ /sec	V= 55004.664 ft ³	Q= 9.365 ft ³ /sec	V= 84281.340 ft ³	Q= 16.758 ft ³ /sec
Total	61.1 acres	2661516 ft ²	Q _{Total} = 4.189 ft ³ /sec	V _{Total} = 55004.664 ft ³	Q _{Total} = 9.365 ft ³ /sec	V _{Total} = 84281.340 ft ³	Q _{Total} = 16.758 ft ³ /sec

			2-	year, T _c		2	-year, 24-ho	ur	:	LO-year,	T _c	10	-year, 24-ho	our	1	00-year,	T _c
Post-Development Characteristics		(flo	ow rate)			volume)			flow rate	e)		(volume)		(flow rate	e)	
Paved/House Area	0 acres	0 ft ²	Q= (0.000 f	t³/sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Gravel Area	0 acres	0 ft ²	Q= (0.000 ft	t³/sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Lawn/Landscaping	0 acres	0 ft ²	Q= (0.000 ft	t³/sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Unimproved Area	61.1 acres	2661516 ft ²	Q= 4	4.189 fi	t³/sec	V=	55004.664	ft ³	Q=	9.365	ft ³ /sec	V=	84281.340	ft ³	Q=	16.758	ft ³ /sec
Total	61.1 acres	2661516 ft ²	Q _{Total} = 4	4.189 fi	t³/sec	V _{Total} =	55004.664	ft°	Q _{Total} =	9.365	ft³/sec	V _{Total} =	84281.340	ft°	Q _{Total} =	16.758	ft³/sec

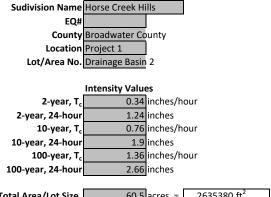
Runoff Flow/Volume Change	∆Q= 0.000 ft ³ /sec	$\Delta V = 0.000 \text{ ft}^3$	∆Q= 0.000 ft³/sec	$\Delta V = 0.000 \text{ ft}^3$	ΔQ= 0.000 ft ³ /sec

Required Minimum Facility Volume: **0** ft³

= input field

Appendix G: Standard Storm Drainage Plan





Ratio	onal Method Co-Efficients (C)				
0.9	Paved/hard surfaces				
0.8	Gravel surfaces				
0.1	Lawn/landscaping				
0.2	Unimproved areas				
Q=C*i*A					

Total Area/Lot Size 60.5 acres = 2635380 ft²

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 4265.2 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)	
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	60.5 acres	2635380 ft ²	Q= 4.148 ft ³ /sec	V= 54464.520 ft ³	Q= 9.273 ft ³ /sec	V= 83453.700 ft ³	Q= 16.593 ft ³ /sec
Total	60.5 acres	2635380 ft ²	Q _{Total} = 4.148 ft ³ /sec	V _{Total} = 54464.520 ft ³	Q _{Total} = 9.273 ft ³ /sec	V _{Total} = 83453.700 ft ³	Q _{Total} = 16.593 ft ³ /sec

		2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Post-Development Characteristics		(flow rate)	volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area 2.349977043 acres	102365 ft ²	Q= 0.725 ft ³ /sec	V= 9519.945 ft ³	Q= 1.621 ft ³ /sec	V= 14587.013 ft ³	Q= 2.900 ft ³ /sec
Gravel Area 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area 58.15002296 acres	2533015 ft ²	Q= 3.987 ft ³ /sec	V= 52348.977 ft ³	Q= 8.912 ft ³ /sec	V= 80212.142 ft ³	Q= 15.949 ft ³ /sec
Total 60.5 acres	2635380 ft ²	Q _{Total} = 4.712 ft ³ /sec	V _{Total} = 61868.922 ft ³	Q _{Total} = 10.533 ft [°] /sec	V _{Total} = 94799.154 ft ³	Q _{Total} = 18.849 ft [°] /sec

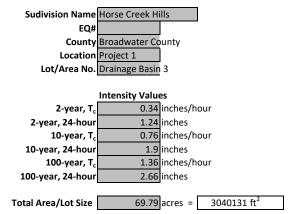
	Runoff Flow/Volume Change	∆Q= 0.564 ft ^³ /sec	∆V= 7404.402 ft ^³	∆Q= 1.261 ft ³ /sec	ΔV= 11345.454 ft ³	ΔQ= 2.256 ft ³ /sec
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Required Minimum Facility Volume: 7404.4 ft³

= input field

Appendix G: Standard Storm Drainage Plan





Ratio	Rational Method Co-Efficients (C)						
0.9	Paved/hard surfaces						
0.8	Gravel surfaces						
0.1	Lawn/landscaping						
0.2	Unimproved areas						
Q=C*i*A							

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 2729.2 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)	
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	69.79180441 acres	3040131 ft ²	Q= 4.785 ft ³ /sec	V= 62829.374 ft ³	Q= 10.697 ft ³ /sec	V= 96270.815 ft ³	Q= 19.142 ft ³ /sec
Total	69.79180441 acres	3040131 ft ²	Q _{Total} = 4.785 ft ³ /sec	V _{Total} = 62829.374 ft ³	Q _{Total} = 10.697 ft ³ /sec	V _{Total} = 96270.815 ft ³	Q _{Total} = 19.142 ft ³ /sec

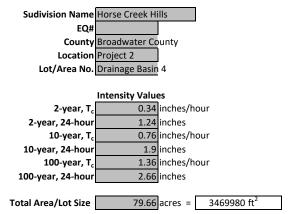
		2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, Т _с
Post-Development Characteristics		(flow rate)	volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area 1.503673095 acres	65500 ft ²	Q= 0.464 ft ³ /sec	V= 6091.500 ft ³	Q= 1.037 ft ³ /sec	V= 9333.750 ft ³	Q= 1.856 ft ³ /sec
Gravel Area 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area 68.28813131 acres	2974631 ft ²	Q= 4.682 ft ³ /sec	V= 61475.707 ft ³	Q= 10.466 ft ³ /sec	V= 94196.648 ft ³	Q= 18.729 ft ³ /sec
Total 69.79180441 acres	3040131 ft ²	Q _{Total} = 5.146 ft [°] /sec	V _{Total} = 67567.207 ft ³	Q _{Total} = 11.503 ft [°] /sec	V _{Total} = 103530.398 ft ³	Q _{Total} = 20.585 ft ³ /sec

Runoff Flow/Volume Change	∆Q= 0.361 ft ³ /sec	ΔV= 4737.833 ft ³	∆Q= 0.807 ft ³ /sec	ΔV = 7259.583 ft ³	ΔQ= 1.443 ft ³ /sec

Required Minimum Facility Volume: 4737.8 ft³

= input field





Rati	onal Method Co-Efficients (C)				
0.9	Paved/hard surfaces				
0.8 Gravel surfaces					
0.1 Lawn/landscaping					
0.2	Unimproved areas				
Q=C*i*	A				

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 5685.9 ft³

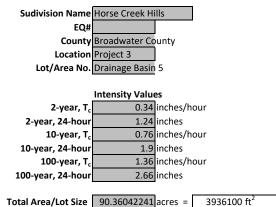
			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-D	Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	79.65977961 acres	3469980 ft ²	Q= 5.462 ft ³ /sec	V= 71712.920 ft ³	Q= 12.209 ft ³ /sec	V= 109882.700 ft ³	Q= 21.848 ft ³ /sec
Total	79.65977961 acres	3469980 ft ²	Q _{Total} = 5.462 ft ³ /sec	V _{Total} = 71712.920 ft ³	Q _{Total} = 12.209 ft ³ /sec	V _{Total} = 109882.700 ft ³	Q _{Total} = 21.848 ft ³ /sec

Г		2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Post-Development Characteristics		(flow rate)	volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area 3.132713499 acres	136461 ft ²	Q= 0.967 ft ³ /sec	V= 12690.873 ft ³	Q= 2.161 ft ³ /sec	V= 19445.693 ft ³	Q= 3.866 ft ³ /sec
Gravel Area 0 acres	0 ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping 0 acres	0 ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area 76.52706612 acres	3333519 ft ²	Q= 5.247 ft ³ /sec	V= 68892.726 ft ³	Q= 11.729 ft ³ /sec	V= 105561.435 ft ³	Q= 20.989 ft ³ /sec
Total 79.65977961 acres	3469980 ft ²	Q _{Total} = 6.214 ft ³ /sec	V _{Total} = 81583.599 ft ³	Q _{Total} = 13.890 ft [°] /sec	V _{Total} = 125007.128 ft ³	Q _{Total} = 24.855 ft ³ /sec

	Runoff Flow/Volume Change	∆Q= 0.752 ft ³ /sec	ΔV= 9870.679 ft ³	∆Q= 1.680 ft ³ /sec	∆V= 15124.428 ft ³	ΔQ= 3.007 ft ³ /sec
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Required Minimum Facility Volume: 9870.7 ft³





Ratio	onal Method Co-Efficients (C)
0.9	Paved/hard surfaces
0.8	Gravel surfaces
0.1	Lawn/landscaping
0.2	Unimproved areas
Q=C*i*	Α.

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 5246.7 ft³

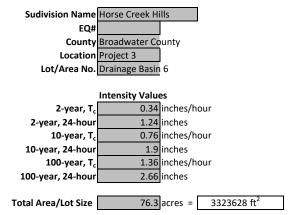
					-									
			2	2-year, T	c	2	-year, 24-ho	ur		10-year, T _c	10	-year, 24-hour	1	L00-year, T _c
Pre-D	Development Character	istics	(f	low rate	e)		(volume)			(flow rate)		(volume)	((flow rate)
Paved/House Area	0 acres	ft ²	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000 ft ³ /sec	V=	0.000 ft ³	Q=	0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000 ft ³ /sec	V=	0.000 ft ³	Q=	0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000 ft ³ /sec	V=	0.000 ft ³	Q=	0.000 ft ³ /sec
Unimproved Area	90.36042241 acres	3936100 ft ²	Q=	6.196	ft ³ /sec	V=	81346.067	ft ³	Q=	13.849 ft ³ /sec	V=	124643.167 ft ³	Q=	24.783 ft ³ /sec
Total	90.36042241 acres	3936100 ft ²	Q _{Total} =	6.196	ft ³ /sec	V _{Total} =	81346.067	ft ³	Q _{Total} =	13.849 ft ³ /sec	V _{Total} =	124643.167 ft ³	Q _{Total} =	24.783 ft ³ /sec

		2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Post-Development Characteristics		(flow rate)	volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area 2.890725436 acres	125920 ft ²	Q= 0.892 ft ³ /sec	V= 11710.560 ft ³	Q= 1.994 ft ³ /sec	V= 17943.600 ft ³	Q= 3.568 ft ³ /sec
Gravel Area 0 acres	0 ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping 0 acres	0 ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area 87.46969697 acres	3810180 ft ²	Q= 5.998 ft ³ /sec	V= 78743.720 ft ³	Q= 13.406 ft ³ /sec	V= 120655.700 ft ³	Q= 23.990 ft ³ /sec
Total 90.36042241 acres	3936100 ft ²	Q _{Total} = 6.889 ft ³ /sec	V _{Total} = 90454.280 ft ³	Q _{Total} = 15.400 ft [°] /sec	V _{Total} = 138599.300 ft ³	Q _{Total} = 27.558 ft ³ /sec

	Runoff Flow/Volume Change	∆Q= 0.694 ft³/sec	ΔV= 9108.213 ft ³	∆Q= 1.551 ft ³ /sec	ΔV= 13956.133 ft ³	ΔQ= 2.775 ft ³ /sec
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Required Minimum Facility Volume: 9108.2 ft³





Ratio	onal Method Co-Efficients (C)				
0.9	Paved/hard surfaces				
0.8 Gravel surfaces					
0.1 Lawn/landscaping					
0.2	Unimproved areas				
Q=C*i*	A				

Initial Stormwater Facility Volume (0.5" x Impervious Area) =	0 ft ³

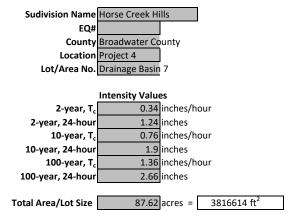
			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		istics	(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	76.3 acres	3323628 ft ²	Q= 5.232 ft ³ /sec	V= 68688.312 ft ³	Q= 11.694 ft ³ /sec	V= 105248.220 ft ³	Q= 20.927 ft ³ /sec
Total	76.3 acres	3323628 ft ²	Q _{Total} = 5.232 ft ³ /sec	V _{Total} = 68688.312 ft ³	Q _{Total} = 11.694 ft ³ /sec	V _{Total} = 105248.220 ft ³	Q _{Total} = 20.927 ft ³ /sec

			2-yea	ır, T _c	2	-year, 24-ho	ur	1	LO-year, 1	۲ _c	10	-year, 24-ho	our	1	00-year, 1	ſ
Post-Dev	elopment Character	ristics	(flow rate)			volume)		(flow rate)		(volume)		(flow rate))		
Paved/House Area	0 acres	ft ²	Q= 0.00	00 ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Gravel Area	0 acres	0 ft ²	Q= 0.00	00 ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Lawn/Landscaping	0 acres	0 ft ²	Q= 0.00	00 ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Unimproved Area	76.3 acres	3323628 ft ²	Q= 5.23	32 ft ³ /sec	V=	68688.312	ft ³	Q=	11.694	ft ³ /sec	V=	105248.220) ft ³	Q=	20.927	ft ³ /sec
Total	76.3 acres	3323628 ft ²	Q _{Total} = 5.23	32 ft³/sec	V _{Total} =	68688.312	ft°	Q _{Total} =	11.694	ft³/sec	V _{Total} =	105248.220) ft [°]	Q _{Total} =	20.927	ft³/sec

Runoff Flow/Volume Change	∆Q= 0.000 ft ³ /sec	ΔV= 0.000 ft ³	∆Q= 0.000 ft³/sec	$\Delta V = 0.000 \text{ ft}^{3}$	∆Q= 0.000 ft³/sec

Required Minimum Facility Volume: 0 ft³





Rational Method Co-Efficients (C)					
0.9	Paved/hard surfaces				
0.8	Gravel surfaces				
0.1	Lawn/landscaping				
0.2	Unimproved areas				
Q=C*i*A					

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 3776 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)	
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	87.61740129 acres	3816614 ft ²	Q= 6.008 ft ³ /sec	V= 78876.689 ft ³	Q= 13.429 ft ³ /sec	V= 120859.443 ft ³	Q= 24.031 ft ³ /sec
Total	87.61740129 acres	3816614 ft ²	Q _{Total} = 6.008 ft ³ /sec	V _{Total} = 78876.689 ft ³	Q _{Total} = 13.429 ft ³ /sec	V _{Total} = 120859.443 ft ³	Q _{Total} = 24.031 ft ³ /sec

		2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Post-Development Characteristics		(flow rate)	volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area 2.080440771 acres	90624 ft ²	Q= 0.642 ft ³ /sec	V= 8428.032 ft ³	Q= 1.435 ft ³ /sec	V= 12913.920 ft ³	Q= 2.568 ft ³ /sec
Gravel Area 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area 85.53696051 acres	3725990 ft ²	Q= 5.865 ft ³ /sec	V= 77003.793 ft ³	Q= 13.110 ft ³ /sec	V= 117989.683 ft ³	Q= 23.460 ft ³ /sec
Total 87.61740129 acres	3816614 ft ²	Q _{Total} = 6.507 ft ³ /sec	V _{Total} = 85431.825 ft [°]	Q _{Total} = 14.545 ft ³ /sec	V _{Total} = 130903.603 ft ³	Q _{Total} = 26.028 ft ³ /sec

	Runoff Flow/Volume Change	∆Q= 0.499 ft³/sec	∆V= 6555.136 ft ^³	∆Q= 1.116 ft ³ /sec	ΔV= 10044.160 ft ³	∆Q= 1.997 ft ^³ /sec
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Required Minimum Facility Volume: 6555.1 ft³



Appendix 2 – Pond Sizing Calculations

Appendix 2 – Pond Size Overview Table

Pond No.	Pond Name	Storage Types				Bottom Elevation	Pond Depth	Top Elevation	Available Storage
	Fond Name	Contours	Trapezoid	UG Chambers	Manual	(ft)	(ft)	(ft)	(cuft)
1	Strawbeery Roan Pond - Sta. 68+00		х			100.00	2.75	102.75	5,389
2	Strawberry Roan Pond - Sta. 92+00		x			100.00	2.75	102.75	8,293
3	Lot Pond Typ.		х			100.00	2.00	102.00	1,016
4	Strawberry Roan Trail Pond - Sta. 46+00		х			100.00	3.00	103.00	5,214
5	Strawberry Roan Pond - Sta. 35+00		х			100.00	2.75	102.75	4,588
6	Buckskin Trail Pond - Sta 6+00		х			100.00	2.75	102.75	2,828
7	Bucksin Trail Ponds - Cul-de-Sac North & south		х			100.00	2.75	102.75	1,480
8	Strawberry Roan Pond - Sta. 4+00		х			100.00	2.75	102.75	7,241
9	Appaloosa Trail Ponds - Cul-de-Sac North & South		х			100.00	2.75	102.75	2,828



Sudivision Name	Horse Creek Hi	lls 1				
EQ#						
County	Broadwater Co	unty				
Location	Project 1 - SRT	Pond Sta	. 92+00			
Lot/Area No.	Drainage Basin	s 1 & 2				
	Intensity Value	es				
2-year, T _c	0.34	inches/h	our			
2-year, 24-hour	1.24	inches				
10-year, T _c	0.76 inches/hour					
10-year, 24-hour	1.9 inches					
100-year, T _c	1.36	1.36 inches/hour				
100-year, 24-hour	2.66	inches				
Total Area/Lot Size	121.57	acres =	5295530 ft ²			

Rational Method Co-Efficients (C)					
0.9	Paved/hard surfaces				
0.8	Gravel surfaces				
0.1	Lawn/landscaping				
0.2	Unimproved areas				
Q=C*i*	Α				

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 4265.2 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)	
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	121.568641 acres	5295530 ft ²	Q= 8.336 ft ³ /sec	V= 109440.953 ft ³	Q= 18.632 ft ³ /sec	V= 167691.783 ft ³	Q= 33.342 ft ³ /sec
Total	121.568641 acres	5295530 ft ²	Q _{Total} = 8.336 ft ³ /sec	V _{Total} = 109440.953 ft ³	Q _{Total} = 18.632 ft ³ /sec	V _{Total} = 167691.783 ft ³	Q _{Total} = 33.342 ft ³ /sec

		2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Post-Development Characteristics		(flow rate)	volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area 2.349977043 acr	es 102365 ft ²	Q= 0.725 ft ³ /sec	V= 9519.945 ft ³	Q= 1.621 ft ³ /sec	V= 14587.013 ft ³	Q= 2.900 ft ³ /sec
Gravel Area 0 act	es 0 ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping 0 acr	es 0 ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area 119.2186639 acr	es 5193165 ft ²	Q= 8.174 ft ³ /sec	V= 107325.410 ft ³	Q= 18.272 ft ³ /sec	V= 164450.225 ft ³	Q= 32.698 ft ³ /sec
Total 121.568641 acr	es 5295530 ft ²	Q _{Total} = 8.900 ft ³ /sec	V _{Total} = 116845.355 ft ³	Q _{Total} = 19.893 ft [°] /sec	V _{Total} = 179037.238 ft ³	Q _{Total} = 35.598 ft [°] /sec
			_			

Runoff Flow/Volume Change	∆Q= 0.564 ft ³ /sec	∆V= 7404.402 ft ^³	∆Q= 1.261 ft ³ /sec	ΔV= 11345.454 ft ³	ΔQ= 2.256 ft ³ /sec

Required Minimum Facility Volume: 7404.4 ft³



Sudivision Name	Horse Creek Hills	
EQ#		
County	Broadwater County	
Location	Project 1 - SRT Pond Sta. 68+00	
Lot/Area No.	Drainage Basin 3	
	Intensity Values	
2-year, T _c	0.34 inches/hour	
2-year, 24-hour	1.24 inches	
10-year, T _c	0.76 inches/hour	
10-year, 24-hour	1.9 inches	
100-year, T _c	1.36 inches/hour	
100-year, 24-hour	2.66 inches	
Total Area/Lot Size	69.79 acres = 3040131 ft^2	

Rational Method Co-Efficients (C)						
0.9	Paved/hard surfaces					
0.8	Gravel surfaces					
0.1	Lawn/landscaping					
0.2 Unimproved areas						
Q=C*i*A						

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 2729.2 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)	
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	69.79180441 acres	3040131 ft ²	Q= 4.785 ft ³ /sec	V= 62829.374 ft ³	Q= 10.697 ft ³ /sec	V= 96270.815 ft ³	Q= 19.142 ft ³ /sec
Total	69.79180441 acres	3040131 ft ²	Q _{Total} = 4.785 ft ³ /sec	V _{Total} = 62829.374 ft ³	Q _{Total} = 10.697 ft ³ /sec	V _{Total} = 96270.815 ft ³	Q _{Total} = 19.142 ft ³ /sec

		2-year, T _c		2-уе	ar, 24-hour		1	0-year, T	c	10	-year, 24-ho	ur	1	00-year, [·]	T _c
Post-Development Characteristics		(flow rate)			volume)		(flow rate)		(volume)		(flow rate	e)
Paved/House Area 1.503673095 acres	65500 ft ²	Q= 0.464 ft ³ /	/sec	V= 6	091.500 f	ť	Q=	1.037	ft ³ /sec	V=	9333.750	ft ³	Q=	1.856	ft ³ /sec
Gravel Area 0 acres	0 ft ²	Q= 0.000 ft ³ /	/sec	V=	0.000 f	t ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Lawn/Landscaping 0 acres	0 ft ²	Q= 0.000 ft ³ /	/sec	V=	0.000 f	t ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Unimproved Area 68.28813131 acres	2974631 ft ²	Q= 4.682 ft ³ /	/sec	V= 63	1475.707 f	t ³	Q=	10.466	ft ³ /sec	V=	94196.648	ft ³	Q=	18.729	ft ³ /sec
Total 69.79180441 acres	3040131 ft ²	Q _{Total} = 5.146 ft ³ /	/sec	V _{Total} = 67	7567.207 f	ť	Q _{Total} =	11.503	ft³/sec	V _{Total} =	103530.398	ft°	Q _{Total} =	20.585	ft³/sec

	Runoff Flow/Volume Change	∆Q= 0.361 ft ³ /sec	∆V= 4737.833 ft ^³	ΔQ= 0.807 ft ³ /sec	ΔV= 7259.583 ft ³	ΔQ= 1.443 ft ³ /sec
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Required Minimum Facility Volume: 4737.8 ft³



Sudivision Name	Horse Creek Hi	ills
EQ#		
County	Broadwater Co	ounty
Location	Project 2 - SRT	Pond Sta. 46+00
Lot/Area No.	Drainage Basin	4
	Intensity Value	es
2-year, T _c	0.34	inches/hour
2-year, 24-hour	1.24	inches
10-year, T _c	0.76	inches/hour
10-year, 24-hour	1.9	inches
100-year, T _c	1.36	inches/hour
100-year, 24-hour	2.66	inches
otal Area/Lot Size	79.66	$acres = 3469980 \text{ ft}^2$

Rational Method Co-Efficients (C)					
0.9	Paved/hard surfaces				
0.8	Gravel surfaces				
0.1	Lawn/landscaping				
0.2	Unimproved areas				
Q=C*i*A					

 Total Area/Lot Size
 79.66
 acres
 3469980 ft⁻

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 2931.4 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)	
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	79.65977961 acres	3469980 ft ²	Q= 5.462 ft ³ /sec	V= 71712.920 ft ³	Q= 12.209 ft ³ /sec	V= 109882.700 ft ³	Q= 21.848 ft ³ /sec
Total	79.65977961 acres	3469980 ft ²	Q _{Total} = 5.462 ft ³ /sec	V _{Total} = 71712.920 ft ³	Q _{Total} = 12.209 ft ³ /sec	V _{Total} = 109882.700 ft ³	Q _{Total} = 21.848 ft ³ /sec

		2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Post-Development Characteristics		(flow rate)	volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area 1.615105601 acres	70354 ft ²	Q= 0.498 ft ³ /sec	$V = 6542.922 \text{ ft}^3$	Q= 1.114 ft ³ /sec	V= 10025.445 ft ³	Q= 1.993 ft ³ /sec
Gravel Area 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area 78.04467401 acres	3399626 ft ²	Q= 5.351 ft ³ /sec	V= 70258.937 ft ³	Q= 11.962 ft ³ /sec	V= 107654.823 ft ³	Q= 21.405 ft ³ /sec
Total 79.65977961 acres	3469980 ft ²	Q _{Total} = 5.850 ft ³ /sec	V _{Total} = 76801.859 ft ³	Q _{Total} = 13.076 ft [°] /sec	V _{Total} = 117680.268 ft ³	Q _{Total} = 23.398 ft ³ /sec

Runoff Flow/Volume Change	∆Q= 0.388 ft³/sec	ΔV= 5088.939 ft ³	∆Q= 0.866 ft ³ /sec	ΔV= 7797.568 ft ³	ΔQ= 1.550 ft ³ /sec

Required Minimum Facility Volume: 5088.9 ft³



Sudivision Name	Horse Creek Hil	ls					
EQ#							
County	Broadwater County						
Location	Project 3 - SRT	Project 3 - SRT Pond Sta. 35+00					
Lot/Area No.	Drainage Basin 5						
	Intensity Value	S					
2-year, T _c	0.34	inches/ho	bur				
2-year, 24-hour	1.24	inches					
10-year, T _c	0.76	inches/ho	bur				
10-year, 24-hour	1.9	inches					
100-year, T _c	1.36	inches/ho	bur				
100-year, 24-hour	2.66	inches					
		_					
Total Area/Lot Size	90.36	acres =	3936100 ft ²				

Rational Method Co-Efficients (C)					
0.9	Paved/hard surfaces				
0.8	Gravel surfaces				
0.1	Lawn/landscaping				
0.2 Unimproved areas					
Q=C*i*A					

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 2466.7 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)	
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	90.36042241 acres	3936100 ft ²	Q= 6.196 ft ³ /sec	V= 81346.067 ft ³	Q= 13.849 ft ³ /sec	V= 124643.167 ft ³	Q= 24.783 ft ³ /sec
Total	90.36042241 acres	3936100 ft ²	Q _{Total} = 6.196 ft ³ /sec	V _{Total} = 81346.067 ft ³	Q _{Total} = 13.849 ft ³ /sec	V _{Total} = 124643.167 ft ³	Q _{Total} = 24.783 ft ³ /sec

		2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Post-Development Characte	ristics	(flow rate)	volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area 1.359044995 acres	59200 ft ²	Q= 0.419 ft ³ /sec	V= 5505.600 ft ³	Q= 0.937 ft ³ /sec	V= 8436.000 ft ³	Q= 1.677 ft ³ /sec
Gravel Area 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area 89.00137741 acres	3876900 ft ²	Q= 6.103 ft ³ /sec	V= 80122.600 ft ³	Q= 13.641 ft ³ /sec	V= 122768.500 ft ³	Q= 24.410 ft ³ /sec
Total 90.36042241 acres	3936100 ft ²	Q _{Total} = 6.522 ft ³ /sec	V _{Total} = 85628.200 ft ³	Q _{Total} = 14.578 ft [°] /sec	V _{Total} = 131204.500 ft ³	Q _{Total} = 26.087 ft [°] /sec

Runoff Flow/Volume Change	∆Q= 0.326 ft ^³ /sec	ΔV= 4282.133 ft ³	∆Q= 0.729 ft ³ /sec	ΔV = 6561.333 ft ³	ΔQ= 1.305 ft ³ /sec

Required Minimum Facility Volume: 4282.1 ft³



Sudivision Name	Horse Creek Hi	lls	
EQ#			
County	Broadwater Co	unty	
Location	Project 4 - SRT	Sta. 4+00	
Lot/Area No.	Drainage Basin	7	
	Intensity Value	es	
2-year, T _c	0.34	inches/ho	bur
2-year, 24-hour	1.24	inches	
10-year, T _c	0.76	inches/hc	bur
10-year, 24-hour	1.9	inches	
100-year, T _c	1.36	inches/hc	bur
100-year, 24-hour	2.66	inches	
Total Area/Lot Size	87.62	acres =	3816614 ft ²

Ratio	onal Method Co-Efficients (C)				
0.9	Paved/hard surfaces				
0.8	Gravel surfaces				
0.1 Lawn/landscaping					
0.2 Unimproved areas					
Q=C*i*	Ą				

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 3776 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-D	evelopment Characteri	istics	(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	87.61740129 acres	3816614 ft ²	Q= 6.008 ft ³ /sec	V= 78876.689 ft ³	Q= 13.429 ft ³ /sec	V= 120859.443 ft ³	Q= 24.031 ft ³ /sec
Total	87.61740129 acres	3816614 ft ²	Q _{Total} = 6.008 ft ³ /sec	V _{Total} = 78876.689 ft ³	Q _{Total} = 13.429 ft ³ /sec	V _{Total} = 120859.443 ft ³	Q _{Total} = 24.031 ft ³ /sec

		2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Post-Development Characte	ristics	(flow rate)	volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area 2.080440771 acres	90624 ft ²	Q= 0.642 ft ³ /sec	V= 8428.032 ft ³	Q= 1.435 ft ³ /sec	V= 12913.920 ft ³	Q= 2.568 ft ³ /sec
Gravel Area 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area 85.53696051 acres	3725990 ft ²	Q= 5.865 ft ³ /sec	V= 77003.793 ft ³	Q= 13.110 ft ³ /sec	V= 117989.683 ft ³	Q= 23.460 ft ³ /sec
Total 87.61740129 acres	3816614 ft ²	Q _{Total} = 6.507 ft ³ /sec	V _{Total} = 85431.825 ft ³	Q _{Total} = 14.545 ft [°] /sec	V _{Total} = 130903.603 ft ³	Q _{Total} = 26.028 ft ³ /sec
		B	•	-		-

	Runoff Flow/Volume Change	∆Q= 0.499 ft³/sec	ΔV= 6555.136 ft ³	ΔQ= 1.116 ft ³ /sec	ΔV= 10044.160 ft ³	∆Q= 1.997 ft ³ /sec
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Required Minimum Facility Volume: 6555.1 ft³



Sudivision Name	Horse Creek Hills
EQ#	
County	Broadwater County
Location	Project 2 - APT Cul-de-Sac Pond North
Lot/Area No.	Drainage Basin 4
	Intensity Values
2-year, T _c	0.34 inches/hour
2-year, 24-hour	1.24 inches
10-year, T _c	0.76 inches/hour
10-year, 24-hour	1.9 inches
100-year, T _c	1.36 inches/hour
100-year, 24-hour	2.66 inches
Total Area/Lot Size	79.66 acres = 3469980 ft^2

Ratio	onal Method Co-Efficients (C)				
0.9	Paved/hard surfaces				
0.8	Gravel surfaces				
0.1	Lawn/landscaping				
0.2 Unimproved areas					
Q=C*i*	Ą				

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 1377.2 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-D	evelopment Character	istics	(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	79.65977961 acres	3469980 ft ²	Q= 5.462 ft ³ /sec	V= 71712.920 ft ³	Q= 12.209 ft ³ /sec	V= 109882.700 ft ³	Q= 21.848 ft ³ /sec
Total	79.65977961 acres	3469980 ft ²	Q _{Total} = 5.462 ft ³ /sec	V _{Total} = 71712.920 ft ³	Q _{Total} = 12.209 ft ³ /sec	V _{Total} = 109882.700 ft ³	Q _{Total} = 21.848 ft ³ /sec

		2-year, T	c	2	-year, 24-ho	ur	1	LO-year, 1	Г _с	10	-year, 24-hou	ur	1	00-year, 1	Г _с
Post-Development Characte	ristics	(flow rate	e)		volume)		(flow rate	e)		(volume)		(flow rate)
Paved/House Area 0.758803949 acres	33053.5 ft ²	Q= 0.234	ft ³ /sec	V=	3073.976	ft ³	Q=	0.523	ft ³ /sec	V=	4710.124	ft ³	Q=	0.937	ft ³ /sec
Gravel Area 0 acres	0 ft ²	Q= 0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Lawn/Landscaping 0 acres	0 ft ²	Q= 0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Unimproved Area 78.90097567 acres	3436926.5 ft ²	Q= 5.410	ft ³ /sec	V=	71029.814	ft ³	Q=	12.093	ft ³ /sec	V=	108836.006	ft ³		21.640	
Total 79.65977961 acres	3469980 ft ²	Q _{Total} = 5.644	ft³/sec	V _{Total} =	74103.790	ft°	Q _{Total} =	12.616	ft³/sec	V _{Total} =	113546.130	ft°	Q _{Total} =	22.576	ft³/sec

	Runoff Flow/Volume Change	∆Q= 0.182 ft ³ /sec	ΔV= 2390.870 ft ³	∆Q= 0.407 ft³/sec	∆V= 3663.430 ft ³	∆Q= 0.728 ft³/sec
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Required Minimum Facility Volume: 2390.9 ft³



Sudivision Name	Horse Creek Hills
EQ#	
County	Broadwater County
Location	Project 2 - APT Cul-de-Sac Pond South
Lot/Area No.	Drainage Basin 4
	Intensity Values
2-year, T _c	0.34 inches/hour
2-year, 24-hour	1.24 inches
10-year, T _c	0.76 inches/hour
10-year, 24-hour	1.9 inches
100-year, T _c	1.36 inches/hour
100-year, 24-hour	2.66 inches
Total Area/Lot Size	79.66 acres = 3469980 ft ²

Rational Method Co-Efficients (C)					
0.9	Paved/hard surfaces				
0.8	Gravel surfaces				
0.1	Lawn/landscaping				
0.2	Unimproved areas				
Q=C*i*/	Q=C*i*A				

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 1377.2 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-D	evelopment Characteri	istics	(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	79.65977961 acres	3469980 ft ²	Q= 5.462 ft ³ /sec	V= 71712.920 ft ³	Q= 12.209 ft ³ /sec	V= 109882.700 ft ³	Q= 21.848 ft ³ /sec
Total	79.65977961 acres	3469980 ft ²	Q _{Total} = 5.462 ft ³ /sec	V _{Total} = 71712.920 ft ³	Q _{Total} = 12.209 ft ³ /sec	V _{Total} = 109882.700 ft ³	Q _{Total} = 21.848 ft ³ /sec

		2-year, T	c	2	-year, 24-ho	ur	1	LO-year, 1	Г _с	10	-year, 24-hou	ur	1	00-year, 1	Г _с
Post-Development Characte	ristics	(flow rate	e)		volume)		(flow rate	e)		(volume)		(flow rate)
Paved/House Area 0.758803949 acres	33053.5 ft ²	Q= 0.234	ft ³ /sec	V=	3073.976	ft ³	Q=	0.523	ft ³ /sec	V=	4710.124	ft ³	Q=	0.937	ft ³ /sec
Gravel Area 0 acres	0 ft ²	Q= 0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Lawn/Landscaping 0 acres	0 ft ²	Q= 0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Unimproved Area 78.90097567 acres	3436926.5 ft ²	Q= 5.410	ft ³ /sec	V=	71029.814	ft ³	Q=	12.093	ft ³ /sec	V=	108836.006	ft ³		21.640	
Total 79.65977961 acres	3469980 ft ²	Q _{Total} = 5.644	ft³/sec	V _{Total} =	74103.790	ft°	Q _{Total} =	12.616	ft³/sec	V _{Total} =	113546.130	ft°	Q _{Total} =	22.576	ft³/sec

	Runoff Flow/Volume Change	∆Q= 0.182 ft ³ /sec	ΔV= 2390.870 ft ³	∆Q= 0.407 ft³/sec	∆V= 3663.430 ft ³	∆Q= 0.728 ft³/sec
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Required Minimum Facility Volume: 2390.9 ft³



Sudivision Name	Horse Creek Hills
EQ#	
County	Broadwater County
Location	Project 3 - BST Pond Sta. 6+00
Lot/Area No.	Drainage Basin 5
	Intensity Values
2-year, T _c	0.34 inches/hour
2-year, 24-hour	1.24 inches
10-year, T _c	0.76 inches/hour
10-year, 24-hour	1.9 inches
100-year, T _c	1.36 inches/hour
100-year, 24-hour	2.66 inches
Total Area/Lot Size	90.36 acres = 3936100 ft^2

Rational Method Co-Efficients (C)					
0.9	Paved/hard surfaces				
0.8	Gravel surfaces				
0.1	Lawn/landscaping				
0.2	Unimproved areas				
Q=C*i*A					

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 1523.1 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-D	evelopment Characteri	istics	(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	90.36042241 acres	3936100 ft ²	Q= 6.196 ft ³ /sec	V= 81346.067 ft ³	Q= 13.849 ft ³ /sec	V= 124643.167 ft ³	Q= 24.783 ft ³ /sec
Total	90.36042241 acres	3936100 ft ²	Q _{Total} = 6.196 ft ³ /sec	V _{Total} = 81346.067 ft ³	Q _{Total} = 13.849 ft ³ /sec	V _{Total} = 124643.167 ft ³	Q _{Total} = 24.783 ft ³ /sec

		2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Post-Development Characte	ristics	(flow rate)	volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area 0.839187328 acres	36555 ft ²	Q= 0.259 ft ³ /sec	V= 3399.615 ft ³	Q= 0.579 ft ³ /sec	V= 5209.088 ft ³	Q= 1.036 ft ³ /sec
Gravel Area 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping 0 acres	0 ft^2	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area 89.52123508 acres	3899545 ft ²	Q= 6.138 ft ³ /sec	V= 80590.597 ft ³	Q= 13.721 ft ³ /sec	V= 123485.592 ft ³	Q= 24.553 ft ³ /sec
Total 90.36042241 acres	3936100 ft ²	Q _{Total} = 6.397 ft [°] /sec	V _{Total} = 83990.212 ft [°]	Q _{Total} = 14.299 ft [°] /sec	V _{Total} = 128694.679 ft ³	Q _{Total} = 25.588 ft [°] /sec

	Runoff Flow/Volume Change	∆Q= 0.201 ft ³ /sec	∆V= 2644.145 ft ^³	∆Q= 0.450 ft ³ /sec	ΔV= 4051.513 ft ³	∆Q= 0.806 ft ³ /sec
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Required Minimum Facility Volume: 2644.1 ft³



Sudivision Name	Horse Creek Hills	
EQ#		
County	Broadwater County	
Location	Project 3 - BST Cul-de-Sac Pond North	
Lot/Area No.	Drainage Basin 5	
	Intensity Values	
2-year, T _c	0.34 inches/hour	
2-year, 24-hour	1.24 inches	
10-year, T _c	0.76 inches/hour	
10-year, 24-hour	1.9 inches	
100-year, T _c	1.36 inches/hour	
100-year, 24-hour	2.66 inches	
Total Area/Lot Size	90.36 acres = 3936100 ft^2	

Rational Method Co-Efficients (C)					
0.9	Paved/hard surfaces				
0.8	Gravel surfaces				
0.1	Lawn/landscaping				
0.2	Unimproved areas				
Q=C*i*	A				

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 628.44 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)	
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	90.36042241 acres	3936100 ft ²	Q= 6.196 ft ³ /sec	V= 81346.067 ft ³	Q= 13.849 ft ³ /sec	V= 124643.167 ft ³	Q= 24.783 ft ³ /sec
Total	90.36042241 acres	3936100 ft ²	Q _{Total} = 6.196 ft ³ /sec	V _{Total} = 81346.067 ft ³	Q _{Total} = 13.849 ft ³ /sec	V _{Total} = 124643.167 ft ³	Q _{Total} = 24.783 ft ³ /sec

		2-year,	T _c	2	-year, 24-ho	ır	1	0-year, 1	Г _с	10	-year, 24-hou	ır	1	00-year, 1	Г _с
Post-Development Characteristics		(flow rate)			volume)		(flow rate)		(volume)			(flow rate))	
Paved/House Area 0.346246556 acres	15082.5 ft ²	Q= 0.107	ft ³ /sec	V=	1402.673	ft ³	Q=	0.239	ft ³ /sec	V=	2149.256	ft ³	Q=	0.427	ft ³ /sec
Gravel Area 0 acres	0 ft ²	Q= 0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Lawn/Landscaping 0 acres	0 ft ²	Q= 0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Unimproved Area 90.01417585 acres	3921017.5 ft ²	Q= 6.172	ft ³ /sec	V=	81034.362	ft ³	Q=	13.796	ft ³ /sec	V=	124165.554	ft ³	Q=	24.688	ft ³ /sec
Total 90.36042241 acres	3936100 ft ²	Q _{Total} = 6.279	ft³/sec	V _{Total} =	82437.034	ft°	Q _{Total} =	14.035	ft³/sec	V _{Total} =	126314.810	ft°	Q _{Total} =	25.115	ft³/sec

Runoff Flow/Volume Change	∆Q= 0.083 ft ³ /sec	ΔV= 1090.968 ft ³	∆Q= 0.186 ft³/sec	∆V= 1671.644 ft ^³	∆Q= 0.332 ft ³ /sec

Required Minimum Facility Volume: 1091 ft³



Sudivision Name	Horse Creek Hills							
EQ#								
County	Broadwater County							
Location	roject 3 - BST Cul-de-Sac Pond South							
Lot/Area No.	rainage Basin 5							
	Intensity Values							
2-year, T _c	0.34 inches/hour							
2-year, 24-hour	1.24 inches							
10-year, T _c	0.76 inches/hour							
10-year, 24-hour	1.9 inches							
100-year, T _c	1.36 inches/hour							
100-year, 24-hour	2.66 inches							
Total Area/Lot Size	90.36 acres = 3936100 ft ²							

Ratio	onal Method Co-Efficients (C)						
0.9	Paved/hard surfaces						
0.8	Gravel surfaces						
0.1	Lawn/landscaping						
0.2	Unimproved areas						
Q=C*i*	Q=C*i*A						

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 628.44 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)	
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	90.36042241 acres	3936100 ft ²	Q= 6.196 ft ³ /sec	V= 81346.067 ft ³	Q= 13.849 ft ³ /sec	V= 124643.167 ft ³	Q= 24.783 ft ³ /sec
Total	90.36042241 acres	3936100 ft ²	Q _{Total} = 6.196 ft ³ /sec	V _{Total} = 81346.067 ft ³	Q _{Total} = 13.849 ft ³ /sec	V _{Total} = 124643.167 ft ³	Q _{Total} = 24.783 ft ³ /sec

		2-year,	T _c	2	-year, 24-ho	ır	1	0-year, 1	Г _с	10	-year, 24-hou	ır	1	00-year, 1	Г _с
Post-Development Characteristics		(flow rate)			volume)		(flow rate)		(volume)			(flow rate))	
Paved/House Area 0.346246556 acres	15082.5 ft ²	Q= 0.107	ft ³ /sec	V=	1402.673	ft ³	Q=	0.239	ft ³ /sec	V=	2149.256	ft ³	Q=	0.427	ft ³ /sec
Gravel Area 0 acres	0 ft ²	Q= 0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Lawn/Landscaping 0 acres	0 ft ²	Q= 0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec	V=	0.000	ft ³	Q=	0.000	ft ³ /sec
Unimproved Area 90.01417585 acres	3921017.5 ft ²	Q= 6.172	ft ³ /sec	V=	81034.362	ft ³	Q=	13.796	ft ³ /sec	V=	124165.554	ft ³	Q=	24.688	ft ³ /sec
Total 90.36042241 acres	3936100 ft ²	Q _{Total} = 6.279	ft³/sec	V _{Total} =	82437.034	ft°	Q _{Total} =	14.035	ft³/sec	V _{Total} =	126314.810	ft°	Q _{Total} =	25.115	ft³/sec

Runoff Flow/Volume Change	∆Q= 0.083 ft ³ /sec	ΔV= 1090.968 ft ³	∆Q= 0.186 ft³/sec	∆V= 1671.644 ft ^³	∆Q= 0.332 ft ³ /sec

Required Minimum Facility Volume: 1091 ft³



Sudivision Name	Horse Creek Hi	ills									
EQ#											
County	Broadwater Co	ounty									
Location	Individual Stor	mwater Ponds									
Lot/Area No.	All Lots										
Intensity Values											
2-year, T _c	0.34	inches/hour									
2-year, 24-hour	1.24	inches									
10-year, T _c	0.76	inches/hour									
10-year, 24-hour	1.9	inches									
100-year, T _c	1.36	inches/hour									
100-year, 24-hour	2.66	inches									
Total Area/Lot Size	5.35	acres = 233046 ft^2									

Ratio	nal Method Co-Efficients (C)						
0.9	Paved/hard surfaces						
0.8	Gravel surfaces						
0.1	Lawn/landscaping						
0.2	Unimproved areas						
Q=C*i*	O=C*i*A						

Initial Stormwater Facility Volume (0.5" x Impervious Area) = 545.83 ft³

			2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Pre-Development Characteristics		(flow rate)	(volume)	(flow rate)	(volume)	(flow rate)	
Paved/House Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Gravel Area	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping	0 acres	ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area	5.35 acres	233046 ft ²	Q= 0.367 ft ³ /sec	$V = 4816.284 \text{ ft}^3$	Q= 0.820 ft ³ /sec	V= 7379.790 ft ³	Q= 1.467 ft ³ /sec
Total	5.35 acres	233046 ft ²	Q _{Total} = 0.367 ft ³ /sec	V _{Total} = 4816.284 ft ³	Q _{Total} = 0.820 ft ³ /sec	V _{Total} = 7379.790 ft ³	Q _{Total} = 1.467 ft ³ /sec

		2-year, T _c	2-year, 24-hour	10-year, T _c	10-year, 24-hour	100-year, T _c
Post-Development Characteristics		(flow rate)	volume)	(flow rate)	(volume)	(flow rate)
Paved/House Area 0.300734619 acres	13100 ft ²	Q= 0.093 ft ³ /sec	V= 1218.300 ft ³	Q= 0.207 ft ³ /sec	V= 1866.750 ft ³	Q= 0.371 ft ³ /sec
Gravel Area 0 acres	0 ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Lawn/Landscaping 0 acres	0 ft ²	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec	$V = 0.000 \text{ ft}^3$	Q= 0.000 ft ³ /sec
Unimproved Area 5.049265381 acres	219946 ft ²	Q= 0.346 ft ³ /sec	V= 4545.551 ft ³	Q= 0.774 ft ³ /sec	V= 6964.957 ft ³	Q= 1.385 ft ³ /sec
Total 5.35 acres	233046 ft ²	Q _{Total} = 0.439 ft [°] /sec	V _{Total} = 5763.851 ft ³	Q _{Total} = 0.981 ft [°] /sec	V _{Total} = 8831.707 ft ³	Q _{Total} = 1.756 ft ³ /sec

	Runoff Flow/Volume Change	∆Q= 0.072 ft ^³ /sec	∆V= 947.567 ft ^³	∆Q= 0.161 ft³/sec	ΔV= 1451.917 ft ³	ΔQ= 0.289 ft ³ /sec
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Required Minimum Facility Volume: 947.57 ft³

Appendix 3 – Culvert and Swale Sizing Calculations

Flow Data for SRT Culverts @ Sta. 93+50

(2) Two 18-in cmp culverts in parallel

1. Total Drainage Area Size

Drainage Area Size (sq. ft.) 2,661,025.00

2. Pre-development Drainage Area Characteristics:

Surface Type	Square Footage	Acres
Paved Areas	0.00	0.00
Structures	0.00	0.00
Graveled Area	0.00	0.00
Landscape	0.00	0.00
Unimproved	2,661,025.00	61.09
Total lot size	2,661,025.00	61.09

3. Post-development Drainage Area Characteristics:

Surface Type	Square Footage	Acres
Paved Areas	33,500.00	0.77
Structures	7,000.00	0.16
Graveled Area		0.00
Landscape		0.00
Unimproved	2,620,525.00	60.16
Total lot size	2,661,025.00	61.09

4. Required Initial Stormwater Facility Volume (Retained on Site)

	Cubic Feet	Acre-Feet
Retained First 0.5 inch runoff volume	1,687.50	0.04

5. Weighted Coefficient

Surface Type	Pre-Development	Post-Development
Paved Areas	0.00	0.69
Structures	0.00	0.14
Graveled Area	0.00	0.00
Landscape	0.00	0.00
Unimproved	12.22	12.03
Total Weighted Coef.	12.22	12.87
Cw	0.20	0.211

6. Flow Calculation (cfs)

M!	1.29 #NUM!
M!	9.68
M! 71	/.40

7. Volume Calculation (cf)

Flow used to size

Frequency of Storm Event	Pre-Development	Post-Development	Change (Post-Pre)
2-year	#NUM!	15,443.83	#NUM!
10-year	#NUM!	34,854.31	#NUM!
100-year	#NUM!	62,624.43	#NUM!

8. Final Required Volume

3. Post-development Hydraulic Path:

Flow Type	Surface Description	Flow Length (ft)	Land Slope (ft/ft)	Depth of Flow in Channel (in) or Culvert (in)	Channel - Top Width (ft.)	Channel - Bottom Width (ft.)	Cross Sectional Flow Area (ft^2)	Wetted Perimeter (ft)	n	Average Velocity (ft/s)	Tt (hr)	Tt (min)
Sheet	Short Grass Prairie	300	0.037						0.15	n/a	0.55	33.00
Shallow	Short-grass pasture	3184	0.064906832						0.073	1.71	0.52	31.03
Channel_Triangular	Bare Soil	303	0.01980198	24	12		12.00	24.33	0.02	6.54	0.01	0.77

4. Time of Concentration and Rainfall Intensity (24-hour storm event):

Appendix F: http://www.nrcs.usda.gov/Internet/FSE_DOCUMENTS/:

Pre-development Path

Total Time of Concentration (min)	0.00
Rainfall Intensity (in/hr), 2 Year	#NUM!
Rainfall Intensity (in/hr), 10 Year	#NUM!
Rainfall Intensity (in/hr), 100 Year	#NUM!

Post-development Path

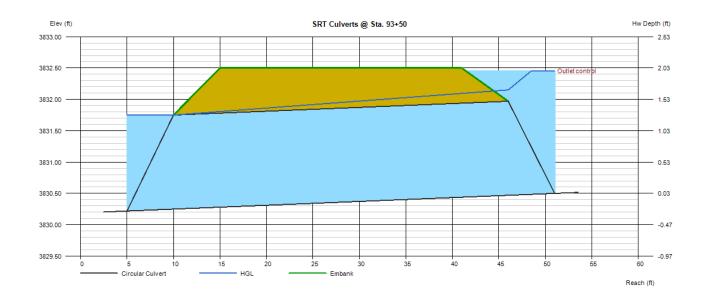
Total Time of Concentration (min)	64.81
Rainfall Intensity (in/hr), 2 Year	0.33
Rainfall Intensity (in/hr), 10 Year	0.75
Rainfall Intensity (in/hr), 100 Year	1.35

Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

SRT Culverts @ Sta. 93+50

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 3830.25 = 36.00 = 0.61 Capacity = 3830.47 = 18.0	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 1.00 = 20.00 = Normal
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 12.00
No. Barrels	= 2	Qpipe (cfs)	= 12.00
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Corrugate Metal Pipe	Veloc Dn (ft/s)	= 3.40
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 3.40
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 3831.75
		HGL Up (ft)	= 3832.15
Embankment		Hw Elev (ft)	= 3832.46
Top Elevation (ft)	= 3832.50	Hw/D (ft)	= 1.32
Top Width (ft)	= 26.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 100.00	-	



Flow Data for SRT Culvert @ Sta. 89+00

(1) One 18-in cmp culvert (Controlling Culvert for all Typical Culverts under roads in Projects 1-4, and Driveway crossings in Project 1)

1. Total Drainage Area Size

Drainage Area Size (sq. ft.)	2,023,380.00

2. Pre-development Drainage Area Characteristics:

Surface Type	Square Footage	Acres
Paved Areas	0.00	0.00
Structures	0.00	0.00
Graveled Area	0.00	0.00
Landscape	0.00	0.00
Unimproved	2,023,380.00	46.45
Total lot size	2,023,380.00	46.45

3. Post-development Drainage Area Characteristics:

Surface Type	Square Footage	Acres
Paved Areas	55,400.00	1.27
Structures	14,000.00	0.32
Graveled Area		0.00
Landscape		0.00
Unimproved	1,953,980.00	44.86
Total lot size	2,023,380.00	46.45

4. Required Initial Stormwater Facility Volume (Retained on Site)

	Cubic Feet	Acre-Feet
Retained First 0.5 inch runoff volume	2,891.67	0.07

5. Weighted Coefficient

Surface Type	Pre-Development	Post-Development
Paved Areas	0	00 1.14
Structures	0	00 0.29
Graveled Area	0	00 0.00
Landscape	0	00 0.00
Unimproved	9	29 8.97
Total Weighted Coef.	9	29 10.41
Cw	0	20 0.224

6. Flow Calculation (cfs)

Frequency of Storm Event	Pre-Development Post-Development		Change (Post-Pre)	
2-year	#NUM!	3.52	#NUM!	
10-year	#NUM!	7.88		
100-year	#NUM!	14.11		

7. Volume Calculation (cf)

Flow Used for Sizing

Frequency of Storm Event	Pre-Development	Post-Development	Change (Post-Pre)
2-year	#NUM!	12,674.12	#NUM!
10-year	#NUM!	28,358.26	#NUM!
100-year	#NUM!	50,797.20	#NUM!

3. Post-development Hydraulic Path:

Flow Type	Surface Description	Flow Length (ft)	Land Slope (ft/ft)		Depth of Flow in Channel (in) or Culvert (in)	Channel - Top Width (ft.)	Channel - Bottom Width (ft.)	Cross Sectional Flow Area (ft^2)	Wetted Perimeter (ft)	n	Average Velocity (ft/s)	Tt (hr)	Tt (min)
Sheet	Short Grass Prairie	300	0.037	15	10	12				0.15	n/a	0.55	33.00
Shallow	Short-grass pasture	3220	0.049689441							0.073	1.50	0.60	35.87
Channel_Triangular	Bare Soil	660	0.060606061		24	12		12.00	24.33	0.02	11.45	0.02	0.96
	Appendix F: http://www.ncs.usda.gov/Internet/F3						v/Internet/FSE_						

4. Time of Concentration and Rainfall Intensity (24-hour storm event):

Pre-development Path

Total Time of Concentration (min)	0.00
Rainfall Intensity (in/hr), 2 Year	#NUM!
Rainfall Intensity (in/hr), 10 Year	#NUM!
Rainfall Intensity (in/hr), 100 Year	#NUM!

Post-development Path

DEQ Page 240

Total Time of Concentration (min)	69.83
Rainfall Intensity (in/hr), 2 Year	0.34
Rainfall Intensity (in/hr), 10 Year	0.76
Rainfall Intensity (in/hr), 100 Year	1.36

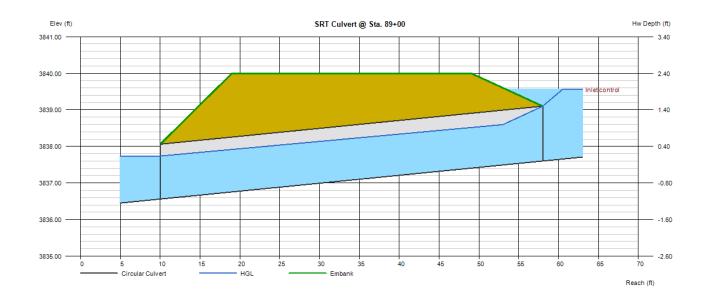
Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Tuesday, Mar 24 2020

SRT Culvert @ Sta. 89+00

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 3836.56 = 48.00 = 2.17 = 3837.60 = 18.0	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 1.00 = 10.00 = Normal
Shape	= Circular	Highlighted	
Span (in)	= 18.0	Qtotal (cfs)	= 8.00
No. Barrels	= 1	Qpipe (cfs)	= 8.00
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Corrugate Metal Pipe	Veloc Dn (ft/s)	= 5.38
Culvert Entrance	= Projecting	Veloc Up (ft/s)	= 5.79
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9	HGL Dn (ft)	= 3837.74
		HGL Up (ft)	= 3838.70
Embankment		Hw Elev (ft)	= 3839.56
Top Elevation (ft)	= 3840.00	Hw/D (ft)	= 1.31
Top Width (ft)	= 30.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 100.00	-	



Flow Data for APT Driveway Culvert @ Sta. 11+50

(1) One 15-in CMP Culvert (Controlling Driveway Culvert for Projects #2-4) **1. Total Drainage Area Size**

2. Pre-development Drainage Area Characteristics:

Surface Type	Square Footage	Acres
Paved Areas	0.00	0.00
Structures	0.00	0.00
Graveled Area	0.00	0.00
Landscape	0.00	0.00
Unimproved	143,401.00	3.29
Total lot size	143,401.00	3.29

3. Post-development Drainage Area Characteristics:

Surface Type	Square Footage	Acres
Paved Areas	16,780.00	0.39
Structures	0.00	0.00
Graveled Area		0.00
Landscape		0.00
Unimproved	126,621.00	2.91
Total lot size	143,401.00	3.29

4. Required Initial Stormwater Facility Volume (Retained on Site)

	Cubic Feet	Acre-Feet
Retained First 0.5 inch runoff volume	699.17	0.02

5. Weighted Coefficient

Surface Type	Pre-Development	Post-Development
Paved Areas	0.00	0.35
Structures	0.00	0.00
Graveled Area	0.00	0.00
Landscape	0.00	0.00
Unimproved	0.66	0.58
Total Weighted Coef.	0.66	0.93
Cw	0.20	0.282

6. Flow Calculation (cfs)

Frequency of Storm Event	Pre-Development	nent Post-Development Change (l	
2-year	#NUM!	0.46	#NUM!
10-year	#NUM!	1.05	
100-year	#NUM!	7 1.90	

7. Volume Calculation (cf)

Flow used for Sizing

Frequency of Storm Event	Pre-Development	Post-Development	Change (Post-Pre)
2-year	#NUM!	1,662.09	#NUM!
10-year	#NUM!	3,792.98	#NUM!
100-year	#NUM!	6,841.60	#NUM!

8. Final Required Volume

3. Post-development Hydraulic Path:

Flow Type	Surface Description	Flow Length (ft)	Land Slope (ft/ft)		Depth of Flow in Channel (in) or Culvert (in)	Channel - Top Width (ft.)	Channel - Bottom Width (ft.)	Cross Sectional Flow Area (ft^2)	Wetted Perimeter (ft)	n	Average Velocity (ft/s)	Tt (hr)	Tt (min)
Sheet	Short Grass Prairie	300	0.046666667							0.15	n/a	0.50	30.08
Shallow	Short-grass pasture	150	0.066666667							0.073	1.73	0.02	1.44
Channel_Triangular	Bare Soil	890	0.039325843		24	12		12.00	24.33	0.02	9.22	0.03	1.61
	Appendix F: http://www.ncs.usda.gov/Internet/FS						v/Internet/FSE_						

4. Time of Concentration and Rainfall Intensity (24-hour storm event):

Pre-development Path

Total Time of Concentration (min)	0.00
Rainfall Intensity (in/hr), 2 Year	#NUM!
Rainfall Intensity (in/hr), 10 Year	#NUM!
Rainfall Intensity (in/hr), 100 Year	#NUM!

Post-development Path

Total Time of Concentration (min)	33.13
Rainfall Intensity (in/hr), 2 Year	0.50
Rainfall Intensity (in/hr), 10 Year	1.14
Rainfall Intensity (in/hr), 100 Year	2.06

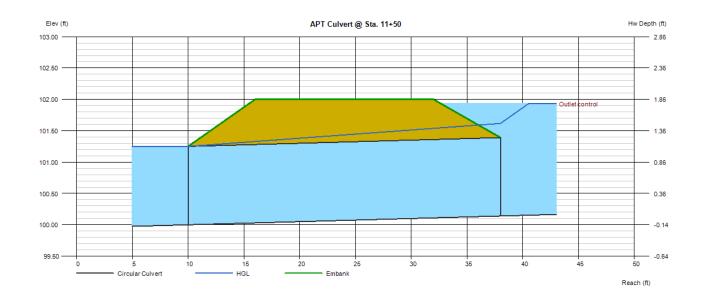
Culvert Report

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Tuesday, Mar 24 2020

APT Driveway Culvert @ Sta. 11+50

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 100.00 = 28.00 = 0.50 = 100.14 = 15.0	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 1.00 = 10.00 = Normal
Shape	= Circular	Highlighted	
Span (in)	= 15.0	Qtotal (cfs)	= 4.00
No. Barrels	= 1 Capacity	Qpipe (cfs)	= 4.00
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	 Circular Corrugate Metal Pipe 	Veloc Dn (ft/s)	= 3.26
Culvert Entrance	= Projecting	Veloc Up (ft/s)	= 3.26
Coeff. K,M,c,Y,k	= 0.034, 1.5, 0.0553, 0.54, 0.9	HGL Dn (ft)	= 101.25
		HGL Up (ft)	= 101.62
Embankment		Hw Elev (ft)	= 101.93
Top Elevation (ft)	= 102.00	Hw/D (ft)	= 1.43
Top Width (ft)	= 16.00	Flow Regime	= Outlet Control
Crest Width (ft)	= 100.00		



Flow Data for SRT Culvert @ Sta. 3+25

(1) One 36-in cmp culvert (Controlling Culvert for all Existing drainage gully crossings in Projects 1-4)

1. Total Drainage Area Size

Drainage Area Size (sq. ft.)	2,612,765.00

2. Pre-development Drainage Area Characteristics:

Surface Type	Square Footage	Acres
Paved Areas	0.00	0.00
Structures	0.00	0.00
Graveled Area	0.00	0.00
Landscape	0.00	0.00
Unimproved	2,612,765.00	59.98
Total lot size	2,612,765.00	59.98

3. Post-development Drainage Area Characteristics:

Surface Type	Square Footage	Acres
Paved Areas	138,624.00	3.18
Structures	21,000.00	0.48
Graveled Area		0.00
Landscape		0.00
Unimproved	2,453,141.00	56.32
Total lot size	2,612,765.00	59.98

4. Required Initial Stormwater Facility Volume (Retained on Site)

	Cubic Feet	Acre-Feet
Retained First 0.5 inch runoff volume	6,651.00	0.15

5. Weighted Coefficient

Surface Type	Pre-Development	Post-Development
Paved Areas	0.00	2.86
Structures	0.00	0.43
Graveled Area	0.00	0.00
Landscape	0.00	0.00
Unimproved	12.00	11.26
Total Weighted Coef.	12.00	14.56
Cw	0.20	0.243

6. Flow Calculation (cfs)

Frequency of Storm Event	Pre-Development	Post-Development	Change (Post-Pre)
2-year	#NUM!	5.22	#NUM!
10-year	#NUM!	11.91	
100-year	#NUM!	21.49	

7. Volume Calculation (cf)

Flow used for Sizing

∕∖

Frequency of Storm Event	Pre-Development	Post-Development	Change (Post-Pre)
2-year	#NUM!	18,795.02	#NUM!
10-year	#NUM!	42,891.23	#NUM!
100-year	#NUM!	77,365.11	#NUM!

3. Post-development Hydraulic Path:

Flow Type	Surface Description	Flow Length (ft)	Land Slope (ft/ft)	Culvert Diameter (in)	Depth of Flow in Channel (in) or Culvert (in)	Channel - Top Width (ft.)	Channel - Bottom Width (ft.)	Cross Sectional Flow Area (ft^2)	Wetted Perimeter (ft)	n	Average Velocity (ft/s)	Tt (hr)	Tt (min)
Sheet	Short Grass Prairie	300	0.05	15	10	12				0.15	n/a	0.49	29.26
Shallow	Short-grass pasture	2264	0.065812721							0.073	1.72	0.37	21.91
•	Appendix F: http://www.nrcs.usda.gov/internet/FSE						v/Internet/FSE_						

4. Time of Concentration and Rainfall Intensity (24-hour storm event):

Pre-development Path

rie-development ratii	
Total Time of Concentration (min)	0.00
Rainfall Intensity (in/hr), 2 Year	#NUM!
Rainfall Intensity (in/hr), 10 Year	#NUM!
Rainfall Intensity (in/hr), 100 Year	#NUM!

Post-development Path

Total Time of Concentration (min)	51.17
Rainfall Intensity (in/hr), 2 Year	0.36
Rainfall Intensity (in/hr), 10 Year	0.82
Rainfall Intensity (in/hr), 100 Year	1.48

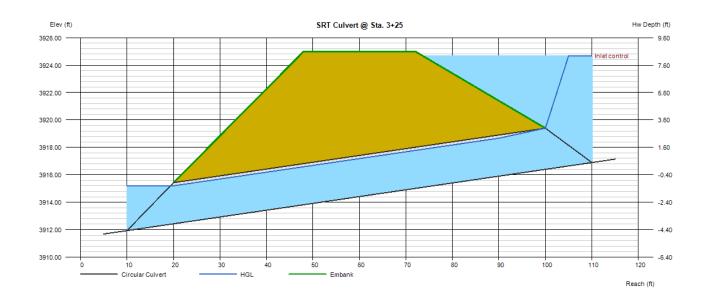
Culvert Report

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SRT Culvert @ Sta. 3+25

Invert Elev Dn (ft) Pipe Length (ft) Slope (%) Invert Elev Up (ft) Rise (in)	= 3912.43 = 80.00 = 4.96 = 3916.40 = 36.0	Calculations Qmin (cfs) Qmax (cfs) Tailwater Elev (ft)	= 5.00 = 100.00 = Normal
Shape	= Circular	Highlighted	
Span (in)	= 36.0	Qtotal (cfs)	= 80.00
No. Barrels	= 1	Qpipe (cfs)	= 80.00
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Corrugate Metal Pipe	Veloc Dn (ft/s)	= 11.73
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 11.73
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 3915.20
		HGL Up (ft)	= 3919.17
Embankment		Hw Elev (ft)	= 3924.69
Top Elevation (ft)	= 3925.00	Hw/D (ft)	= 2.76
Top Width (ft)	= 24.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 300.00		



Flow Data for Lower Confederate Road Crossing

(2) Two 24-in cmp culverts in parallel - sized for existing crossing 1. Total Drainage Area Size

Drainage Area Size (sq. ft.)

2. Pre-development Drainage Area Characteristics:

Surface Type	Square Footage	Acres
Paved Areas	0.00	0.00
Structures	0.00	0.00
Graveled Area	0.00	0.00
Landscape	0.00	0.00
Unimproved	3,816,615.00	87.62
Total lot size	3,816,615.00	87.62

3. Post-development Drainage Area Characteristics:

Surface Type	Square Footage	Acres
Paved Areas	138,624.00	3.18
Structures	21,000.00	0.48
Graveled Area		0.00
Landscape		0.00
Unimproved	3,656,991.00	83.95
Total lot size	3,816,615.00	87.62

4. Required Initial Stormwater Facility Volume (Retained on Site)

	Cubic Feet	Acre-Feet
Retained First 0.5 inch runoff volume	6,651.00	0.15

5. Weighted Coefficient

Surface Type	Pre-Development	Post-Development
Paved Areas	0.00	2.86
Structures	0.00	0.43
Graveled Area	0.00	0.00
Landscape	0.00	0.00
Unimproved	17.52	16.79
Total Weighted Coef.	17.52	20.09
Cw	0.20	0.229

6. Flow Calculation (cfs)

Frequency of Storm Event		Pre-Development	Post-Development	Change (Post-Pre)	
2-year		#NUM!	6.63	#NUM!	
10-year		#NUM!	15.06		
100-year		#NUM!	27.10	1	
7 Volume Calculation (cf)	Flov	w used for Sizing			

7. Volume Calculation (cf)

Frequency of Storm Event	Pre-Development	Post-Development	Change (Post-Pre)
2-year	#NUM!	23,884.40	#NUM!
10-year	#NUM!	54,198.40	#NUM!
100-year	#NUM!	97,567.93	#NUM!

8. Final Required Volume

3. Post-development Hydraulic Path:

Flow Type	Surface Description	Flow Length (ft)	Land Slope (ft/ft)	Culvert Diameter (in)	Depth of Flow in Channel (in) or Culvert (in)	Channel - Top Width (ft.)	Channel - Bottom Width (ft.)	Cross Sectional Flow Area (ft^2)	Wetted Perimeter (ft)	n	Average Velocity (ft/s)	Tt (hr)	Tt (min)
Sheet	Short Grass Prairie	300	0.05							0.15	n/a	0.49	29.26
Shallow	Short-grass pasture	3080	0.055194805							0.073	1.58	0.54	32.55

4. Time of Concentration and Rainfall Intensity (24-hour storm event):

Appendix F: http://www.nrcs.usda.gov/Internet/FSE_

Pre-development Path

Total Time of Concentration (min)	0.00
Rainfall Intensity (in/hr), 2 Year	#NUM!
Rainfall Intensity (in/hr), 10 Year	#NUM!
Rainfall Intensity (in/hr), 100 Year	#NUM!

Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Tuesday, Mar 24 2020

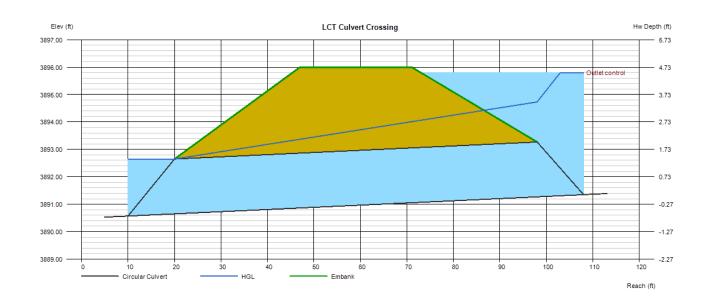
Lower Confederate Road Culvert Crossing

Invert Elev Dn (ft) Pipe Length (ft) Slope (%)	= 3890.65 = 78.00 = 0.80	Calculations Qmin (cfs) Qmax (cfs)	= 5.00 = 100.00
Invert Elev Up (ft)	= 3891.27 Capacity	Tailwater Elev (ft)	= Normal
Rise (in)	= 24.0	N	
Shape	= Circular	Highlighted	
Span (in)	= 24.0	Qtotal (cfs)	= 40.00
No. Barrels	= 2	Qpipe (cfs)	= 40.00
n-Value	= 0.024	Qovertop (cfs)	= 0.00
Culvert Type	= Circular Corrugate Metal Pipe	Veloc Dn (ft/s)	= 6.37
Culvert Entrance	= Mitered to slope (C)	Veloc Up (ft/s)	= 6.37
Coeff. K,M,c,Y,k	= 0.021, 1.33, 0.0463, 0.75, 0.7	HGL Dn (ft)	= 3892.65
		HGL Up (ft)	= 3894.73
Embankment		Hw Elev (ft)	= 3895.80
Top Elevation (ft)	= 3896.00	Hw/D (ft)	= 2.27
Top Width (ft)	= 24.00	Flow Regime	= Outlet Cont

Crest Width (ft)

24.00 = 400.00

	Υ.	,	
4	Highlighted		
	Qtotal (cfs)	=	40.00
	Qpipe (cfs)	=	40.00
	Qovertop (cfs)	=	0.00
l Pipe	Veloc Dn (ft/s)	=	6.37
	Veloc Up (ft/s)	=	6.37
5, 0.7	HGL Dn (ft)	=	3892.65
	HGL Up (ft)	=	3894.73
	Hw Elev (ft)	=	3895.80
	Hw/D (ft)	=	2.27
	Flow Regime	=	Outlet Control



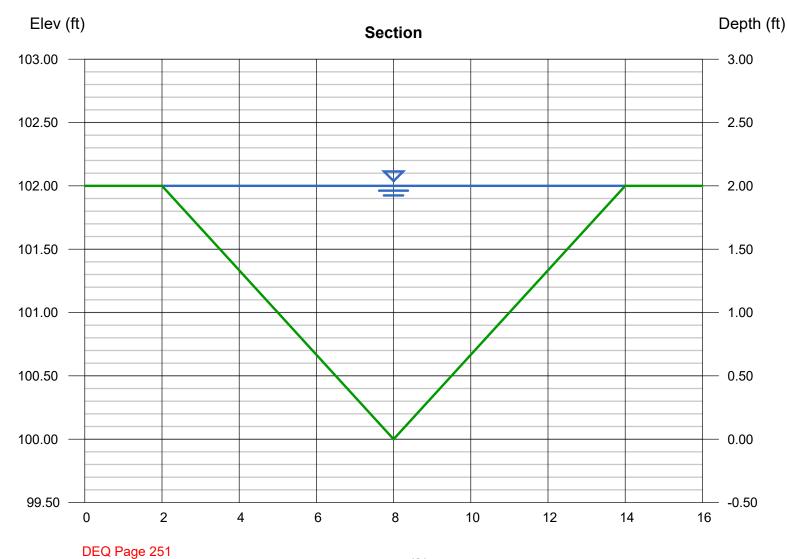
Channel Report

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Tuesday, Mar 24 2020

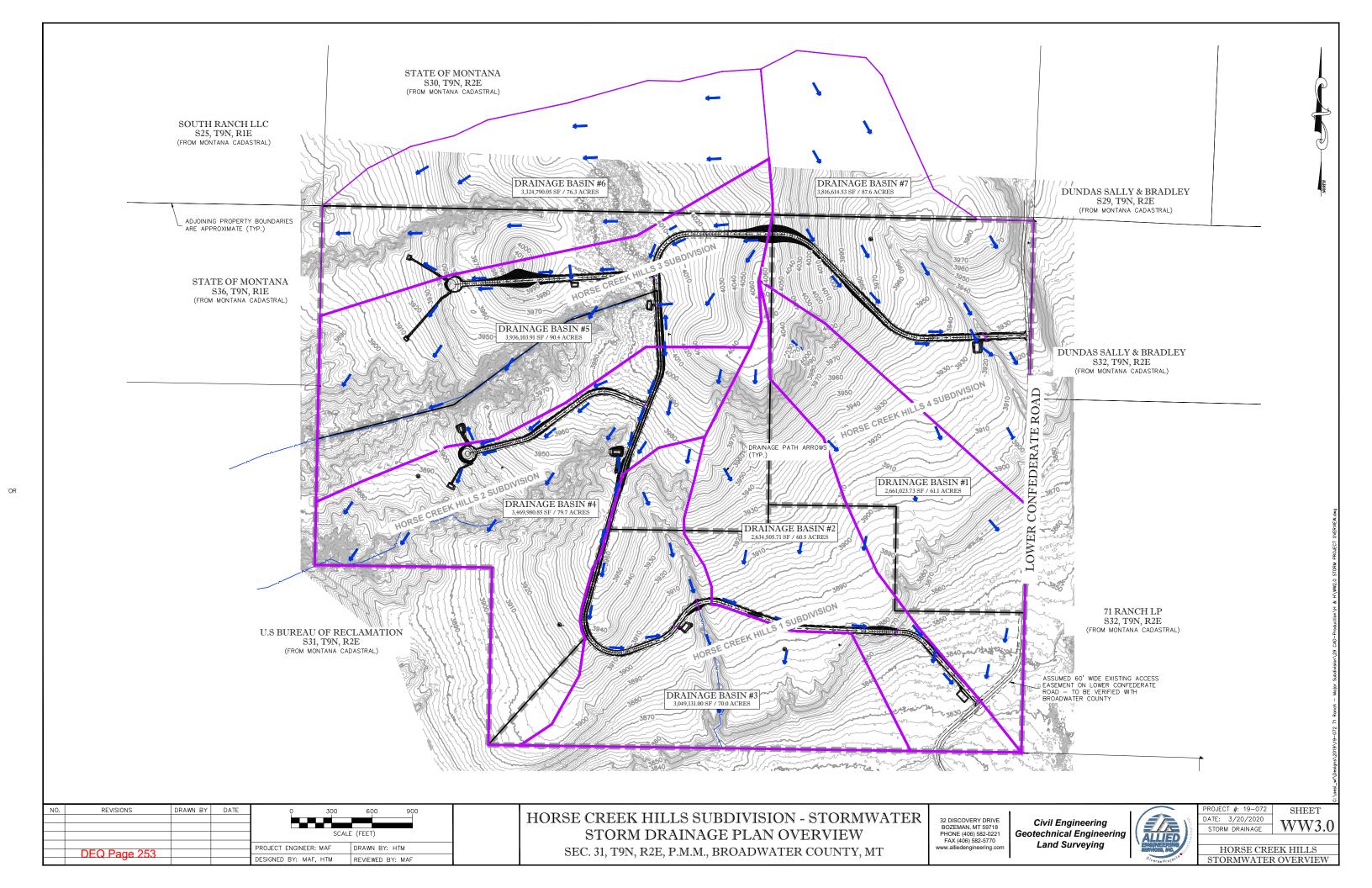
Typical Swale

2.00
48.70
12.00
4.06
12.65
1.75
12.00
2.26



Reach (ft)

Appendix 4 – Stormwater Plans



		S	FRAWBE	RRY ROA	AN TRAIL			
SEGMENT ID #	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHIN & EASTING
L189	0+00.00	826,482.1902; 1,461,639.8195	N/A	755.72	S88° 27′ 40.34"W	N/A	7+55.72	826,461.8963; 1,460,884.3754
C1	7+55.72	826,461.8963; 1,460,884.3754	400.00	342.99	N66 58 24.92 W	N/A	10+98.71	826,591.9879; 1460578.2912
L190	10+98.71	826,591.9879; 1,460,578.2912	N/A	735.22	N44 19' 15.89"W	N/A	18+33.93	827,117.9894; 1,460,064.6099
C2	18+33.93	827,117.9894; 1,460,064.6099	400.00	298.01	N65 39 52.42"W	N/A	21+31.94	827,237.9727; 1459799.3139
L191	21+31.94	827,237.9727; 1,459,799.3139	N/A	674.27	S89° 58' 32.43"W	N/A	28+06.21	827,237.6864; 1,459,125.0454
C3	28+06.21	827,237.6864; 1,459,125.0454	250.00	391.59	S45' 06' 11.21"W	N/A	31+97.80	826,988.6924; 1458875.1535
L192	31+97.80	826,988.6924; 1,458,875.1535	N/A	708.07	S3 00' 48.58"E	N/A	39+05.86	826,281.6037; 1,458,912.3774
C4	39+05.86	826,281.6037; 1,458,912.3774	300.00	127.11	S9°03'11.56"W	N/A	40+32.97	826,157.0147; 1458892.5259
L193	40+32.97	826,157.0147; 1,458,892.5259	N/A	653.61	S21 11 28.51"W	N/A	46+86.58	825,547.6048; 1,458,656.2583
C5	46+86.58	825,547.6048; 1,458,656.2583	250.00	25.34	S18 17' 13.31"W	N/A	47+11.93	825,523.5509; 1458648.3093
L194	47+11.93	825,523.5509; 1,458,648.3093	N/A	1,123.31	S15°22′58.11"W	N/A	58+35.23	824,440.4879; 1,458,350.3337
C6	58+35.23	824,440.4879; 1,458,350.3337	250.00	544.51	S47 00' 47.37"E	N/A	63+79.74	824,138.3787; 1458674.4553
L195	63+79.74	824,138.3787; 1,458,674.4553	N/A	232.07	N70° 35' 27.16"E	N/A	66+11.81	824,215.4972; 1,458,893.3338
C7	66+11.81	824,215.4972; 1,458,893.3338	250.00	153.67	N52 58 54.92"E	N/A	67+65.47	824,306.5655; 1459014.1063
L196	67+65.47	824,306.5655; 1,459,014.1063	N/A	117.56	N35°22′22.69″E	N/A	68+83.03	824,402.4253; 1,459,082.1623
C8	68+83.03	824,402.4253; 1,459,082.1623	250.00	323.94	N72°29'36.32"E	N/A	72+06.97	824,493.1952; 1459369.9324
L197	72+06.97	824,493.1952; 1,459,369.9324	N/A	511.62	S70° 23' 10.05"E	N/A	77+18.59	824,321.4557; 1,459,851.8638
C9	77+18.59	824,321.4557; 1,459,851.8638	250.00	75.58	S79 02' 48.73"E	N/A	77+94.17	824,307.1498; 1459925.7840
L198	77+94.17	824,307.1498; 1,459,925.7840	N/A	777.91	S87* 42' 27.42"E	N/A	85+72.08	824,276.0342; 1,460,703.0703
C10	85+72.08	824,276.0342; 1,460,703.0703	250.00	199.23	S64 52 38.91"E	N/A	87+71.31	824,193.6704; 1460878.7185
L199	87+71.31	824,193.6704; 1.460.878.7185	N/A	605.19	S42 03 14.75 E	N/A	93+76.50	823,744.3085; 1.461.284.0946

NO.

			APPA	LOOSA	ΓRAIL			
EGMENT ID#	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L200	0+00.00	825,957.8812; 1,458,815.3220	N/A	254.84	N68 48 31.49"W	N/A	2+54.84	826,050.0031; 1,458,577.7099
L203	0+00.00	825,957.8812; 1,458,815.3220	N/A	254.84	N68° 48' 31.49"W	N/A	2+54.84	826,050.0031; 1,458,577.7099
C11	2+54.84	826,050.0031; 1,458,577.7099	250.00	250.90	S82 26' 26.76"W	N/A	5+05.74	826,018.3653; 1458339.3019
C13	2+54.84	826,050.0031; 1,458,577.7099	250.00	250.90	S82 26' 26.76"W	N/A	5+05.74	826,018.3653; 1458339.3019
L201	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53° 41' 25.01"W	N/A	9+64.33	825,746.8117; 1,457,969.7578
L204	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53 41' 25.01"W	N/A	9+64.33	825,746.8117; 1,457,969.7578
C12	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64 49 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
C14	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64 49 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
L202	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75 57 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
L205	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75° 57′ 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
				1 0337 8 1 1	ENODTH			
EGMENT ID#	START STATION		RADIUS [FT]	LENGTH [FT]	E NORTH LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L207	0+00.00	825,638.2166; 1,457,536.3127	N/A	2.86	N82° 46′ 27.03″W	N/A	0+02.86	825,638.5769; 1,457,533.4707
L208	0+02.86	825,638.5769; 1,457,533.4707	N/A	3.09	N59°05'34.29"W	N/A	0+05.95	825,640.1618; 1,457,530.8234
L209	0+05.95	825,640.1618; 1,457,530.8234	N/A	12.89	N43' 59' 30.64"W	N/A	0+18.84	825,649.4369; 1,457,521.8690
L210	0+18.84	825,649.4369; 1,457,521.8690	N/A	3.41	N43° 59′ 30.64"W	N/A	0+22.25	825,651.8888; 1,457,519.5019
L211	0+22.25	825,651.8888; 1,457,519.5019	N/A	0.44	N90° 00' 00.00"W	N/A	0+22.69	825,651.8888; 1,457,519.0603
L212	0+22.69	825,651.8888; 1,457,519.0603	N/A	19.42	N57° 58' 04.11"W	N/A	0+42.12	825,662.1907; 1,457,502.5944
L213	0+42.12	825,662.1907; 1.457.502.5944	N/A	106.03	N35°14'27.11"W	N/A	1+48.15	825,748.7927; 1.457.441.4109
L214	1+48.15	825,748.7927; 1,457,441.4109	N/A	86.24	N17° 26' 26.64"W	N/A	2+34.39	825,831.0663; 1,457,415.5637
			· · · · ·					
					LE SOUTH			
SEGMENT ID #	Γ START STATION	START NORTHING & EASTING	RADIUS [FT]	E LENGTH	I LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L215	0+00.00	825,608.4328; 1,457,567.4019	N/A	12.52	S70°26′48.72″W	V N/A	0+12.52	825,604.2412; 1,457,555.6000
L216	0+12.52	825,604.2412; 1,457,555.6000	N/A	28.25	S27° 40' 18.04"W	/ N/A	0+40.77	825,579.2224; 1,457,542.4806
L217	0+40.77	825,579.2224; 1,457,542.4806	N/A	19.89	528' 26' 49.91"W	/ N/A	0+60.66	825,561.7344; 1,457,533.0062
L218	0+60.66	825,561.7344; 1,457,533.0062	N/A	16.83	S40° 09' 35.39"W	V N/A	0+77.50	825,548.8707; 1,457,522.1510
L219	0+77.50	825,548.8707; 1,457,522.1510	N/A	19.21	S39° 58' 28.96"W	V N/A	0+96.70	825,534.1519; 1,457,509.8116
L220	0+96.70	825,534.1519; 1,457,509.8116	N/A	54.21	S64' 59' 00.52"W	V N/A	1+50.92	825,511.2259; 1,457,460.6836
L221	1+50.92	825,511.2259; 1,457,460.6836	N/A	44.40	S66' 03' 31.98"W	V N/A	1+95.32	825,493.2081; 1,457,420.1029
L222	1+95.32	825,493.2081; 1,457,420.1029	N/A	175.28	S30' 10' 36.13"W	/ N/A	3+70.60	825,341.6834; 1,457,331.9958
	<u> </u>		-1	-1	-1		1	1
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		BDIVISIO		-	IWATER	BOZE	COVERY DRIVE MAN, MT 59718	Civil Engin
LIGN	MENT CO	ORDINAT	ЕТА	BLES		FAX	E (406) 582-0221 (406) 582-5770 edengineering.com	Geotechnical E Land Surv
		BROADWAT						

		1		LOOSA 1	1	1	1	
GMENT ID#	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L200	0+00.00	825,957.8812; 1,458,815.3220	N/A	254.84	N68 48 31.49 W	N/A	2+54.84	826,050.0031; 1,458,577.7099
L203	0+00.00	825,957.8812; 1,458,815.3220	N/A	254.84	N68 48 31.49 W	N/A	2+54.84	826,050.0031; 1,458,577.7099
C11	2+54.84	826,050.0031; 1,458,577.7099	250.00	250.90	S82 26' 26.76"W	N/A	5+05.74	826,018.3653; 1458339.3019
C13	2+54.84	826,050.0031; 1,458,577.7099	250.00	250.90	S82* 26' 26.76"W	N/A	5+05.74	826,018.3653; 1458339.3019
L201	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53° 41' 25.01"W	N/A	9+64.33	825,746.8117; 1,457,969.7578
L204	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53° 41′ 25.01″W	N/A	9+64.33	825,746.8117; 1,457,969.7578
C12	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64° 49' 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
C14	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64 49 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
L202	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75° 57' 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
L205	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75° 57' 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
				1 SWALI	ENORTH			
EGMENT ID #	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L207	0+00.00	825,638.2166; 1,457,536.3127	N/A	2.86	N82 46 27.03 W	N/A	0+02.86	825,638.5769; 1,457,533.4707
L208	0+02.86	825,638.5769; 1,457,533.4707	N/A	3.09	N59'05'34.29"W	N/A	0+05.95	825,640.1618; 1,457,530.8234
L209	0+05.95	825,640.1618; 1,457,530.8234	N/A	12.89	N43 59 30.64"W	N/A	0+18.84	825,649.4369; 1,457,521.8690
L210	0+18.84	825,649.4369; 1,457,521.8690	N/A	3.41	N43 59 30.64"W	N/A	0+22.25	825,651.8888; 1,457,519.5019
L211	0+22.25	825,651.8888; 1,457,519.5019	N/A	0.44	N90°00'00.00"W	N/A	0+22.69	825,651.8888; 1,457,519.0603
L212	0+22.69	825,651.8888; 1,457,519.0603	N/A	19.42	N57 58' 04.11"W	N/A	0+42.12	825,662.1907; 1,457,502.5944
L213	0+42.12	825,662.1907; 1,457,502.5944	N/A	106.03	N35°14'27.11"W	N/A	1+48.15	825,748.7927; 1,457,441.4109
L214	1+48.15	825,748.7927; 1,457,441.4109	N/A	86.24	N17' 26' 26.64"W	N/A	2+34.39	825,831.0663; 1,457,415.5637
		A	PT PON	D 2 SWAI	LE SOUTH			
SEGMENT ID #	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L215	0+00.00	825,608.4328; 1,457,567.4019	N/A	12.52	S70' 26' 48.72"W	N/A	0+12.52	825,604.2412; 1,457,555.6000
L216	0+12.52	825,604.2412;	N/A	28.25	S27° 40' 18.04"W	N/A	0+40.77	825,579.2224; 1,457,542.4806
L217	0+40.77	1,457,555.6000 825,579.2224;	N/A	19.89	S28* 26' 49.91"W	N/A	0+60.66	825,561.7344;
L218	0+60.66	1,457,542.4806 825,561.7344;	N/A	16.83	S40° 09' 35.39"W	N/A	0+77.50	1,457,533.0062 825,548.8707;
L219	0+77.50	1,457,533.0062 825,548.8707;	N/A	19.21	S39' 58' 28.96"W	N/A	0+96.70	1,457,522.1510 825,534.1519;
L220	0+96.70	1,457,522.1510 825,534.1519;	N/A	54.21	S64' 59' 00.52"W	N/A	1+50.92	1,457,509.8116 825,511.2259;
L220	1+50.92	1,457,509.8116	N/A	44.40	S66' 03' 31.98"W	N/A	1+95.32	1,457,460.6836 825,493.2081;
		1,457,460.6836 825,493.2081;	,					1,457,420.1029 825,341.6834;
L222	1+95.32	1,457,420.1029	N/A	175.28	S30' 10' 36.13"W	N/A	3+70.60	1,457,331.9958

EGMENT				LOOSA	1		1	1
ID#	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L200	0+00.00	825,957.8812; 1,458,815.3220	N/A	254.84	N68 48 31.49"W	N/A	2+54.84	826,050.0031; 1,458,577.7099
L203	0+00.00	825,957.8812; 1,458,815.3220	N/A	254.84	N68 48 31.49"W	N/A	2+54.84	826,050.0031; 1,458,577.7099
C11	2+54.84	826,050.0031; 1,458,577.7099	250.00	250.90	S82 26' 26.76"W	N/A	5+05.74	826,018.3653; 1458339.3019
C13	2+54.84	826,050.0031; 1,458,577.7099	250.00	250.90	S82 26 26.76"W	N/A	5+05.74	826,018.3653; 1458339.3019
L201	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53° 41' 25.01"W	N/A	9+64.33	825,746.8117; 1,457,969.7578
L204	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53° 41′ 25.01″W	N/A	9+64.33	825,746.8117; 1,457,969.7578
C12	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64 49 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
C14	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64 49 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
L202	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75 57 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
L205	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75° 57′ 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
					ENORTH			
EGMENT ID #	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L207	0+00.00	825,638.2166; 1,457,536.3127	N/A	2.86	N82°46′27.03″W	N/A	0+02.86	825,638.5769; 1,457,533.4707
L208	0+02.86	825,638.5769; 1,457,533.4707	N/A	3.09	N59'05'34.29"W	N/A	0+05.95	825,640.1618; 1,457,530.8234
L209	0+05.95	825,640.1618; 1,457,530.8234	N/A	12.89	N43 59 30.64"W	N/A	0+18.84	825,649.4369; 1,457,521.8690
L210	0+18.84	825,649.4369; 1,457,521.8690	N/A	3.41	N43 59 30.64"W	N/A	0+22.25	825,651.8888; 1,457,519.5019
L211	0+22.25	825,651.8888; 1,457,519.5019	N/A	0.44	N90° 00' 00.00"W	N/A	0+22.69	825,651.8888; 1,457,519.0603
L212	0+22.69	825,651.8888; 1,457,519.0603	N/A	19.42	N57 58 04.11"W	N/A	0+42.12	825,662.1907; 1,457,502.5944
L213	0+42.12	825,662.1907; 1,457,502.5944	N/A	106.03	N35°14′27.11"W	N/A	1+48.15	825,748.7927; 1,457,441.4109
L214	1+48.15	825,748.7927; 1,457,441.4109	N/A	86.24	N17' 26' 26.64"W	N/A	2+34.39	825,831.0663; 1,457,415.5637
		А	PT PON	D 2 SWAI	LE SOUTH			
SEGMENT	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L215	0+00.00	825,608.4328;	N/A	12.52	S70' 26' 48.72"W	/ N/A	0+12.52	825,604.2412;
L216	0+12.52	1,457,567.4019 825,604.2412;	N/A	28.25	S27° 40' 18.04"W	+	0+40.77	1,457,555.6000 825,579.2224;
L210	0+40.77	1,457,555.6000 825,579.2224;	N/A	19.89	S28' 26' 49.91"W		0+60.66	1,457,542.4806 825,561.7344;
L217	0+60.66	1,457,542.4806 825,561.7344;	N/A	16.83	S40° 09' 35.39"W		0+77.50	1,457,533.0062 825,548.8707;
		1,457,533.0062 825,548.8707;	,					1,457,522.1510 825,534.1519;
L219	0+77.50	1,457,522.1510 825,534.1519;	N/A	19.21	S39' 58' 28.96"W		0+96.70	1,457,509.8116 825,511.2259;
	0+96.70	1,457,509.8116 825,511.2259;	N/A	54.21	S64' 59' 00.52"W		1+50.92	1,457,460.6836 825,493.2081;
L220	1+50.92	825,493.2081;	N/A N/A	44.40	S66°03'31.98"W	+	1+95.32	825,341.6834;
L220 L221 L222	1+95.32			175.28	S30' 10' 36.13"W	N/A	3+70.60	

REVISIONS	DRAWN BY	DATE				
					HORSE CREEK HILLS SUBDIVISION - STORMWATER	32 DISC
					ALIGNMENT COORDINATE TABLES	BOZEM/ PHONE
					ALIGINMENT COORDINATE TABLES	FAX (4
DEQ Page 254			PROJECT ENGINEER: MAF	DRAWN BY: HTM	SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT	www.allied
DEQ Fage 204			DESIGNED BY: MAF, HTM	REVIEWED BY: MAF		

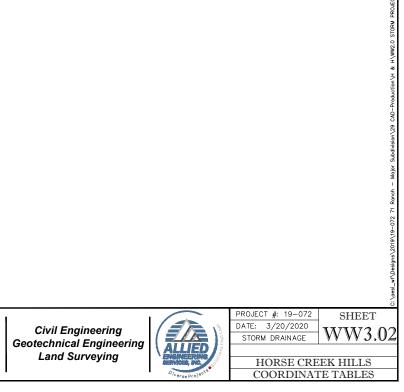


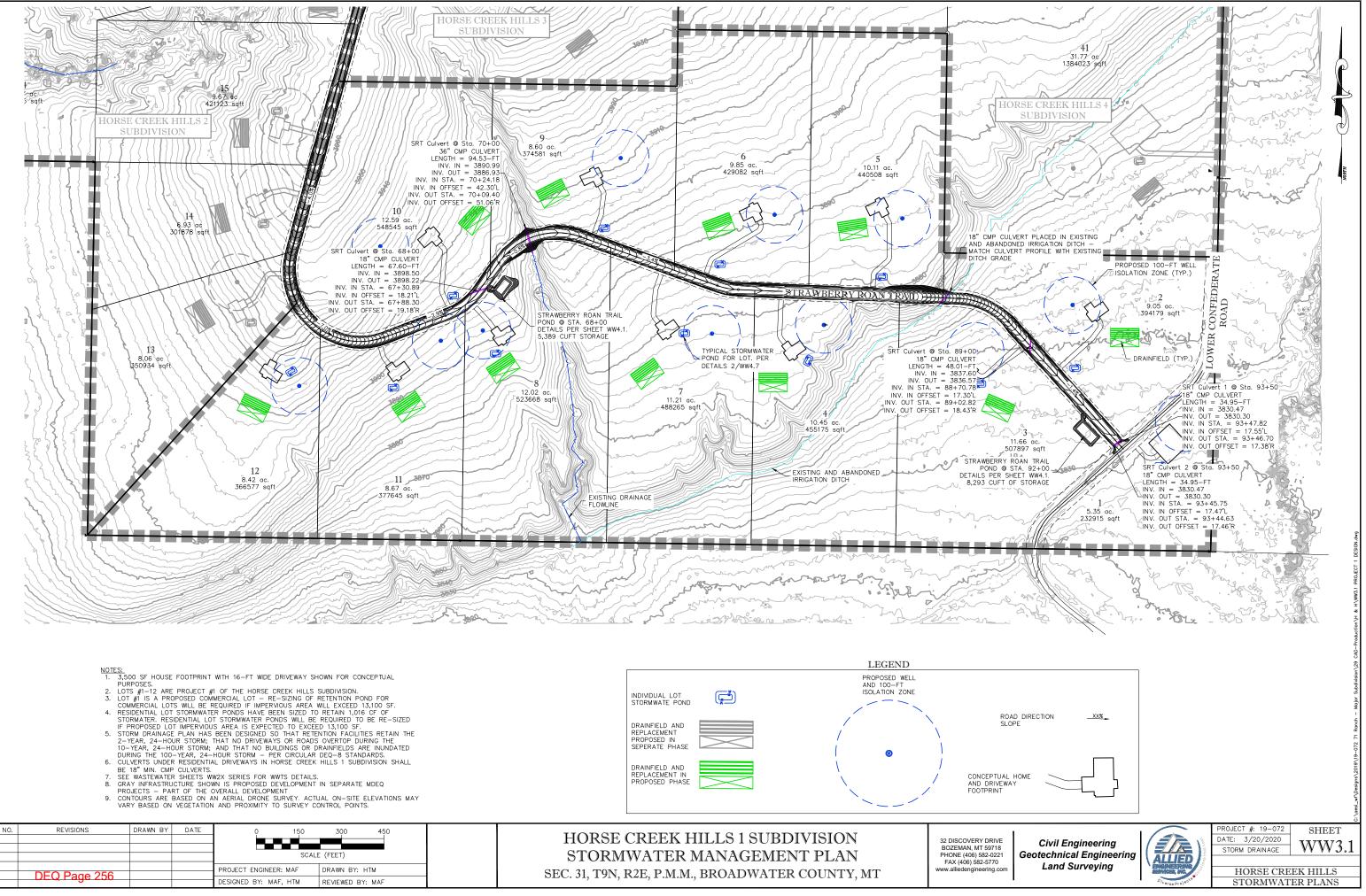
	BUCKSKIN TRAIL									
SEGMENT ID#	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHIN & EASTING		
L206	0+00.00	826,943.5358; 1,458,877.5307	N/A	1,500.00	S86° 54' 54.60"W	N/A	15+00.00	826,862.8140; 1,457,379.7043		

		B	ST PONI	D1SWAL	E NORTH			
SEGMENT ID #	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L223	0+00.00	826,916.6624; 1,457,395.0411	N/A	8.39	N78 12' 17.64"W	N/A	0+08.39	826,918.3775; 1,457,386.8280
L224	0+08.39	826,918.3775; 1,457,386.8280	N/A	11.53	N90°00'00.00"W	N/A	0+19.92	826,918.3775; 1,457,375.2971
L225	0+19.92	826,918.3775; 1,457,375.2971	N/A	21.41	S73° 52' 32.96"W	N/A	0+41.33	826,912.4322; 1,457,354.7319
L226	0+41.33	826,912.4322; 1,457,354.7319	N/A	25.82	S70 28' 32.42"W	N/A	0+67.14	826,903.8045; 1,457,330.4009
L227	0+67.14	826,903.8045; 1,457,330.4009	N/A	16.40	S83° 03' 39.63"W	N/A	0+83.54	826,901.8231; 1,457,314.1204
L228	0+83.54	826,901.8231; 1,457,314.1204	N/A	84.22	N59'15'21.41"W	N/A	1+67.77	826,944.8775; 1,457,241.7354
L229	1+67.77	826,944.8775; 1,457,241.7354	N/A	207.23	N59 15' 21.41"W	N/A	3+74.99	827,050.8137; 1,457,063.6305
L230	3+74.99	827,050.8137; 1,457,063.6305	N/A	51.57	N59°15'21.41"W	N/A	4+26.57	827,077.1785; 1.457.019.3048

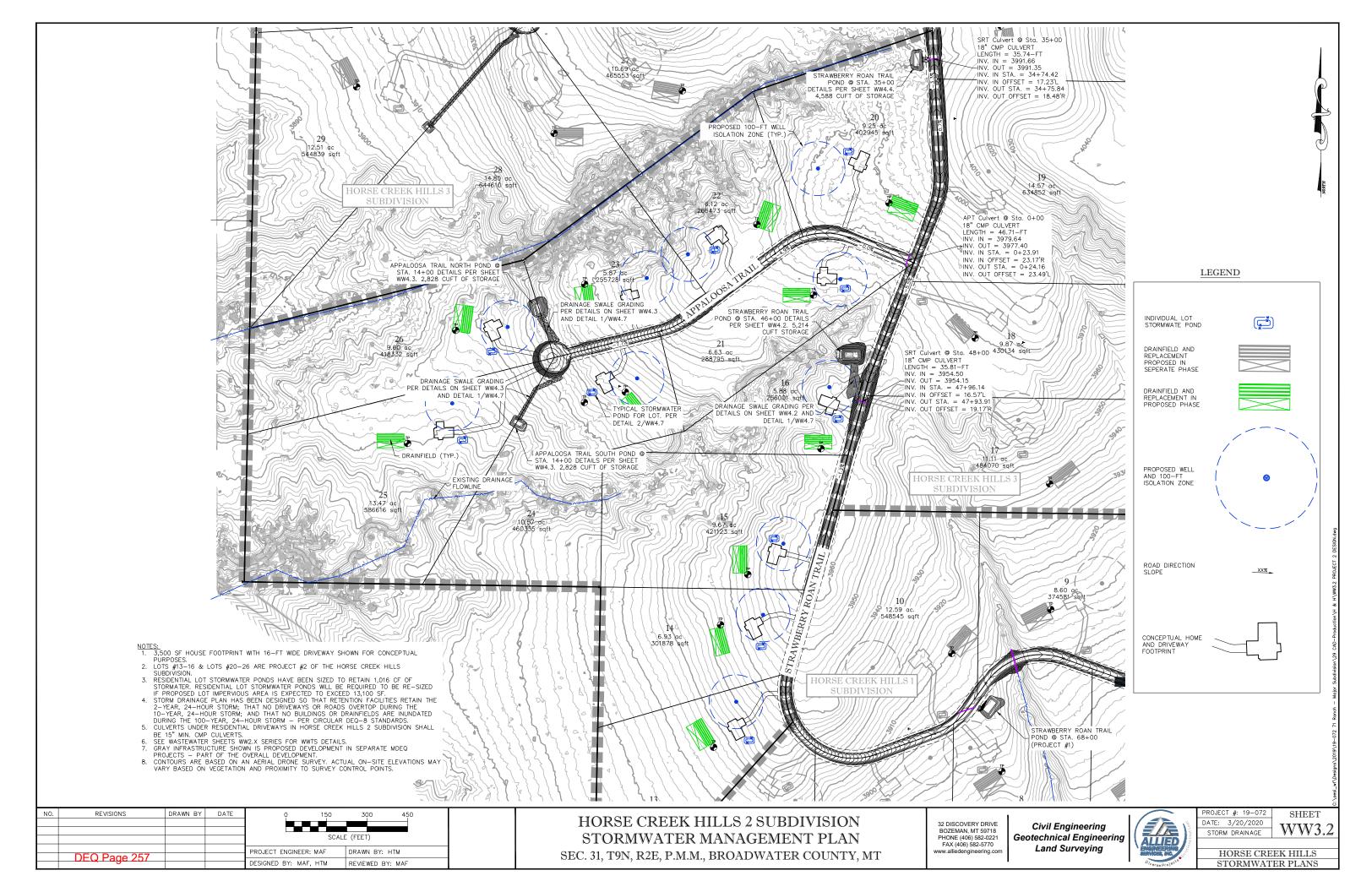
	BST POND 2 SWALE SOUTH										
SEGMENT ID#	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING			
L231	0+00.00	826,810.9266; 1,457,400.7388	N/A	7.82	S70° 49' 15.53"W	N/A	0+07.82	826,808.3590; 1,457,393.3570			
L232	0+07.82	826,808.3590; 1,457,393.3570	N/A	9.05	S82°41'22.27"W	N/A	0+16.87	826,807.2071; 1,457,384.3780			
L233	0+16.87	826,807.2071; 1,457,384.3780	N/A	40.98	S77° 54' 37.00"W	N/A	0+57.85	826,798.6231; 1,457,344.3023			
L234	0+57.85	826,798.6231; 1,457,344.3023	N/A	65.90	S55 49'18.34"W	N/A	1+23.75	826,761.6045; 1,457,289.7866			
L235	1+23.75	826,761.6045; 1,457,289.7866	N/A	444.76	S41° 37' 08.04"W	N/A	5+68.51	826,429.1084; 1,456,994.3865			

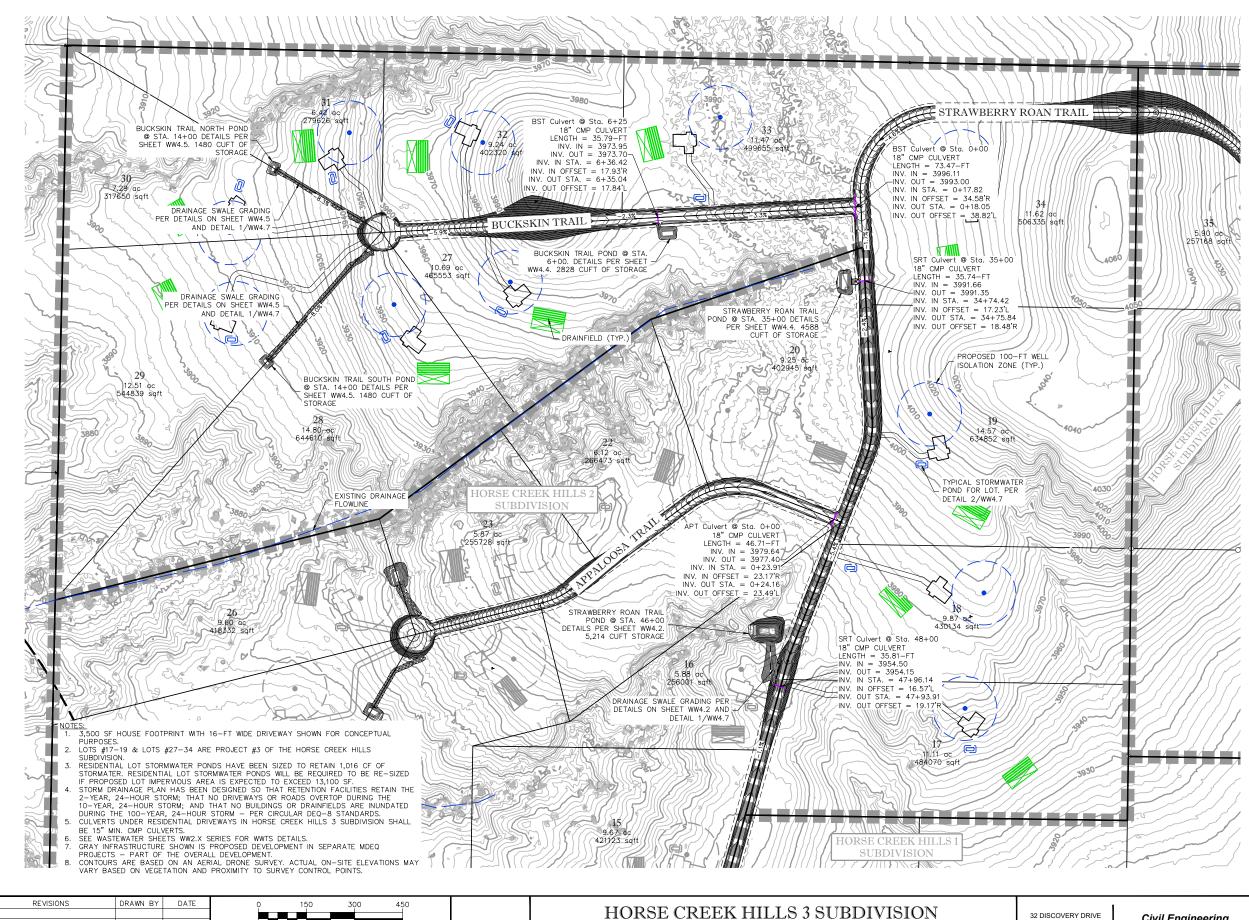
NO.	REVISIONS	DRAWN BY	DATE	PROJECT ENGINEER: MAF	DRAWN BY: HTM	HORSE CREEK HILLS SUBDIVISION - STORMWATER ALIGNMENT COORDINATE TABLES SEC 31 T9N R2E P.M.M. BROADWATER COUNTY MT	32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com
	DEQ Page 255			PROJECT ENGINEER: MAF	DRAWN BY: HTM	SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT	www.alliedengineering.com
	DEQ Page 200			DESIGNED BY: MAF, HTM	REVIEWED BY: MAF		





NOTES:	LEGEND
 SJOD SF HOUSE FOOTPRINT WITH 16-FT WIDE DRIVEWAY SHOWN FOR CONCEPTUAL PURPOSES. LOTS #1-12 ARE PROJECT #1 OF THE HORSE CREEK HILLS SUBDIVISION. LOT #1 IS A PROPOSED COMMERCIAL LOT - RE-SIZING OF RETENTION POND FOR COMMERCIAL LOTS WILL BE REQUIRED IF IMPERVIOUS AREA WILL EXCEED 13,100 SF. RESIDENTIAL LOT STORMWATER PONDS HAVE BEEN SIZED TO RETAIN 1,016 CF OF STORMATER. RESIDENTIAL LOT STORMWATER PONDS WILL BE REQUIRED TO BE RE-SIZED IF PROPOSED LOT IMPERVIOUS AREA IS EXPECTED TO FXCEED 13,100 SF. STORM DRAINAGE PLAN HAS BEEN DESIGNED SO THAT RETENTION FACILITIES RETAIN THE 2-YEAR, 24-HOUR STORM; THAT NO DRIVEWAYS OR ROADS OVERTOP DURING THE 10-YEAR, 24-HOUR STORM; THAT NO DRIVEWAYS OR DRAINFIELDS ARE INUNDATED DURING THE 100-YEAR. 24-HOUR STORM - PER CIRCULAR DEO-8 STANDARDS. CULVERTS UNDER RESIDENTIAL DRIVEWAYS IN HORSE CREEK HILLS 1 SUBDIVISION SHALL BE 18" MIN. CMP CULVERTS. SEE WASTEWATER SHEETS WW2X SERIES FOR WWTS DETAILS. GRAY INFRASTRUCTURE SHOWN IS PROPOSED DEVELOPMENT IN SEPARATE MDEQ PROJECTS - PART OF THE OVERALL DEVELOPMENT IN SEPARATE MDEQ PROJECTS - PART OF THE OVERALL DROVE SURVEY. ACTUAL ON-SITE ELEVATIONS MAY VARY BASED ON VEGETATION AND PROXIMITY TO SURVEY CONTROL POINTS. 	INDIVIDUAL LOT STORMWATE POND DRAINFIELD AND REPLACEMENT PROPOSED IN SEPERATE PHASE DRAINFIELD AND REPLACEMENT IN PROPOSED PHASE ORAINFIELD AND REPLACEMENT IN PROPOSED PHASE
REVISIONS DRAWN BY DATE 0 150 300 450 SCALE (FEET) SCALE (FEET)	HORSE CREEK HILLS 1 SUBDIVISION STORMWATER MANAGEMENT PLAN 32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 G

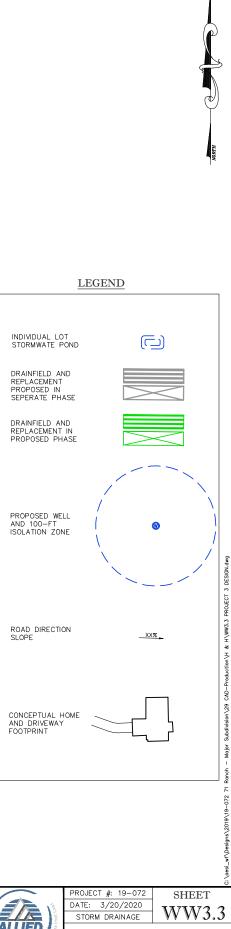




NO.	REVISIONS	DRAWN BY	DATE	Q 1	50	300	450		
				SCALE (FEET)					
				PROJECT ENGINEER: MAI	F	DRAWN BY: H	ТМ		
	DEQ Page 258								
				DESIGNED BY: MAF, HT	M	REVIEWED BY:	MAF		

HORSE CREEK HILLS 3 SUBDIVISION STORMWATER MANAGEMENT PLAN SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT

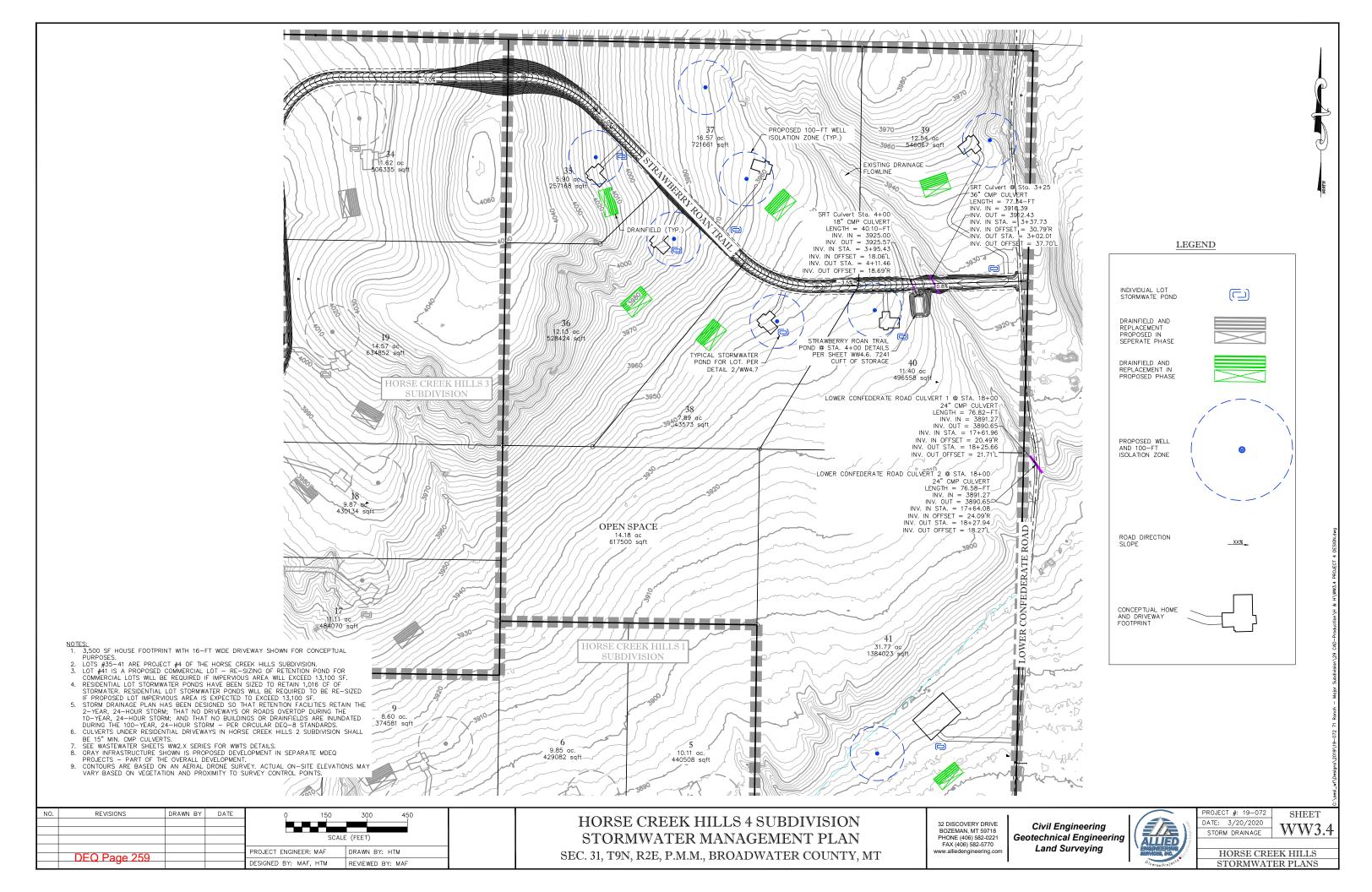
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

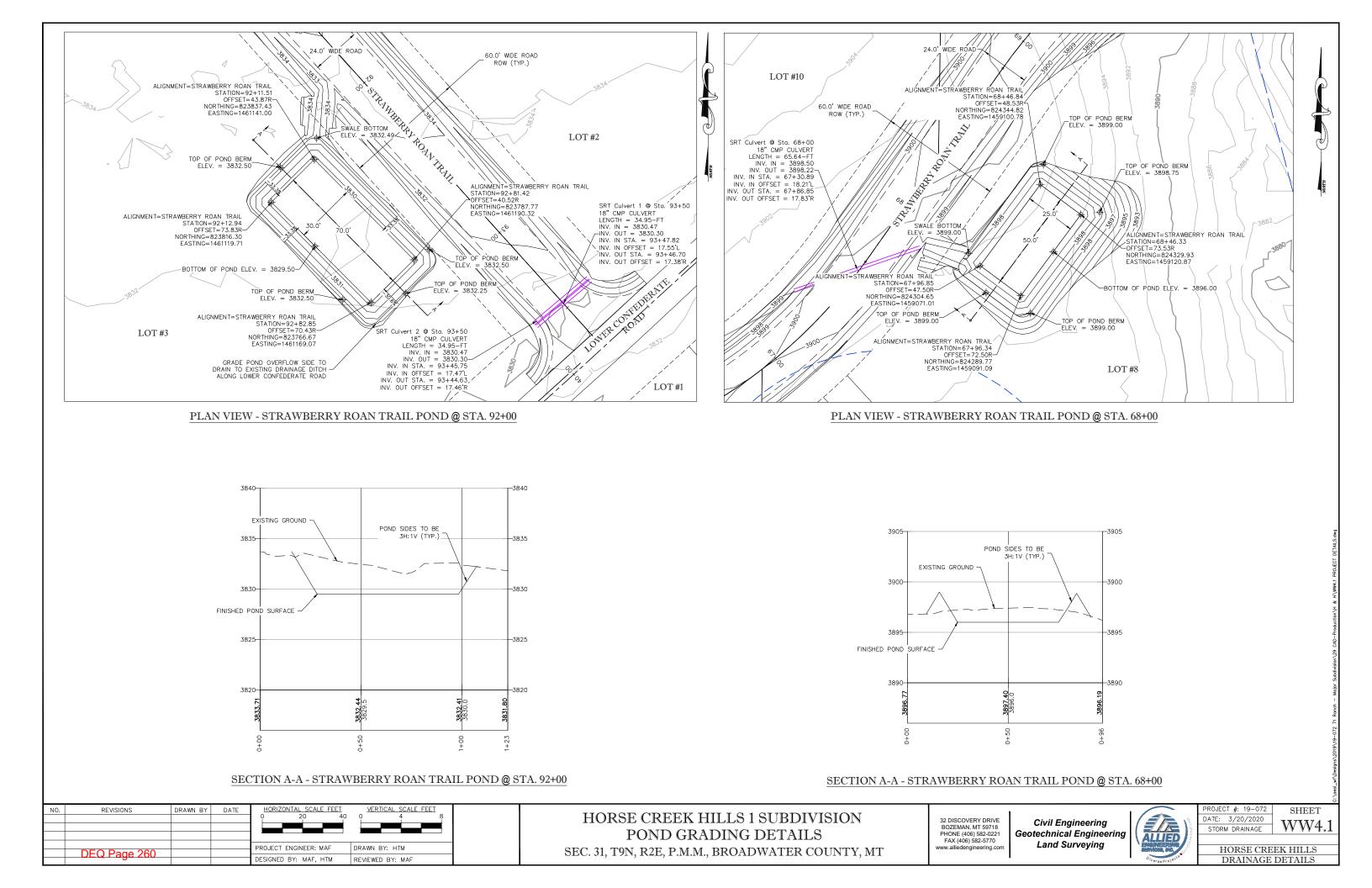


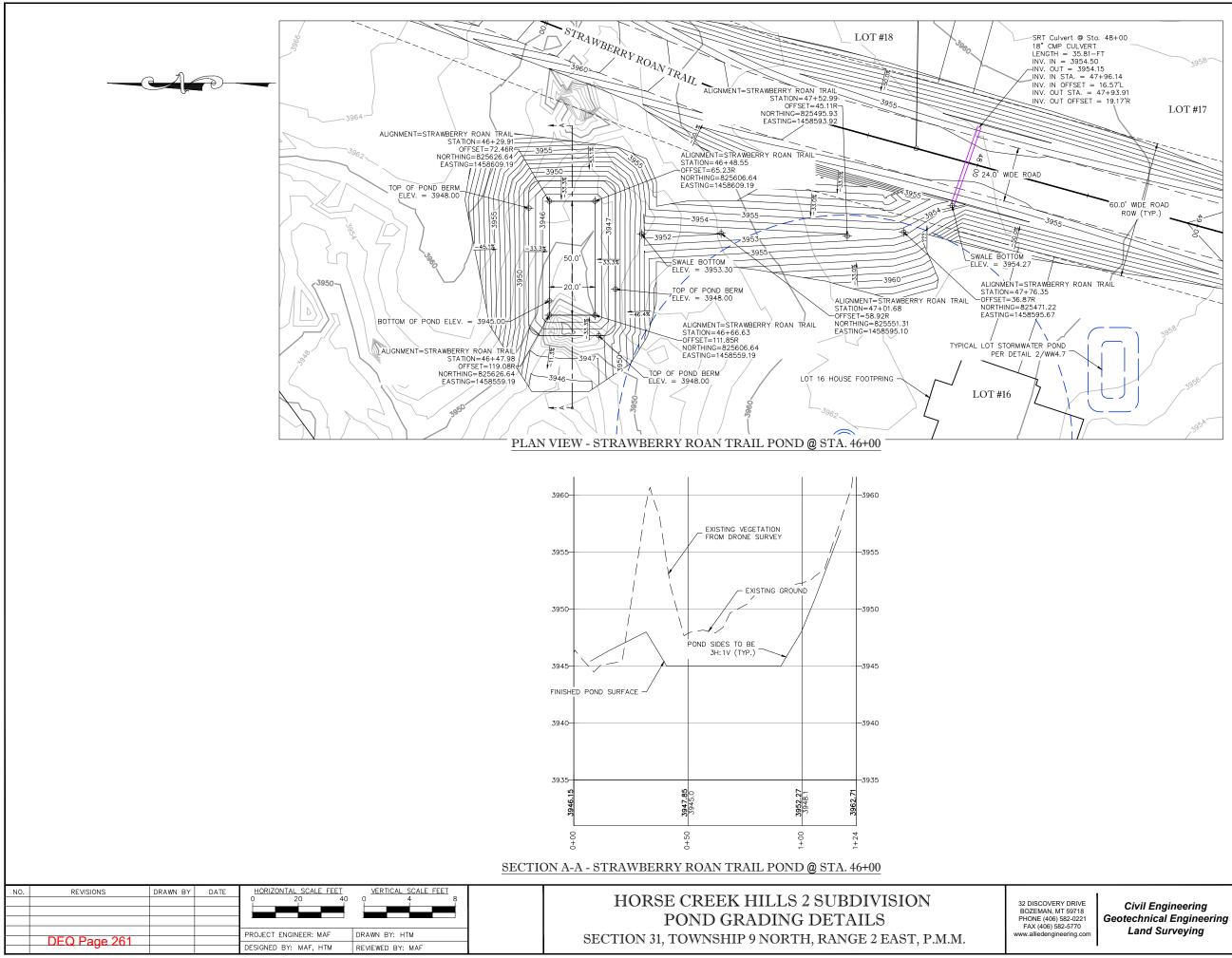
HORSE CREEK HILLS

STORMWATER PLANS



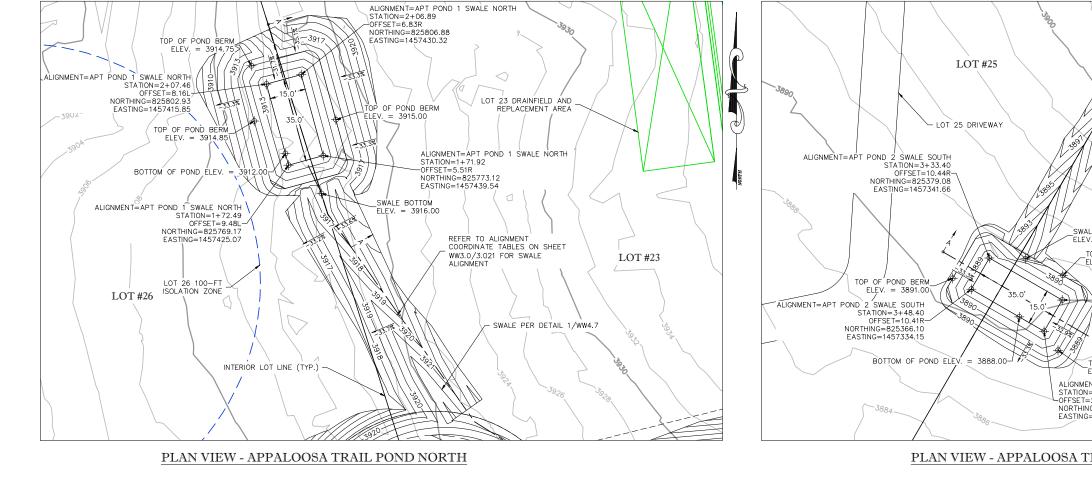


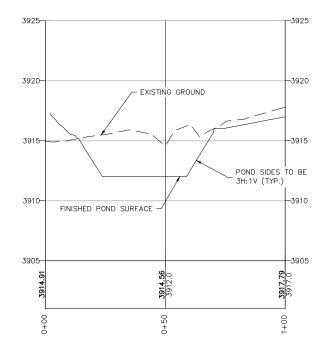




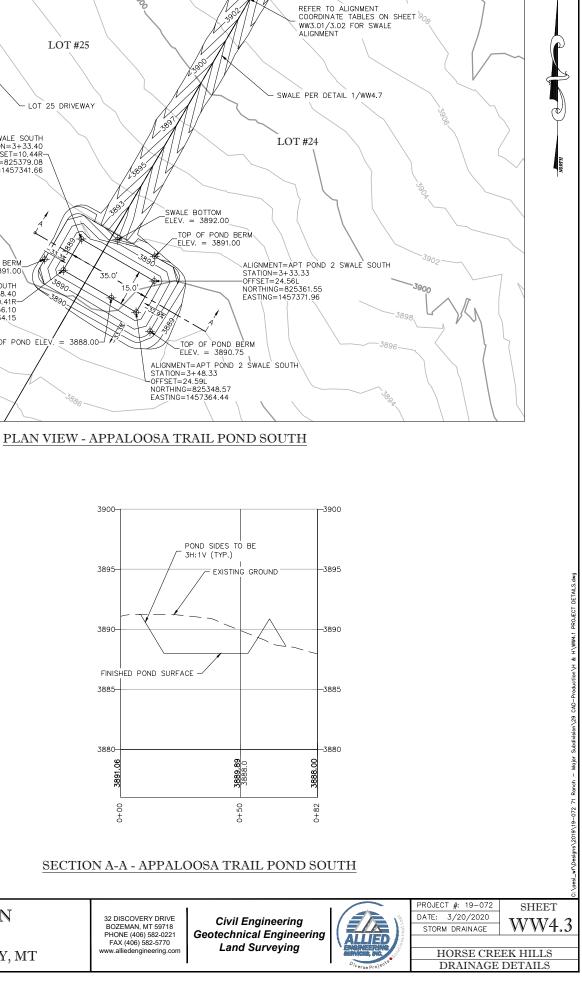






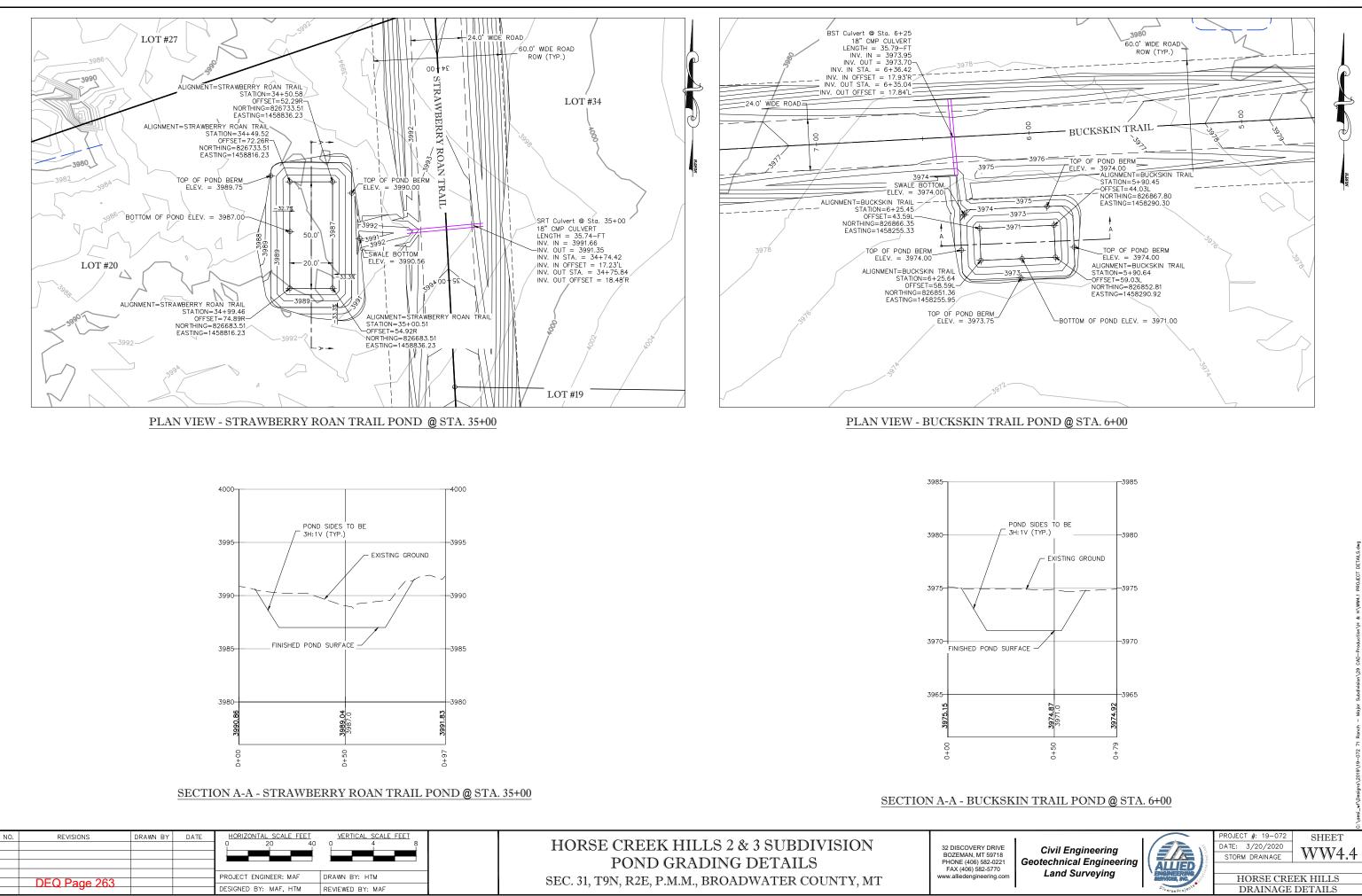


SECTION A-A - APPALOOSA TRAIL POND NORTH



HORSE CREEK HILLS 2 SUBDIVISION	
POND GRADING DETAILS	
SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT	

NO.	REVISIONS	DRAWN BY	DATE	HORIZONTAL SCALE FEET	VERTICAL SCALE FEET	
				0 20 40		
						l I
						l I
						1
				PROJECT ENGINEER: MAF	DRAWN BY: HTM	1
	DEQ Page 262					1
				DESIGNED BY: MAF, HTM	REVIEWED BY: MAF	
				DESIGNED DT. MINT, TTM	NEVIEWED DI. MAI	



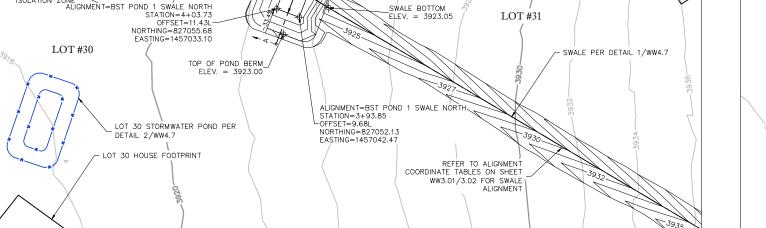
3930	3930	
POND SIDES TO BE 3H: 1V (TYP.) 3925 EXISTING GROUND	3925	3915 POND SIDES TO BE 3H:1V (TYP.)
3920 FINISHED POND SURFACE	3920	3910 EXISTING GROUND
3915	3915	3905 FINISHED POND SURFACE
3910	3910	3900 90 90 90 90 90 90 90 90 90 90 90 90
0++00000000000000000000000000000000000		
SECTION A-A - BUCKSKIN TRAIL P	<u>POND NORTH</u>	SECTION A-A - BUCKSKIN TH
N BY DATE HORIZONTAL SCALE FEET 0 20 40 0 4 8 PROJECT ENGINEER: MAF DRAWN BY: HTM DESIGNED BY: MAF, HTM REVIEWED BY: MAF	HORSE CREEK HILLS 3 SUBDIVISION POND GRADING DETAILS SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT	32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

LOT 31 WELL ISOLATION ZONE

LOT 31 HOUSE FOOTPRINT

Ċ

ORTH



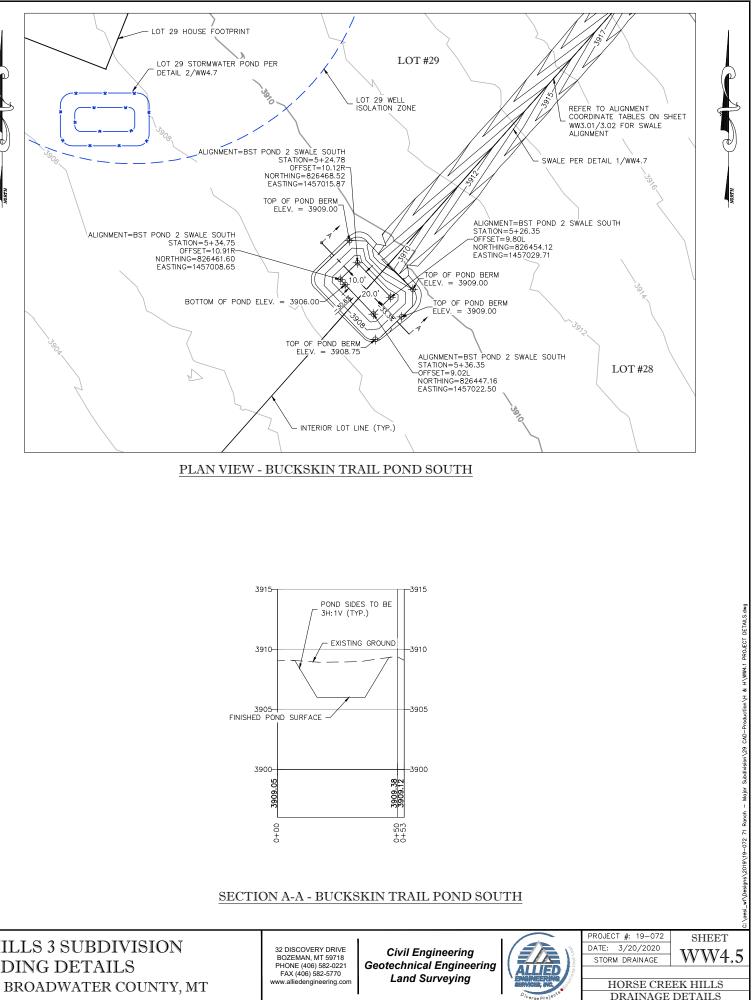
LOT 31 DRAINFIELD AND REPLACEMENT AREA

ALIGNMENT=BST POND 1 SWALE STATION=3+97.30 OFFSET=9.99R NORTHING=827070.81 EASTING=1457049.57

TOP OF POND BERM

__TOP OF POND BERM ELEV. = 3923.00

ELEV. = 3923.00



PLAN VIEW - BUCKSKIN TRAIL POND NORTH

 $\overline{\mathbf{A}}$ 10.0

Tit t

ALIGNMENT=BST POND 1 SWALE NORTH

BOTTOM OF POND ELEV.

LOT 26 100-FT ISOLATION ZONE ALIGNMENT=BST POND 1 SWALE NORTH

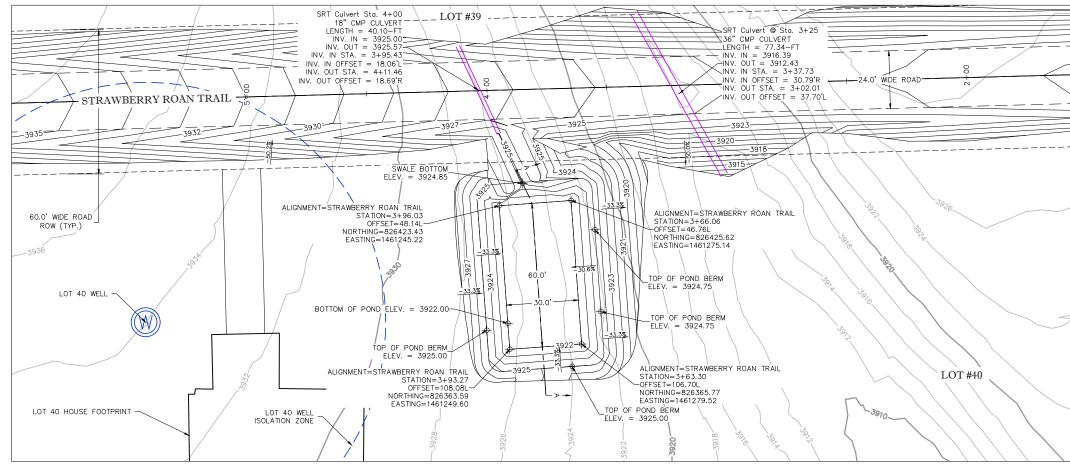
INTERIOR LOT LINE (TYP.)

STATION=4+07.16 OFFSET=8.28R¬ NORTHING=827074.37 EASTING=1457040.22

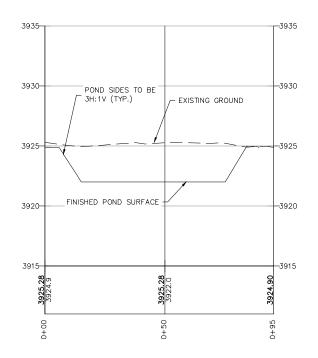
TOP OF POND BERM ELEV. = 3922.75

= 3920.00

NO.	REVISIONS	DRAWN BY	DATE	HORIZONTAL SCALE FEET	VERTICAL SCALE FEET	
				0 20 40		
				PROJECT ENGINEER: MAF	DRAWN BY: HTM	1
	DEO Page 264				BIOWIN BIL IIIM	-
	DEQIUGUEUI			DESIGNED BY: MAF, HTM	REVIEWED BY: MAF	



PLAN VIEW - STRAWBERRY ROAN TRAIL POND @ STA. 4+00



SECTION A-A - STRAWBERRY ROAN TRAIL POND @ STA. 4+00

NO.	REVISIONS	DRAWN BY	DATE	HORIZONTAL SCALE FEET	VERTICAL SCALE FEET	
				0 20 40	0 4 8	
				PROJECT ENGINEER: MAF	DRAWN BY: HTM	1
	DEQ Page 265			PROJECT ENGINEER: MAP		1
	DEQ 1 age 200			DESIGNED BY: MAF, HTM	REVIEWED BY: MAF	

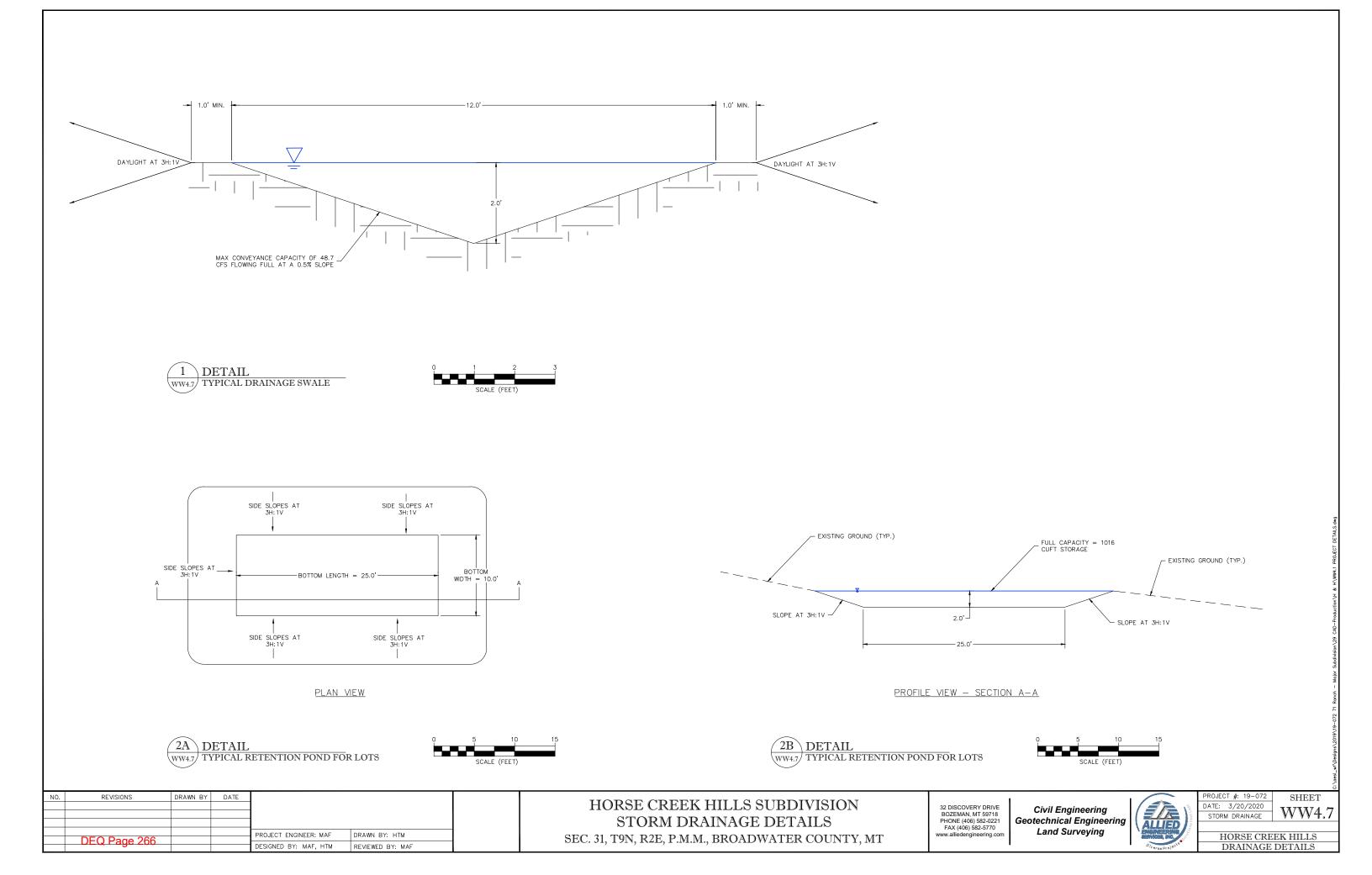
HORSE CREEK HILLS 4 SUBDIVISION POND GRADING DETAILS SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT

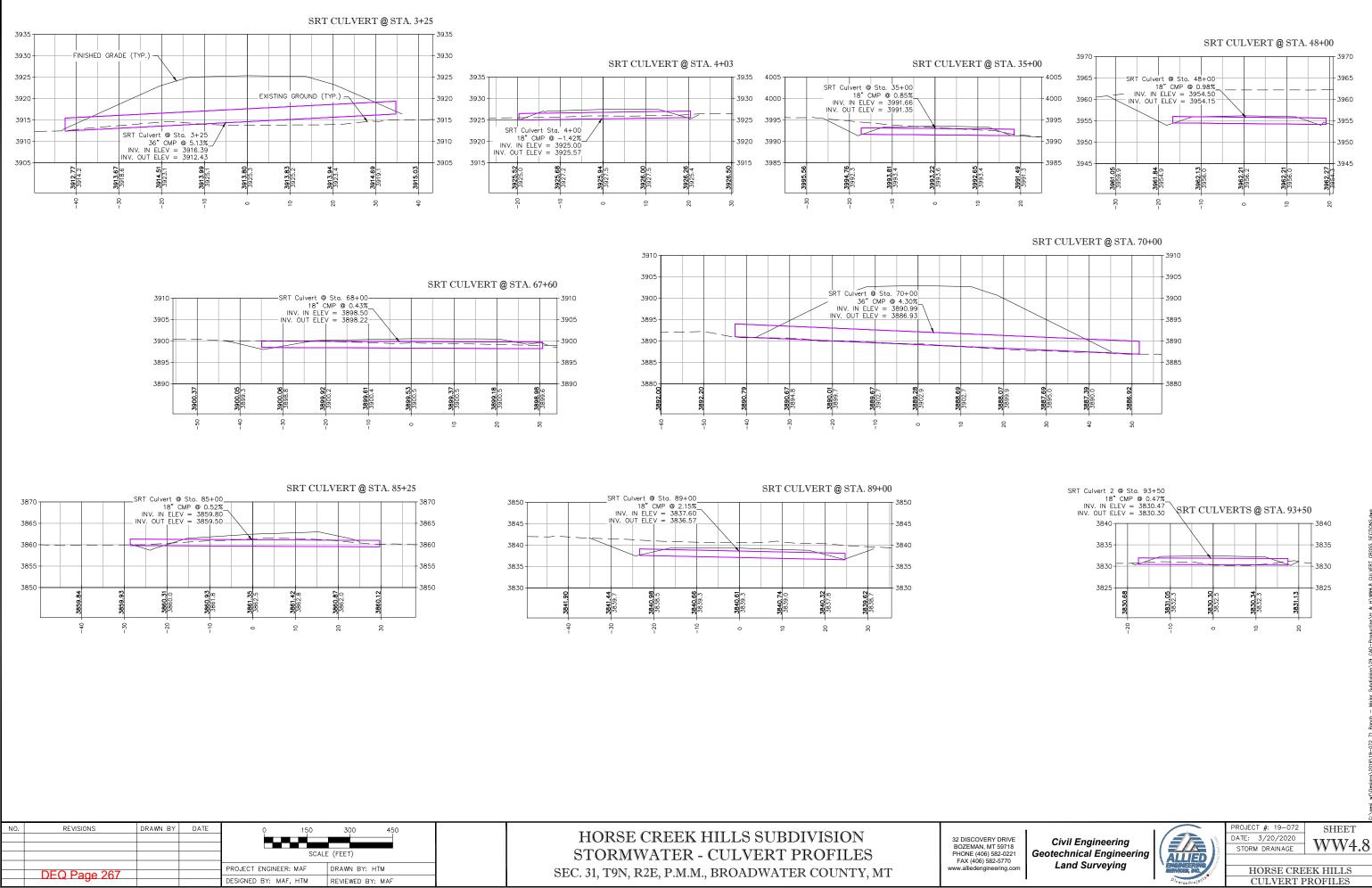
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

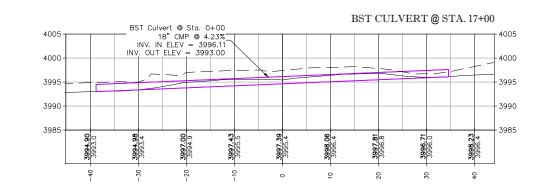




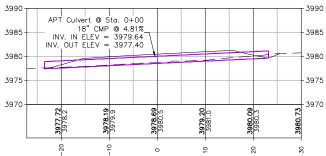


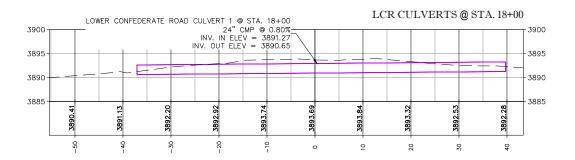






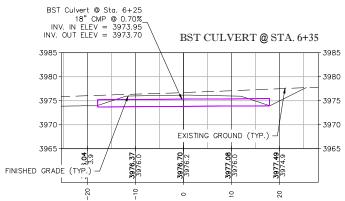






HORSE CREEK HILLS SUBDIVISION
STORMWATER - CULVERT PROFILES
SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT

NO.	REVISIÓNS	DRAWN BY	DATE		0	150	300	450
						SCALE	. (FEET)	
				PROJECT E	NGINEER	MAF	DRAWN BY: H	TM
	DEQ Page 268			TROOLOT E			biomit bii i	
				DESIGNED E		LITM		
	•			DESIGNED E	DI: MAF,		REVIEWED BY:	MAF





Civil Engineering Geotechnical Engineering Land Surveying

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com



ROJECT #: 19-072	SHEET
ATE: 3/20/2020	****
STORM DRAINAGE	WW4.9
HORSE CRE	EK HILLS
CULVERT F	PROFILES

HORSE CREEK HILLS 1-4 SUBDIVISIONS STORM DRAINAGE MAINTENANCE PLAN

The Horse Creek Hills Subdivisions (HOA) shall be responsible for adequate maintenance and operation of all storm drainage facilities (including roadside ditches, ponds, swales, culverts, etc.) located within the "storm drainage" easements and "utility" easements as shown on the Final Plat of Horse Creek Hills 1-4 Subdivisions. The individual lot Owners shall be responsible for adequate maintenance and operation of all storm facilities (including ponds, swales, culverts, etc.) that are only serving their individual needs of their respective lots.

All trash and debris shall be removed from the storm drainage facilities by no later than May 1st of each year. If the HOA fails to remove the trash or debris from the shared storm drainage facilities as described, individual lot owners may cause trash or debris to be removed and proportionately bill the Owners of the subdivision for such efforts. Similarly, if individual lot Owners fail to remove trash or debris from their lot specific storm drainage facilities as described, the HOA may cause trash or debris to be removed and bill the Lot Owner for such efforts.

The Homeowners' Association shall ensure that yearly maintenance is conducted to remove sediment or debris as needed from the storm water swales, ponds, and culverts so that the aforementioned facilities function properly. Until such time that the Association assumes the maintenance responsibilities of the storm drainage facilities, such requirements shall be the responsibility of the Developer.

The control of noxious weeds by the Homeowners' Association on those areas for which the HOA is responsible, including storm drainage easements, roadside ditches, etc. shall comply with the Weed Management and Revegetation Plan as approved by the Broadwater County Weed Control District.

Lawns shall be maintained at a height of $2 \frac{1}{2}$ " – $3 \frac{1}{2}$ " and shall be irrigated/water, fertilized, controlled for noxious weeds, and otherwise properly cared for. If each individual lot owner fails to properly maintain their lawn area, the HOA may cause the lawn to be maintained at the Owner's expense.

Appendix G

Road Plans & Complete Set of MDEQ Plans for Subdivisions 1-4

- Draft Road Construction Plans
- Complete set of MDEQ plans for Subdivisions 1-4

HORSE CREEK HILLS SUBDIVISION

ROAD DESIGN

LOCATION: N $\frac{1}{2}$, N $\frac{1}{2}$ of the SE $\frac{1}{4}$, & NE $\frac{1}{4}$ of the SW $\frac{1}{4}$, SEC 31, T9N. R2E. P.M.M., BROADWATER COUNTY, MONTANA

LATITUDE: 46°29'45.6" LONGITUDE: -111°31'13" **DEVELOPER: 71 RANCH LP** February 12, 2020

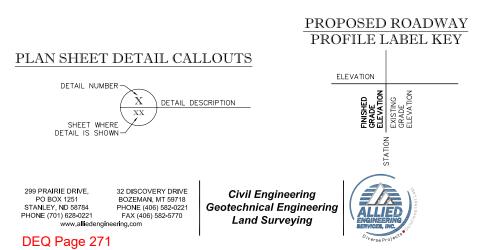
SET NO.

PRELIMINARY NOT

FOR CONSTRUCTION

PROJECT MANAGER: MARK FASTING. PE **DESIGN ENGINEER:** JOSH SMITH. EI PROJECT SURVEYOR: GREG FINCK, PLS

	SHEET INDEX				
SHEET NO.					
GENERA	L SHEETS				
C0-1	EXISTING CONDITIONS & SURVEY CONTROL				
C0-2	PROPOSED IMPROVEMENTS				
ROAD SH	IEETS				
C1-1	STRAWBERRY ROAN TRAIL PLAN & PROFILE (STA 0+00 - STA 14+50)				
C1-2	STRAWBERRY ROAN TRAIL PLAN & PROFILE (STA 14+50 - STA 29+00)				
C1-3	STRAWBERRY ROAN TRAIL PLAN & PROFILE (STA 29+50 - STA 43+50)				
C1-4	STRAWBERRY ROAN TRAIL PLAN & PROFILE (STA 43+50 - STA 58+00)				
C1-5	STRAWBERRY ROAN TRAIL PLAN & PROFILE (STA 58+00 - STA 67+50)				
C1-6	STRAWBERRY ROAN TRAIL PLAN & PROFILE (STA 67+50 - STA 79+50)				
C1-7	STRAWBERRY ROAN TRAIL PLAN & PROFILE (STA 79+50 - STA 93+76)				
C1-8	BUCKSKIN TRAIL PLAN & PROFILE (STA 0+00 - STA 14+50)				
C1-9	APPALOOSA TRAIL PLAN & PROFILE (STA 0+00 - STA 14+50)				
C1-10	ROAD ALIGNMENT COORDINATE TABLES				
ROAD CF	ROSS-SECTION SHEETS				
C2-X	STRAWBERRY ROAN TRAIL CROSS-SECTIONS				
C2-X	BUCKSKIN TRAIL CROSS-SECTIONS				
C2-X	APPALOOSA TRAIL CROSS-SECTIONS				
INTERSE	CTION GRADING SHEETS				
C3-1	STRAWBERRY ROAN TRAIL & LOWER CONFEDERATE ROAD NORTHERN INTERSECTION				
C3-2	STRAWBERRY ROAN TRAIL & LOWER CONFEDERATE ROAD SOUTHERN INTERSECTION				
C3-3	BUCKSKIN TRAIL & STRAWBERRY ROAN TRAIL INTERSECTION				
C3-4	APPALOOSA TRAIL & STRAWBERRY ROAN TRAIL INTERSECTION				
C3-5	BUCKSKIN TRAIL CUL-DE-SAC				
C3-6	APPALOOSA TRAIL CUL-DE-SAC				
SIGNAGE AND UTILITY CONDUIT SHEETS					
C4-1	SIGNAGE PLAN SHEET				
C4-2 UTILITY CONDUIT PLAN (PENDING)					
DETAIL	SHEETS				
C5-0	TYPICAL ROAD SECTION DETAILS				
C5-1	GENERAL CIVIL DETAILS				



CIVIL ABBREVIATIONS:

MAXIMUM MANHOLF

MINIMUM

NORTH

RADIUS

RIGHT

SOUTH SCHEDULE STORM DRAIN SECTION

SUBGRADE

STREET

STATION STANDARD

TYPICAL

VERTICAL

WEST WITH WITHOUT

SQUARE YARD

UNDERGROUND

WATER MAIN

WATER SERVICE

RADIUS POINT

PIPE RIGHT-OF-WAY

MID POINT

MECHANICAL JOINT

MONTANA PUBLIC WORKS

POINT OF CURVATURE

POINT OF TANGENCY

POLYVINYL CHLORIDE

REINFORCED CONCRETE

SANITARY SEWER MAIN

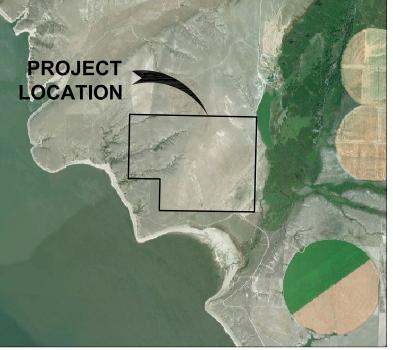
SANITARY SEWER SERVICE

TEMPORARY BENCH MARK TOP BACK OF CURB TOTAL DYNAMIC HEAD

STANDARD SPECIFICATIONS

PLAIN END POLYETHYLENE POINT OF INTERSECTION PROPERTY LINE POUNDS PER SQUARE INCH

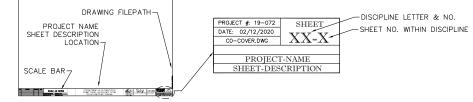
AESI AC AVE BLDG BM	ALLIED ENGINEERING SERVICES, INC. ACRE AVENUE BUILDING BENCHMARK	MAX MH MIN MJ MP MPWSS
BOG	BACK OF GRATE (GUTTER)	N
CL CMP CO CONC COB CY	CENTERLINE CORRUGATED METAL PIPE CLEAN OUT CONCRETE CITY OF BELGRADE CUBIC YARD	PC PE PI PL PSI
DI DIA DWG	DUCTILE IRON DIAMETER DRAWING	PT PVC
E EA EG	EAST EACH EXISTING GRADE	R RP RCP
ELEV EOG EOP EX	ELEVATION EDGE OF GRAVEL EDGE OF PAVEMENT EXISTING	ROW RT S SCH
FETS FG FHYD FL FL FM FT	FLARED END TERMINAL SECTION FINISHED GRADE FIRE HYDRANT FLANGE FLOWLINE SEWER FORCE MAIN FEET	SD SECT SG SS ST STA STD SY
GPM GV	GALLONS PER MINUTE GATE VALVE	ТВМ ТВС
HDPE	HIGH DENSITY POLYETHYLENE	TDH TYP
HORZ HP HWY	HORIZONTAL HIGH POINT HIGHWAY	UG
IE IN IN V	INVERT ELEVATION INCH INVERT	VERT W W/
LF LP LT	LINEAR FEET LOW POINT LEFT	w/ W/O WS



AERIAL MAP 1 000 2,000 3,000 SCALE (FEET)

LEGEND

	PROPERTY LINE
•	FOUND MONUMENT
\triangle	CONTROL POINT
	EX. MAJOR CONTOUR (5' IN
	EX. MINOR CONTOUR (1' IN
	EX. EDGE OF ROAD
	EX. DRAINAGE CULVERT
x x	EX. FENCE
\sim	EX. TREE ROW
	EX. PINE TREE
W	EX. WATER MAIN
gv	EX. GATE VALVE
ЭС.	EX. FIRE HYDRANT
	EX. WELL
s	EX. SEWER MAIN
S	EX. SEWER MANHOLE
OHP	EX. OVERHEAD POWER LINE
	EX. OVERHEAD POWER POL
	EX. ELECTRIC METER
F	EX. UNDERGROUND FIBER C
	EX. TELEPHONE/FIBER OPTI
	AESI S
Г	



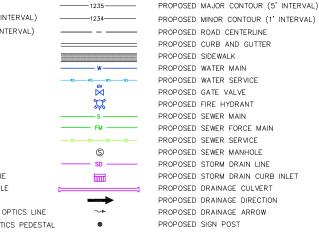
- ACTIVITIES
- CONFLICTS

- AVAILABILITY

- PRACTICABLE

N

- 27. ADDITIONAL MAILBOX PULL-OUT MAY BE REQUIRED, WHICH IS NOT SHOWN ON THESE PLANS. CONTRACTOR SHALL COORDINATE WITH
- ENGINEER AND USPS AS NECESSARY.
- BLOCKS, ETC.), THAT ARE NOT SHOWN ON THESE PLANS.



PROPOSED LOT LINE PROPOSED RIGHT-OF-WAY LINE

ROAD DESIGN

HORSE CREEK HILLS SUBDIVISION -

STANDARD BORDER FORMAT

GENERAL NOTES AND SPECIFICATIONS:

1. THE CONTRACTOR MUST ADHERE TO THE PROJECT PLANS AND SPECIFICATIONS. THE CONSTRUCTION COMPANY MUST BE A LICENSED CONTRACTOR WITH THE STATE OF MONTANA AND BE COVERED BY LIABILITY INSURANCE. A TWO-YEAR WRITTEN WARRANTY FROM THE PROJECT CONTRACTOR TO GALLATIN COUNTY IS REQUIRED FOR ALL ONSITE AND OFFSITE ROAD IMPROVEMENTS

THE EXISTING UNDERGROUND UTILITIES SHOWN ON THE PLAN ARE BASED ON A STANDARD UTILITY LOCATE WITH NO FIELD EXPLORATIONS CONDUCTED TO CONFIRM THEIR LOCATIONS & DEPTHS. THE CONTRACTOR WILL BE RESPONSIBLE FOR LOCATING ALL UNDERGROUND UTILITIES BY CALLING THE NATIONAL 811 "CALL BEFORE YOU DIG" TELEPHONE NUMBER PRIOR TO CONSTRUCTION

ACTIVITIES. ALL ROAD AND STORM DRAINAGE IMPROVEMENTS SHALL BE CONSTRUCTED PER THE ALIGNMENT AND GRADE AS SHOWN ON THE PLANS. CONTRACTOR SHALL FIELD VERIFY LOCATION AND DEPTH OF ALL EXISTING UTILITIES AND STRUCTURES WHERE NEW FACILITIES CROSS OR CONNECT. CONTRACTOR SHALL BE RESPONSIBLE FOR EXPOSING POTENTIAL UTILITY CONFLICTS FAR ENOUGH AHEAD OF CONSTRUCTION TO MAKE NECESSARY GRADE MODIFICATIONS WITHOUT DELAYING THE WORK. ALL UTILITY CONSUMPS SHALL BE POTHOLED OR VACUUMED AS NECESSARY PRIOR TO EXCAVATING OR BORING TO ALLOW THE CONTRACTOR TO PREVENT GRADE OR ALIGNMENT CONFLICTS.

5 AT LEAST 10 BUSINESS DAYS BEFORE BEGINNING ANY EXCAVATION. THE CONTRACTOR SHALL NOTICY THE OWNER AND ENGINEER OF 5. AT LEAST 10 BUSINESS DAYS BEFORE BEGINNING ANY EXCAVATION, THE CONTRACTOR SHALL NOTIFY THE OWNER AND ENGINEER OF UNDERGROUND FACILITIES AND COORDINATE THE WORK WITH THE OWNERS OF SUCH UNDERGROUND FACILITIES. THE INFORMATION SHOWN OR INDICATED IN THE CONTRACT DOCUMENTS WITH RESPECT TO EXISTING UNDERGROUND FACILITIES IS BASED ON INFORMATION AND DATA OBTAINED FROM THE OWNERS OF THE FACILITIES WITHOUT FIELD EXPLORATION, AND AS SUCH, OWNER AND ENGINEER ARE NOT RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF SUCH INFORMATION OVERNIGHT. ALL SUCH TRENCHES SHALL BE BACKFILLED, COMPACTED AND CLOSED BEFORE THE END OF EACH WORK DAY AND NORMAL TRAFFIC FLOWS RESTORED.
IF THE ENGINEER IS CONTRACTED FOR CONSTRUCTION, TAKING, ENGINEER SHALL BE CONTACTED PRIOR TO STAKING. PROVIDE ADVANCED NOTICE SUFFICIENT TO ACCOMMODATE CONSTRUCTION, <u>Z WORKING DAY IS MINIMUM</u>, AND MAY VARY DEPENDING UPON AVAIL ARUITY

AVAILABILITY. 8. LIGHTING, ELECTRICAL, NATURAL GAS, COMMUNICATIONS, LANDSCAPING, ETC. ARE TO BE DESIGNED BY OTHERS. 9. FINAL QUANTITES MAY BE HIGHER OR LOWER THAN THOSE ESTIMATED, PENDING FIELD FINDINGS, SITE CONDITIONS, ETC. 10. STRIP THE EMBANKMENT FOUNDATION AREA, BORROW AREAS AND ALL AREAS TO RECEIVE FILL TO A MINIMUM DEPTH OF 6 INCHES AND AS REQUIRED TO REMOVE ALL ORGANIC SOILS, VEGETATIVE MATTER, ROOTS, AND OTHER PERISHABLE, LOOSE OR OBJECTIONABLE MATERIAL INCLUDING FROZEN SOIL THAT MIGHT INTERFERE WITH COMPACTION OF EMBANKMENT LIFT OR THE BONDING OF EMBANKMENT TO FOUNDATION. OBJECTIONABLE MATERIAL WILL BE AS DETERMINED BY THE ENGINEER. PERFORM STRIPPING OPERATIONS IN A MANNER TO CONSERVE ALL TOPSOIL THAT CONTAINS ORGANICS. 11. TRANSPORT STRIPPED MATERIALS TO STOCKPILE AREAS OUTSIDE OF WATERWAYS AND WETLANDS, SUBJECT TO APPROVAL. COORDINATE WITH OWNER TO IDENTIFY. STOCKPILE AREAS OUTSIDE OF WATERWAYS AND WETLANDS, SUBJECT TO APPROVAL. COORDINATE WITH OWNER TO COMPENDE MATERIALS TO STOCKPILE AREAS OUTSIDE OF WATERWAYS AND WETLANDS, SUBJECT TO APPROVAL. COORDINATE WITH OWNER TO COMPENDE MATERIALS TO STOCKPILE AREAS OUTSIDE OF MATERWAYS AND WETLANDS, SUBJECT TO APPROVAL. COORDINATE WITH OWNER TO COMPENDENT STOCKPILE AREAS OUTSIDE OF MATERWAYS AND WETLANDS, SUBJECT TO APPROVAL. COORDINATE WITH OWNER TO COMPENDENT STOCKPILE AREAS OUTSIDE OF MATERWAYS AND WETLANDS, SUBJECT TO APPROVAL. COORDINATE WITH OWNER TO COMPENDENT STOCKPILE AREAS OUTSIDE OF MATERWAYS AND WETLANDS, SUBJECT TO APPROVAL. COORDINATE WITH OWNER TO COMPENDENT STOCKPILE AREAS OUTSIDE OF MATERWAYS AND WETLANDS, SUBJECT TO APPROVAL. COORDINATE WITH OWNER TO COMPENDENT STOCKPILE AREAS OUTSIDE OF MATERWAYS AND WETLANDS, SUBJECT TO APPROVAL. COORDINATE WITH OWNER TO A TO APPROVE AND A A AND A AND

WITH OWNER TO IDENTIFY STOCKPILE AREAS. LOCATE PILES SO AS NOT TO AFFECT THE OPERATION OF THE EXISTING OPERATIONS, OR

12. TAKE PRECAUTIONS TO PRESERVE, IN A SOUND CONDITION, THE MATERIAL BELOW AND BEYOND THE LINES OF ALL EXCAVATIONS. 13. PERFORM OPERATIONS SO THAT THE EXCAVATIONS WILL YIELD AS MUCH SUITABLE MATERIAL FOR CONSTRUCTION PURPOSES AS

PERFORM OPERATIONS SO THAT THE EXCAVATIONS WILL YIELD AS MUCH SUITABLE MATERIAL FOR CONSTRUCTION PURPOSES AS PRACTICABLE.
 REUSE, AS MUCH AS IS PRACTICABLE, ALL SUITABLE MATERIALS FROM REQUIRED EXCAVATION IN THE PERMANENT CONSTRUCTION. SEPARATE UNSUITABLE MATERIALS NO REMOVE THEM FROM THE WORK AREA AS SOON AS PRACTICABLE.
 SPREAD OUT AND ALLOW MATERIALS TO DRY THAT ARE TOO WET FOR IMMEDIATE COMPACTION UNTIL THE WATER CONTENT IS REDUCED SUFFICIENTLY FOR PLACEMENT IN THE EMBANKMENT. AERATING AND DRYING IS INCIDENTAL TO THE WORK.
 WATER-CONDITION MATERIALS THAT ARE TOO DRY FOR IMMEDIATE COMPACTION. MOISTURE CONDITIONING IS INCIDENTAL TO THE WORK.
 WATER-CONDITION MATERIALS THAT ARE TOO DRY FOR IMMEDIATE COMPACTION. MOISTURE CONDITIONING IS INCIDENTAL TO THE WORK.
 WATER-CONDITION MATERIALS THAT ARE TOO DRY FOR IMMEDIATE COMPACTION. MOISTURE CONDITIONING IS INCIDENTAL TO THE WORK.
 REMCVE SOFT, WET, OBJECTIONABLE, OR OTHERINSE UNSUITABLE MATERIALS AS DETERMINED BY THE ENGINEER.
 DE-WATER AS NECESSARY TO PREVENT THE ACCUMULATION AGAINST OR THE INTERMINGLING OF WATER WITH THE FILL.
 PERFORM EXCAVATION AND PLACEMENT OPERATIONS SUCH THAT THE EMBANKMENT MATERIALS ARE MIXED AND BLENDED TO PROVIDE THE MOST HOMOGENEOUS SECTION AND BEST DEGREE OF COMPACTION AND STABILITY PRACTICAL. ALL FILL SHOULD BE PLACED IN HORIZONTAL LIFTS AND COMPACTED TO AT LEAST 95% OF ASTM D-698. PROVIDE PRIMARY WATER CONDITIONING, MIXING AND BLENDED TO AT LEAST 95% OF ASTM D-698. PROVIDE PRIMARY WATER CONDITIONING, MIXING AND BLENDED TO AT LEAST 95% OF ASTM D-698. PROVIDE PRIMARY WATER CONDITIONING, MIXING AND BLENDED LO STRUEDUN FROM THE SURROUNDING FILL.
 CONTAMINATION, SEGREGATION, AND PARTICLE BREAKDOWN.
 CONTAMINATION, SEGREGATION, AND PARTICLE BREAKDOWN.
 CONTAMINATION SEGREGATION, AND PARTICLE BREAKDOWN.
 CORTRACTOR SHALL COORDINATE DRY UTILITY CONDUIT LOCATIONS, MADATION FROM THE SURGUN

26. IF APPLICABLE, CONTRACTOR SHALL BE RESPONSIBLE FOR ENSURING THAT ALL STORM WATER POLLUTION PREVENTION PLAN (SWPPP) REQUIREMENTS ARE MET.

28. PROJECT SITE DEVELOPMENT MAY REQUIRE ADDITIONAL STORM WATER FACILITY IMPROVEMENTS (SWALES, PONDS, ROADSIDE DITCH

HORSE CREEK HILLS SUBDIVISION C-0 COVER SHEET

UTILITY NOTE: UNDERGROUND UTILITIES SHOWN HEREON ARE BASED ON ONE-CALL UTILITY LOCATIONS, PRIVATE LINES ARE NOT LOCATED BY ONE-CALL. EASEMENT NOTE: THE SHOWN EASENTS MAY NOT BE ALL INCLUSIVE AND MAY NOT REFLECT ANY EASEMENT VACATIONS/ABANDONEMENTS THAT MAY HAVE TAKEN PLACE. CONDITIONS NOTE: CONDITIONS SHOWN ARE AS THEY EXISTED WHEN FIELD SURVEY WAS PERFORMED ON _____ . 20____ DATUM NOTE: VERTICAL DATUM IS NAVD88.

BASIS OF BEARING, COORDINATES BEARINGS SHOWN ARE MONTANA STATE PLANE GRID. DISTANCES ARE GROUND DISTANCES IN INTERNATIONAL FEET.

MONTANA COORDINATE SYSTEM NAD 83 HORIZONTAL DATUM: BOZEMAN CONTINUOUSLY OPERATING REFERENCE STATION

 Display
 Designation

 DP4103
 IDDU
 DUBOIS
 CORS
 ARP

 DM7133
 MTLW
 LEWISTOWN
 CORS
 ARP

 DG9745
 MTEI
 ENGINC
 CORS
 ARP

MONTANA STATE PLANE NAD 83 (2011)(EPOCH: 2010.0000) NORTH LATITUDE 45'46'36.41912" WEST LONGITUDE 111'04'57.06703" TS: INTERNATIONAL FEET UNITS: Convergence angle: -01'09'27"

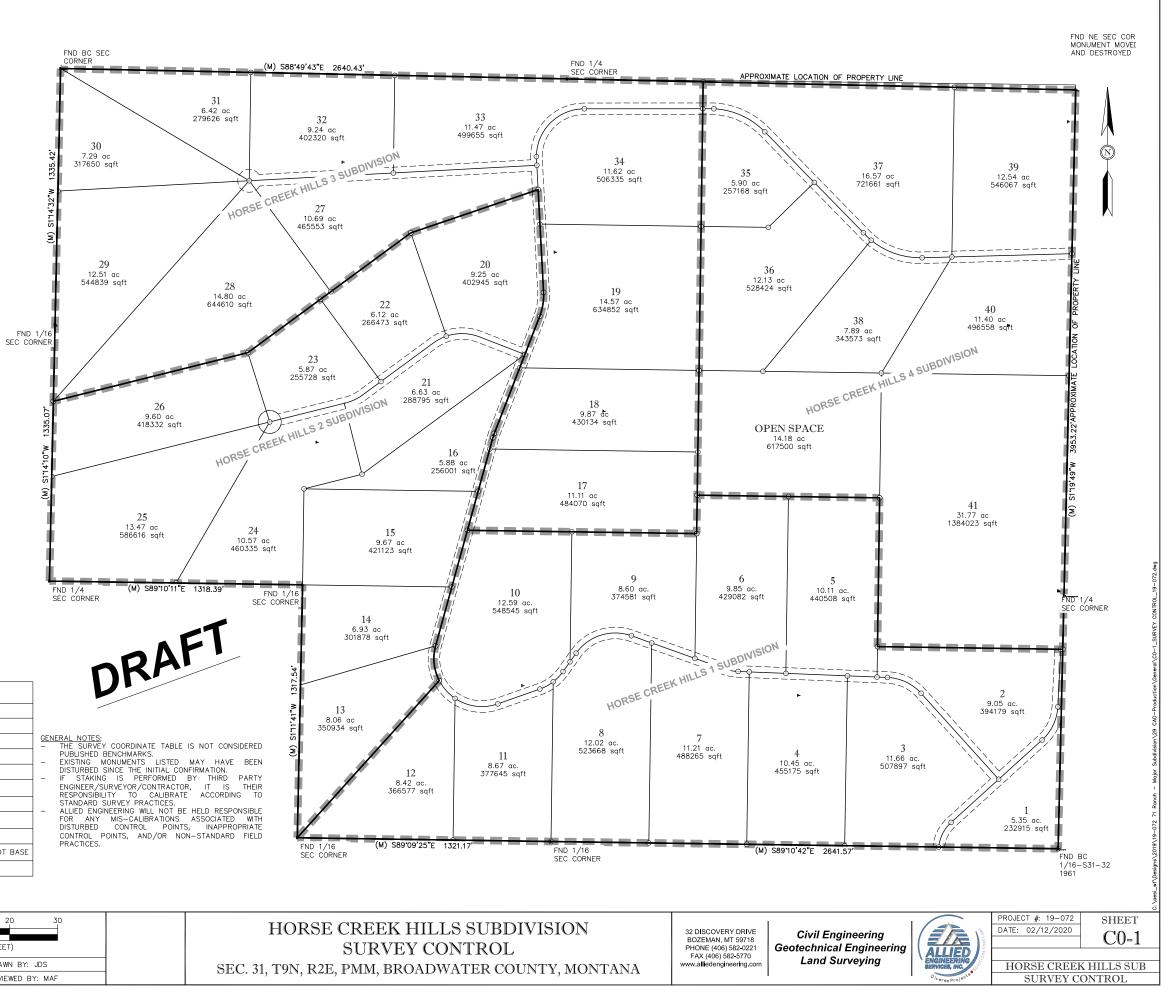
LEGEND

	INDEX CONTOUR
	CONTOUR MINOR (1' INTERVALS)
	PROPERTY LINE
	EASEMENT LINE
x	BARB WIRE FENCE
D	WOOD FENCE
OHP	OVERHEAD POWER
G	UNDERGROUND GAS
TEL	UNDERGROUND PHONE
— Е ——	UNDERGROUND ELECTRIC
	ROAD CENTERLINE
	EDGE OF PAVEMENT
	EDGE OF GRAVEL
	EDGE OF BUILDING
٠	FOUND MONUMENT AS NOTED
\triangle	CONTROL POINT
*	BENCHMARK
\odot	WATER WELL
_	STREET SIGN
م	POWER POLE
_	GUY ANCHOR
2	ELECTRICAL PEDESTAL
EM	ELECTRICAL METER
E	TELEPHONE PEDESTAL
×28 80	GAS METER
× S	GAS VALVE
	TEST PIT
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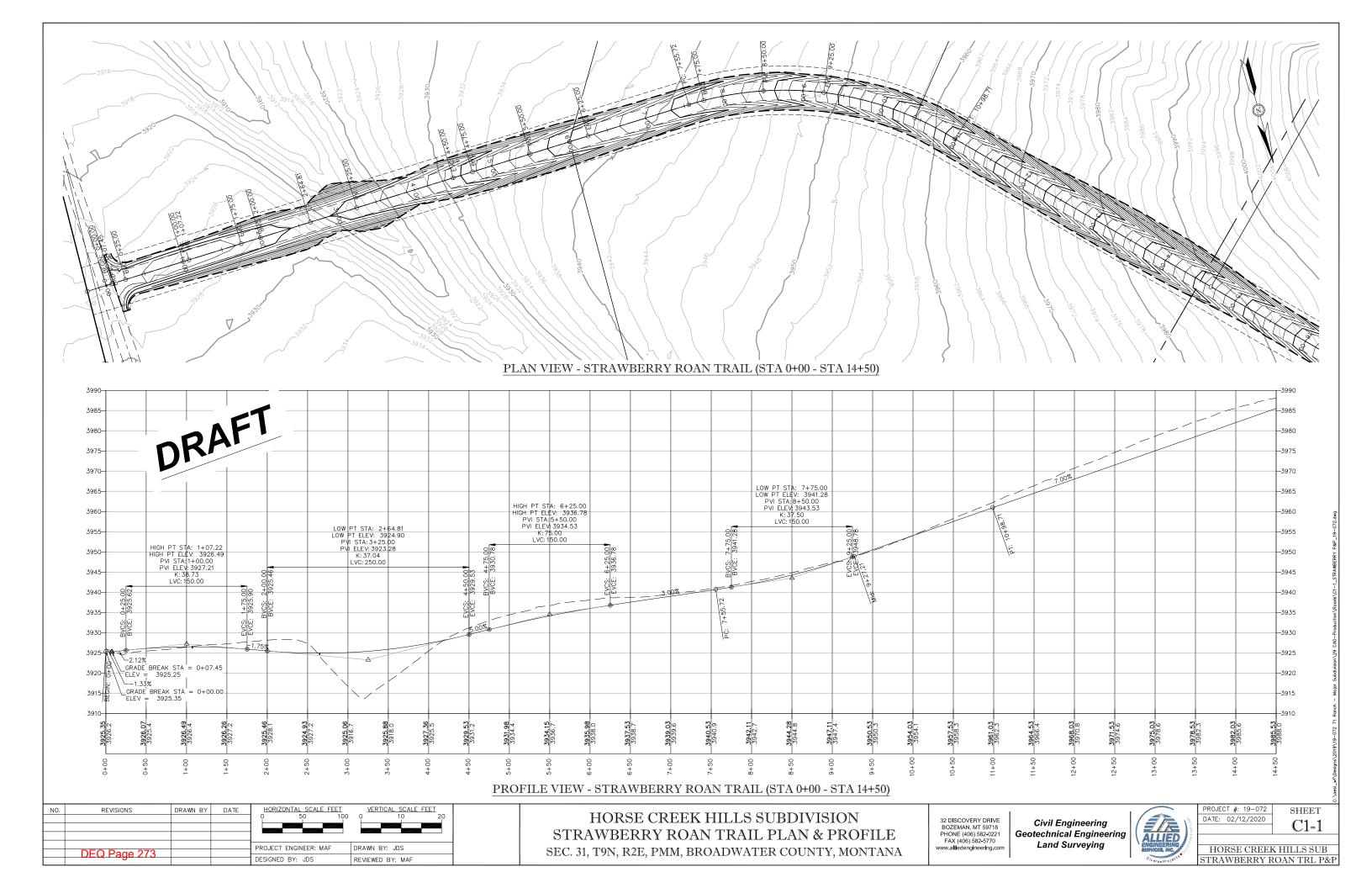
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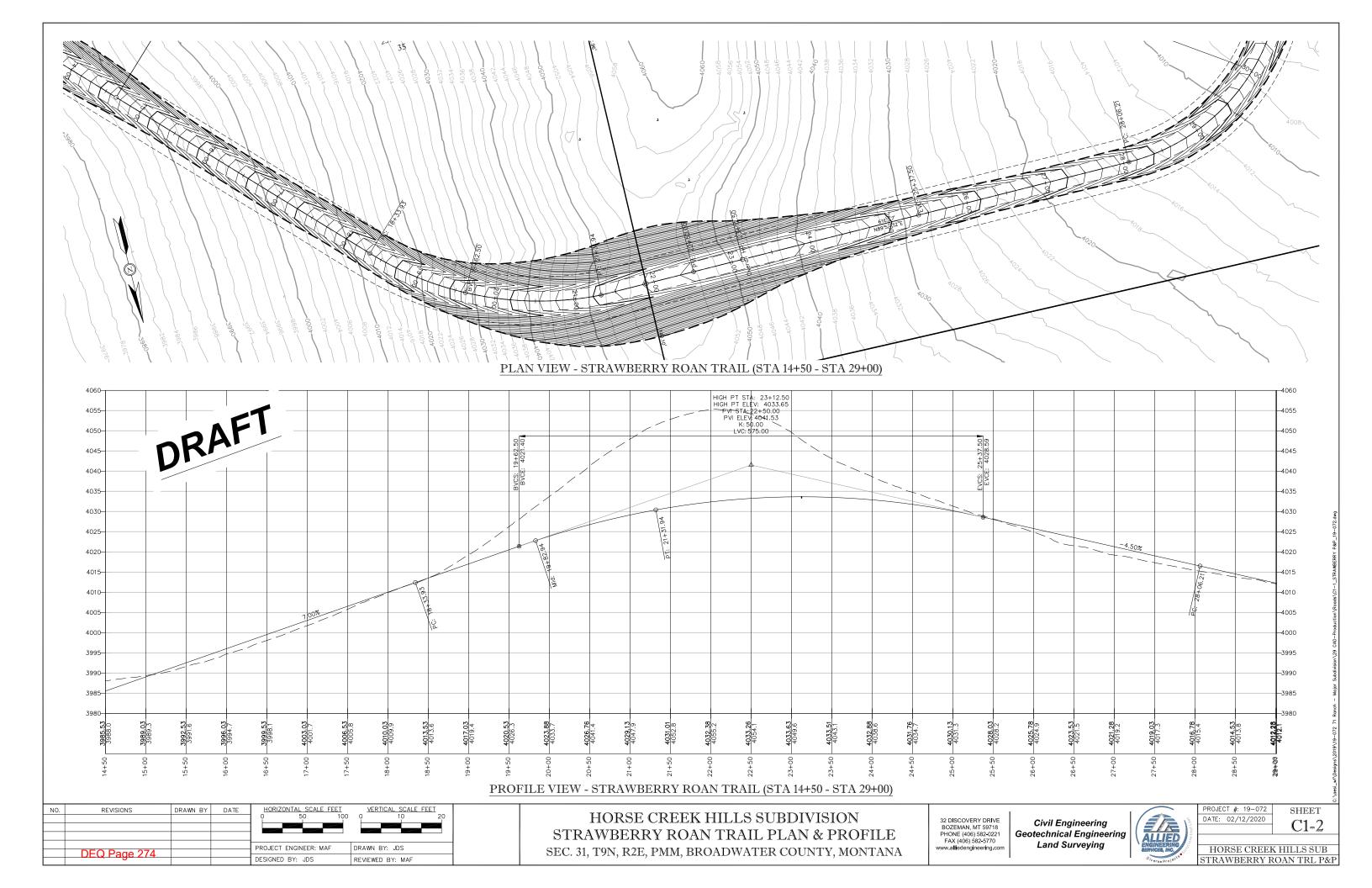
SURVEY CONTROL COORDINATE TABLE

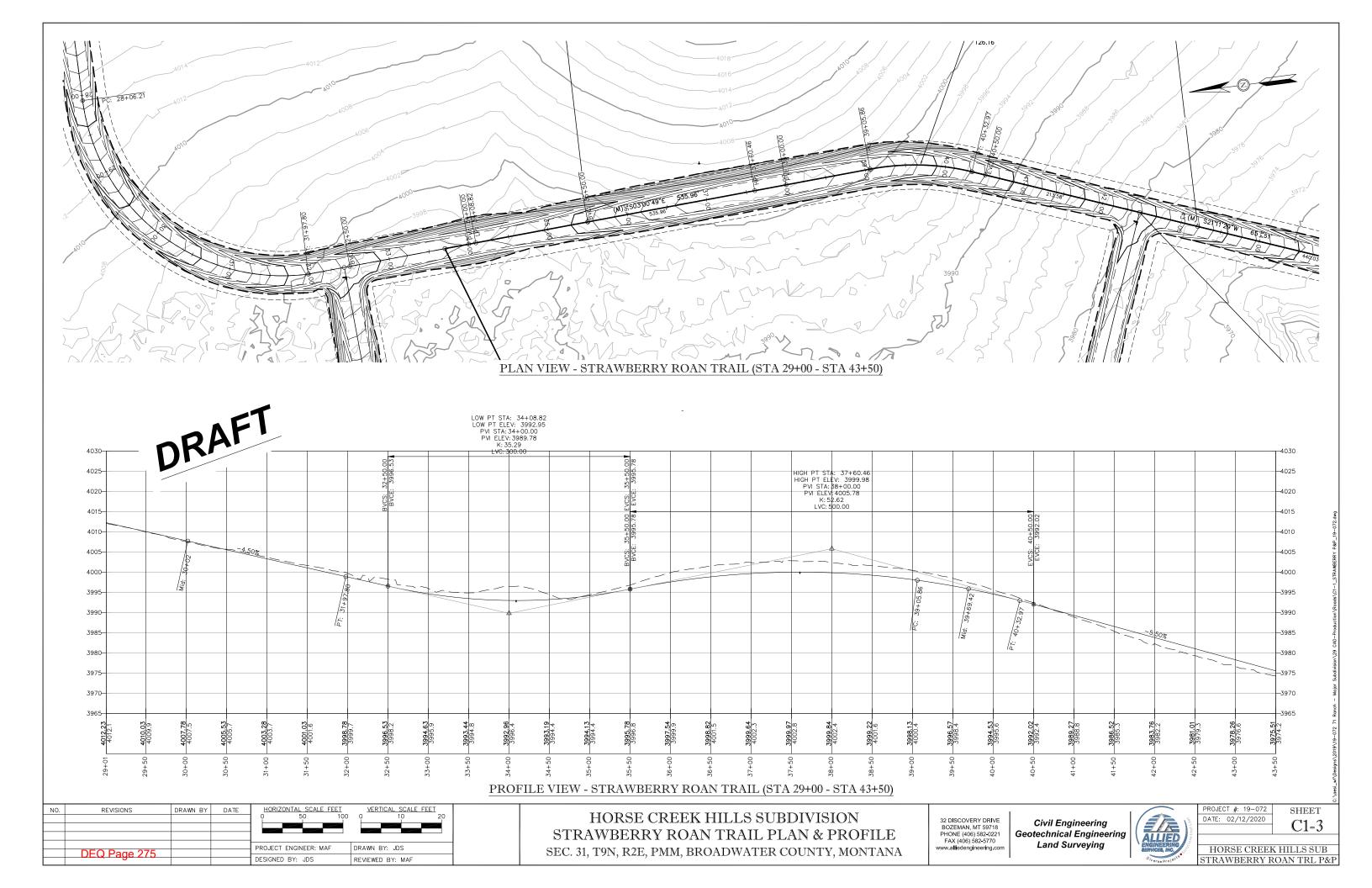
POINT NUMBER	NORTHING	EASTING	ELEVATION	DESCRIPTION
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84	823,441.13	1,457,630.01	3,889.45	6006
85	824,758.38	1,457,657.48	3,905.52	6005
86	824,777.48	1,456,339.22	3,816.10	6004
87	826,112.24	1,456,368.03	3,880.19	1/16 COR
88	827,393.36	1,459,036.85	4,016.18	6002
714	823,383.80	1,461,592.33	3,825.13	BC S1/16-S31-32-1961
755	827,447.34	1,456,396.97	3,897.86	BC SEC COR N T6
810	824,702.23	1,461,623.47	3,851.96	BC 1/4 COR 31/32 N BENT SHOT BASE
1000	827,335.96	1,461,684.10	3,970.62	CALC POINT

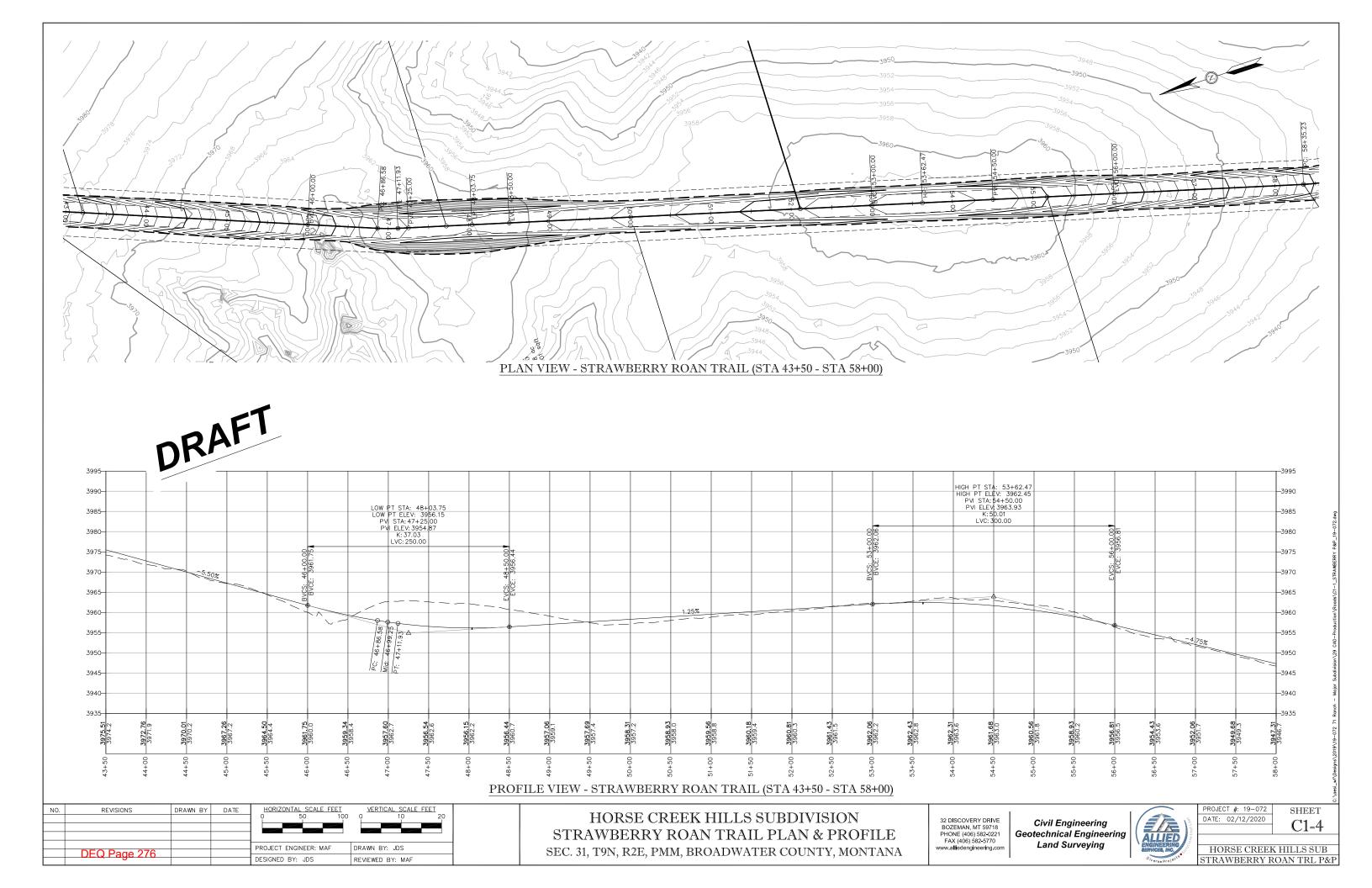


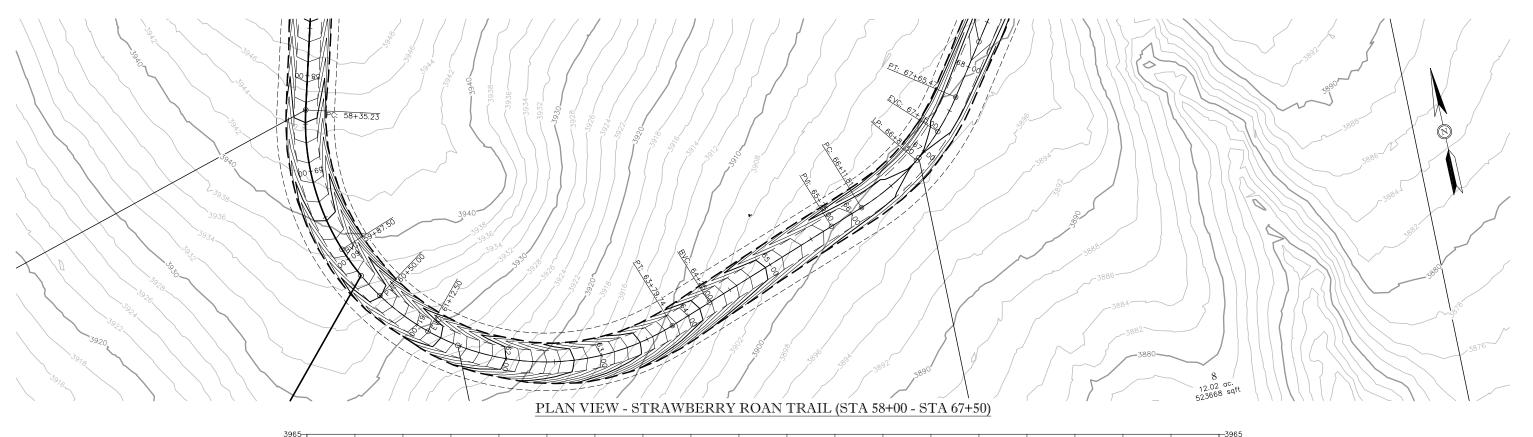
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				PROJECT ENGINEER: MAF	DRAWN BY: JDS
	DEO Page 272				
				DESIGNED BY: JDS	REVIEWED BY: MAF







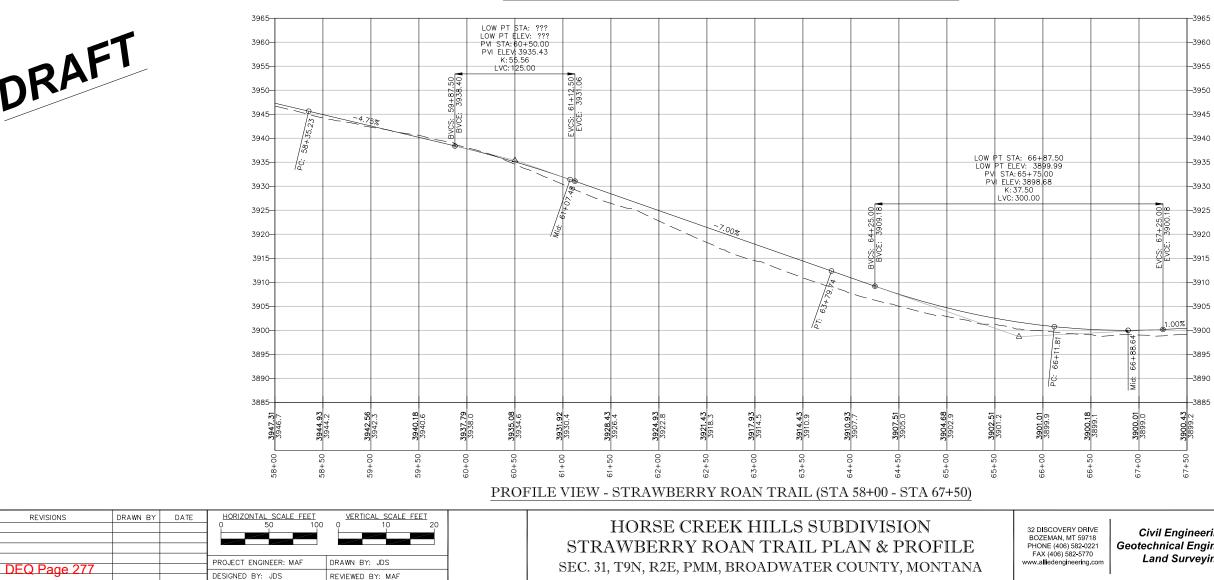






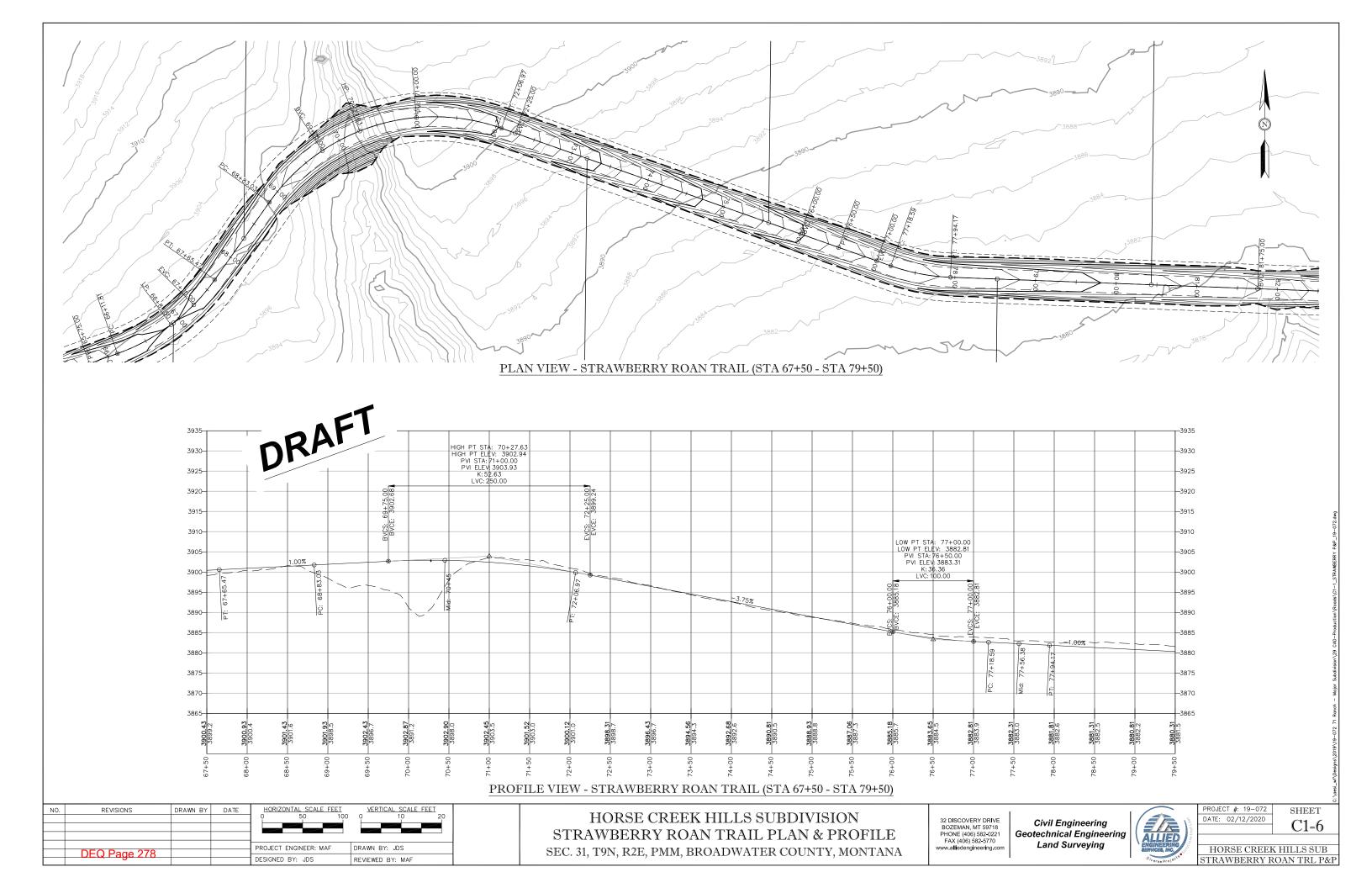
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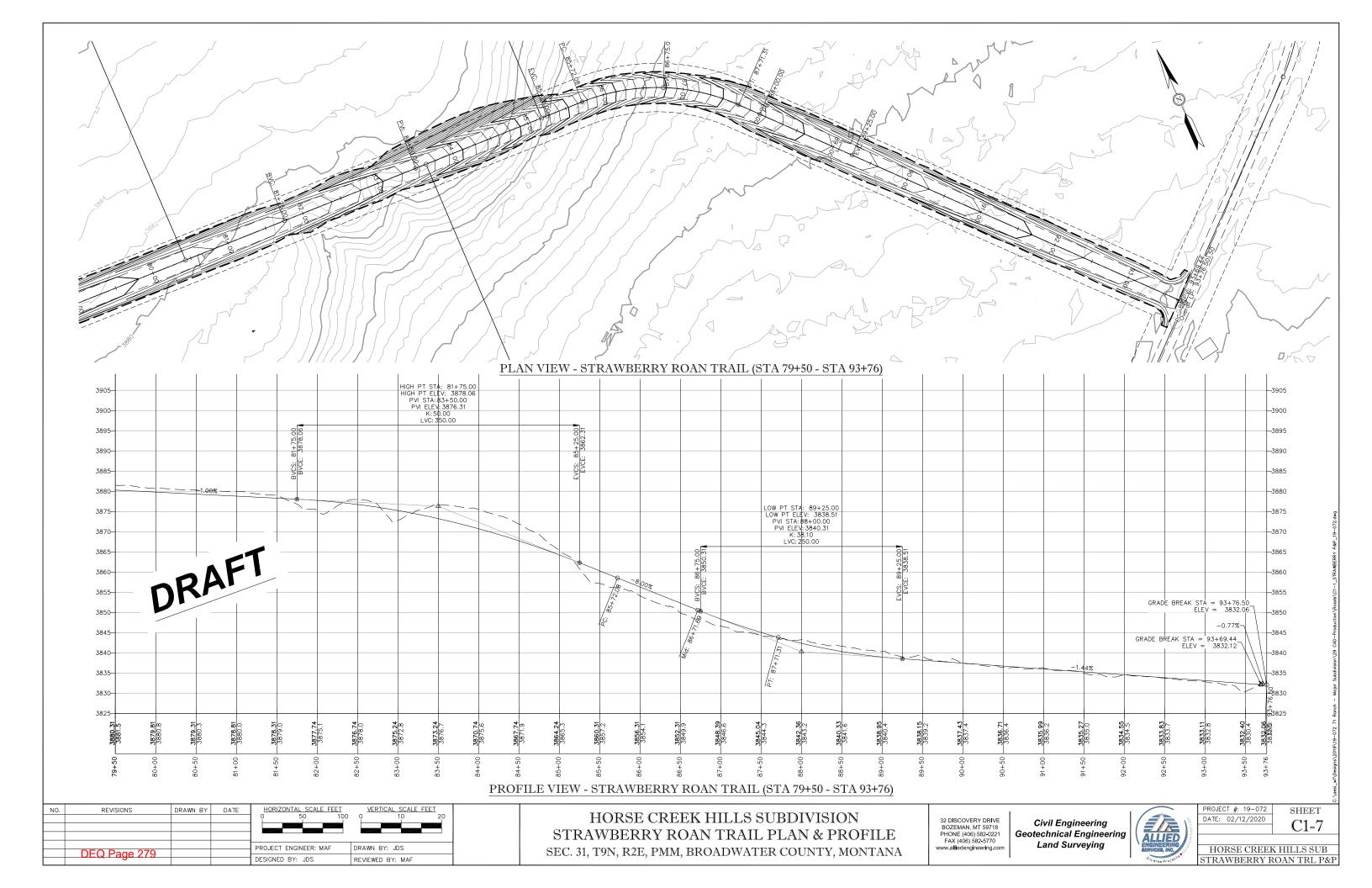
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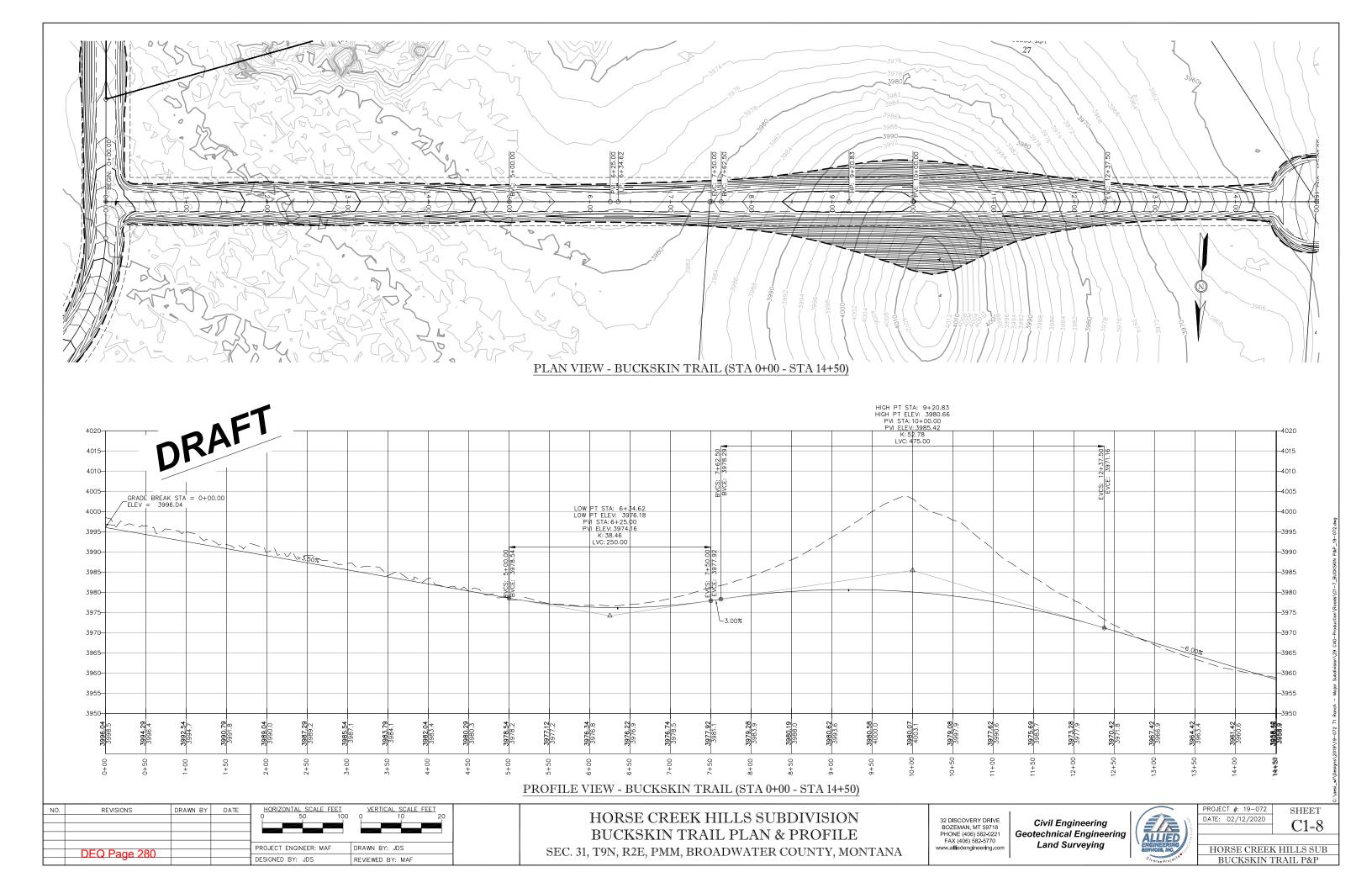


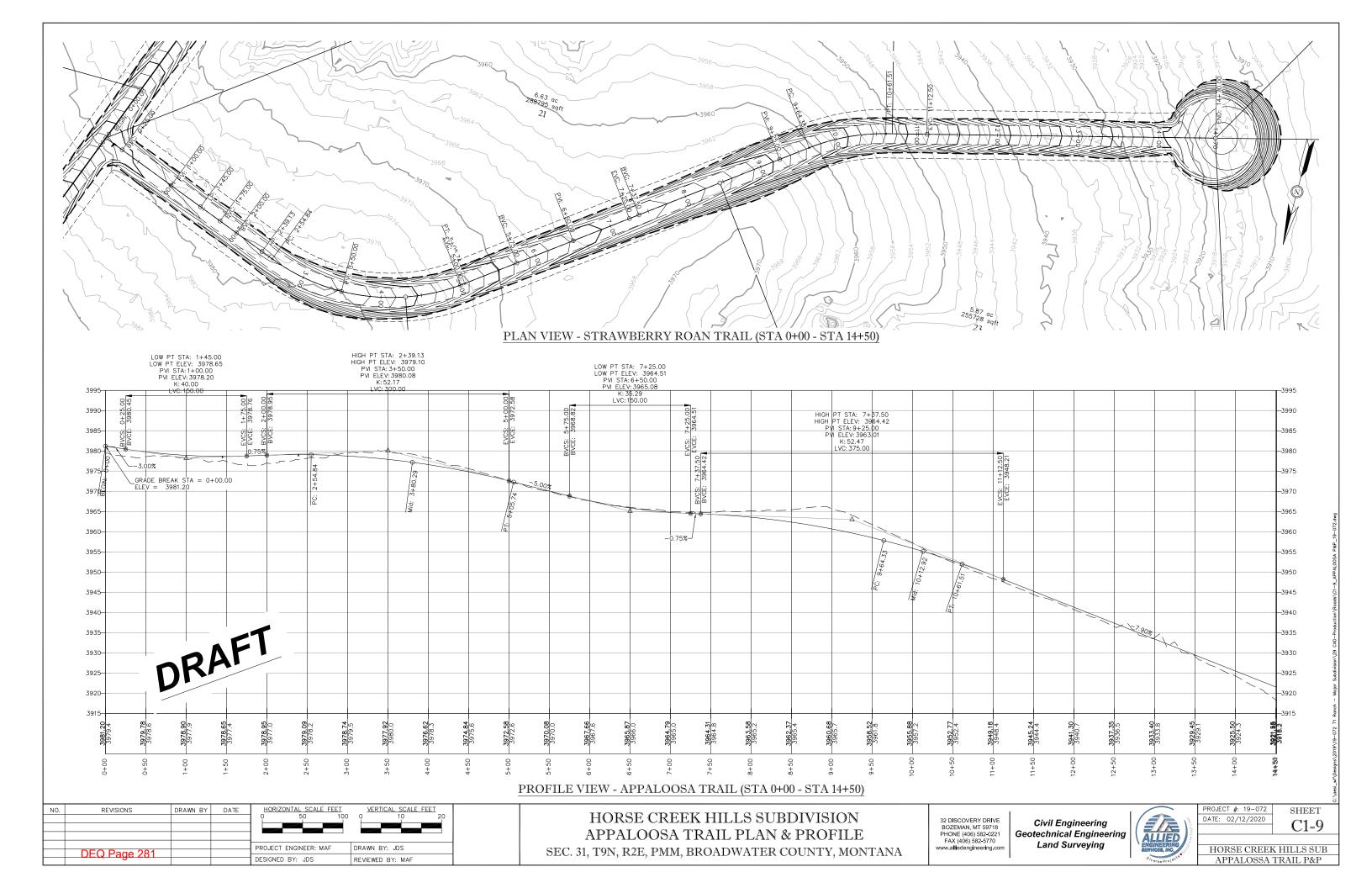


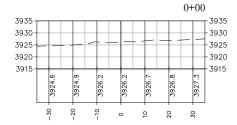
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PROJECT #: 19-072	SHEET
DATE: 02/12/2020	
	C1-5
HORSE CREE	K HILLS SUB
STRAWBERRY	ROAN TRL P&P

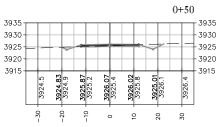


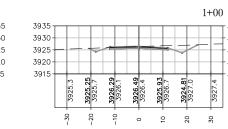


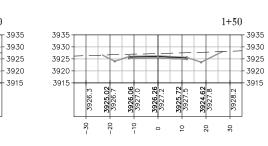


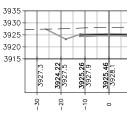


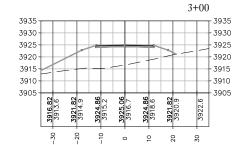


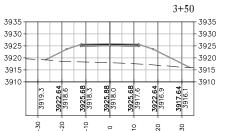






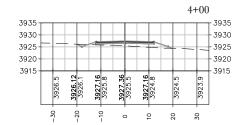


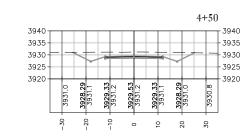


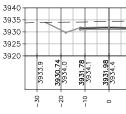


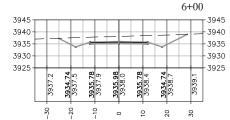
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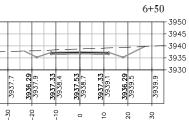
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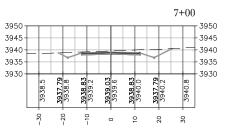


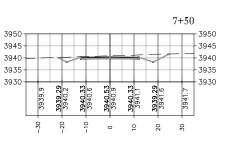


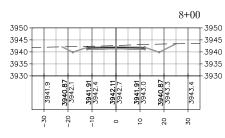




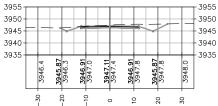








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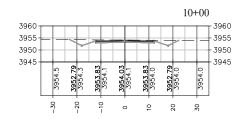
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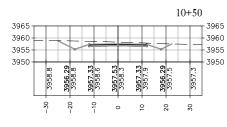
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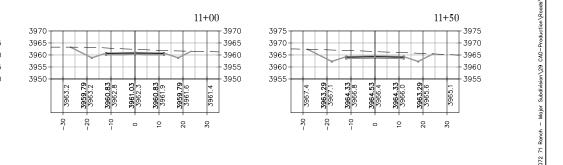
SCALE (FEET

DRAWN BY: JDS

REVIEWED BY: MAF







HORSE CREEK HILLS SUBDIVISION STRAWBERRY ROAN TRAIL CROSS-SECTIONS SEC. 31, T9N, R2E, PMM, BROADWATER COUNTY, MONTANA

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.cor

PROJECT ENGINEER: MAF

DESIGNED BY: JDS

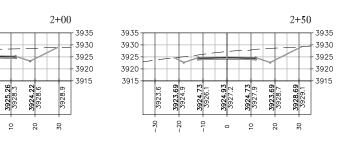
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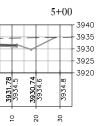
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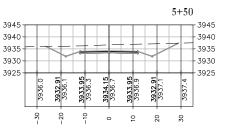
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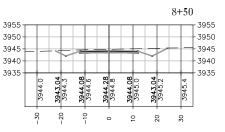
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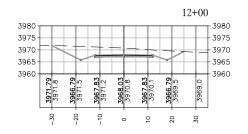


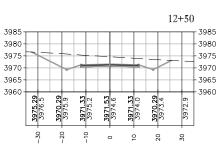






PROJECT #: 19-072	SHEET
DATE: 02/12/2020	CO 1
	C2-1
HORSE CREEF	K HILLS SUB
STRAWBERRY	ROAN X-SECs





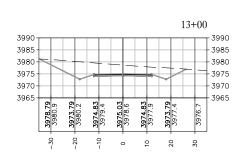
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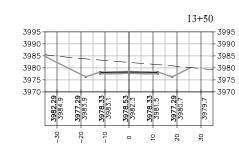
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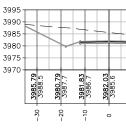
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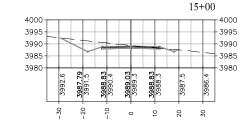
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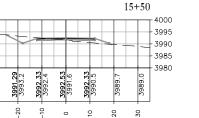
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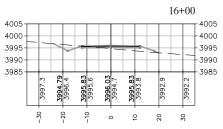


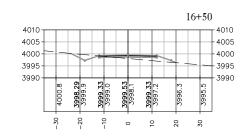


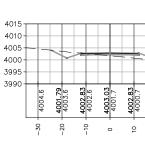


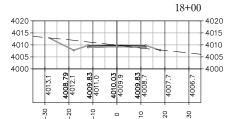


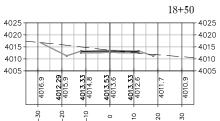


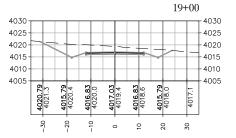


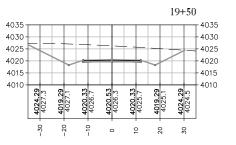


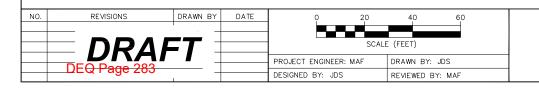






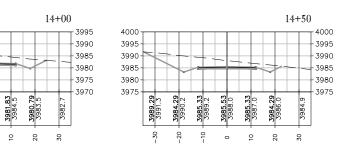


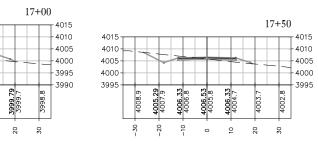




HORSE CREEK HILLS SUBDIVISION STRAWBERRY ROAN TRAIL CROSS-SECTIONS SEC. 31, T9N, R2E, PMM, BROADWATER COUNTY, MONTANA

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

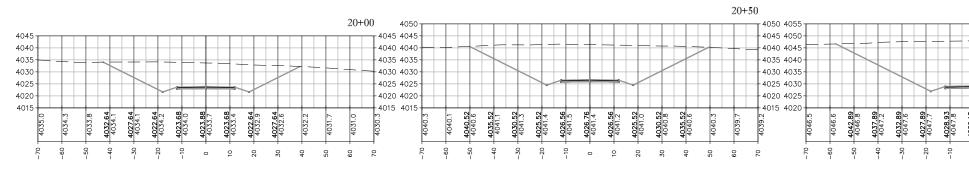


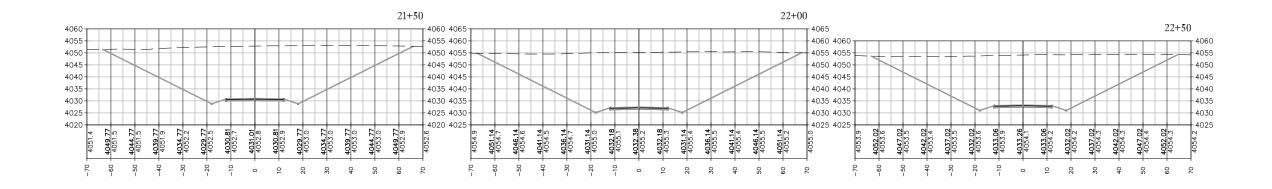


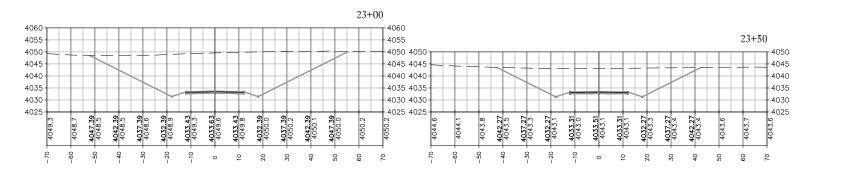


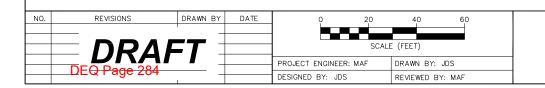


SHEET
C2-2
K HILLS SUB
ROAN X-SECs







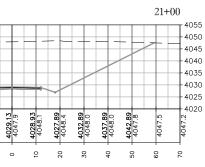


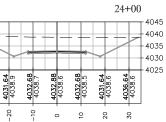
HORSE CREEK HILLS SUBDIVISION STRAWBERRY ROAN TRAIL CROSS-SECTIONS SEC. 31, T9N, R2E, PMM, BROADWATER COUNTY, MONTANA

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> 32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770

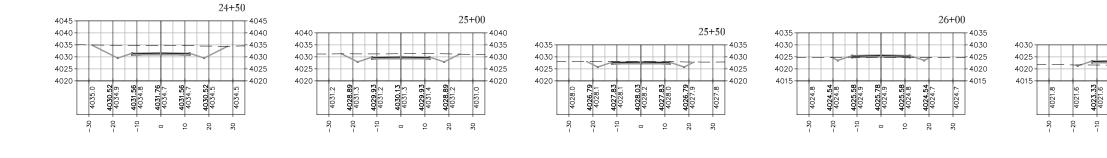
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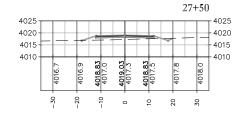




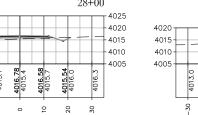


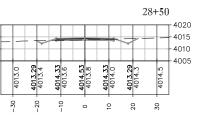
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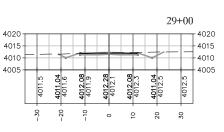


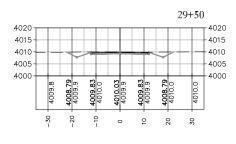


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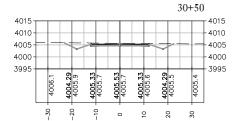


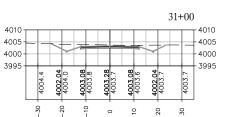


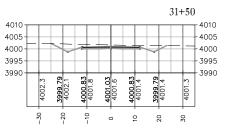


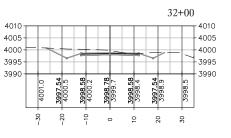
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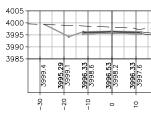
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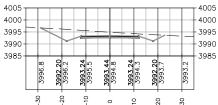












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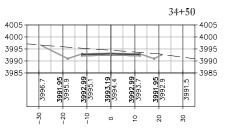
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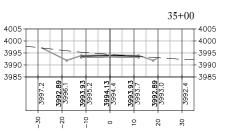
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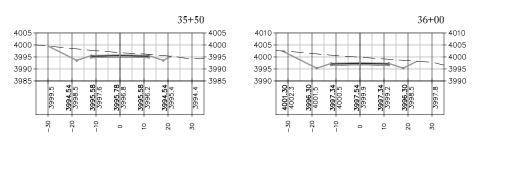
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DESIGNED BY: JDS

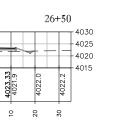












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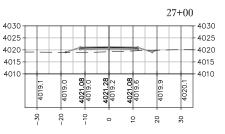
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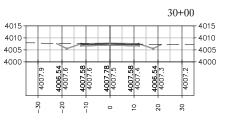
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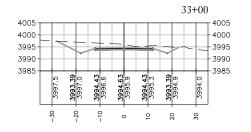
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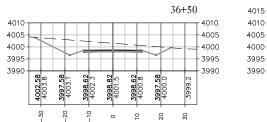


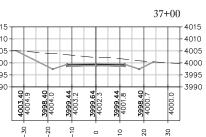


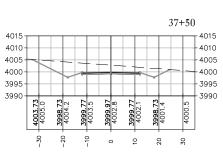


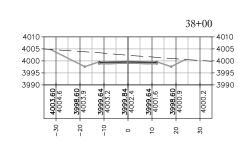


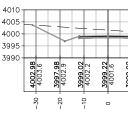
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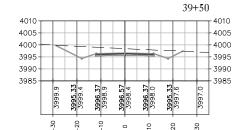


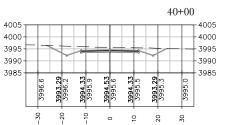


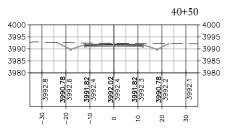


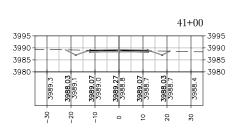


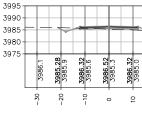


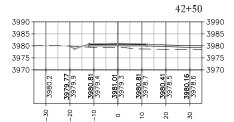


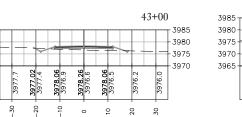












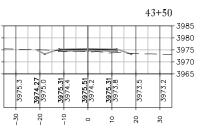
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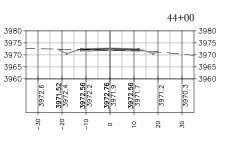
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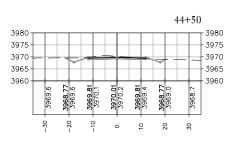
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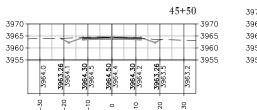
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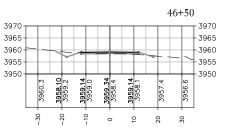
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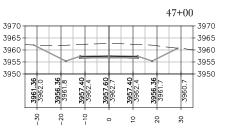
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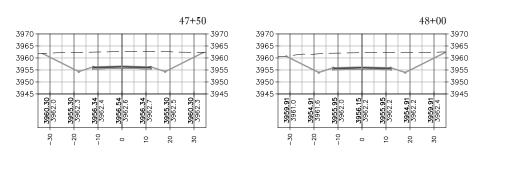
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DESIGNED BY: JDS

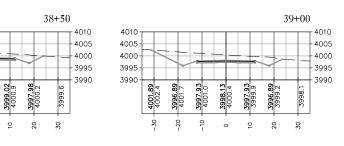


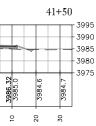


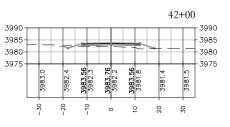


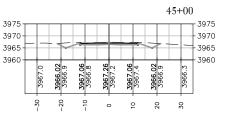
HORSE CREEK HILLS SUBDIVISION STRAWBERRY ROAN TRAIL CROSS-SECTIONS SEC. 31, T9N, R2E, PMM, BROADWATER COUNTY, MONTANA

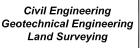
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com





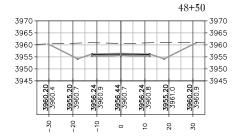


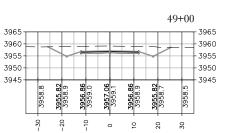


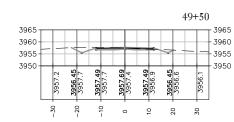


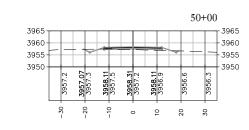


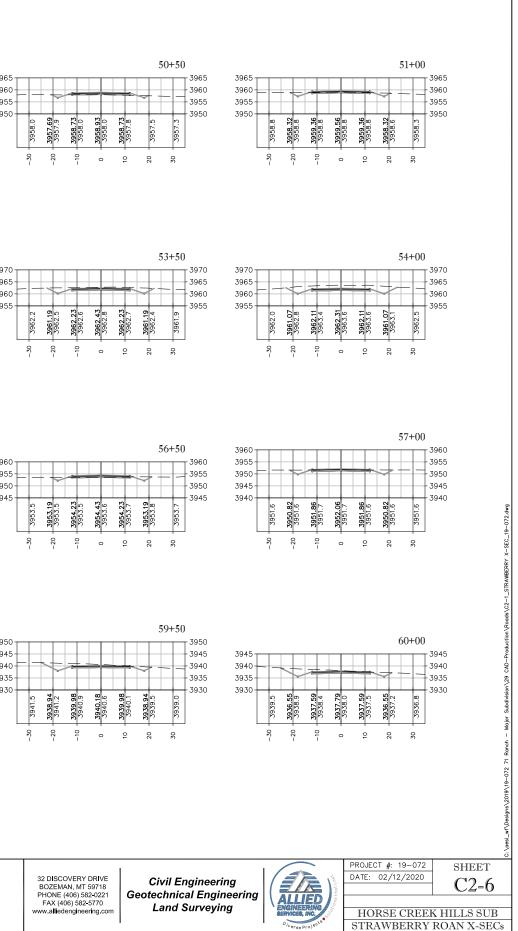
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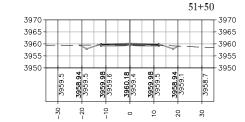


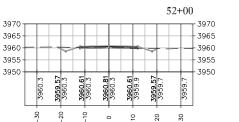












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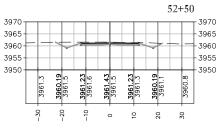
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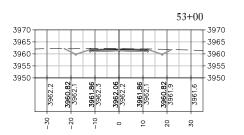
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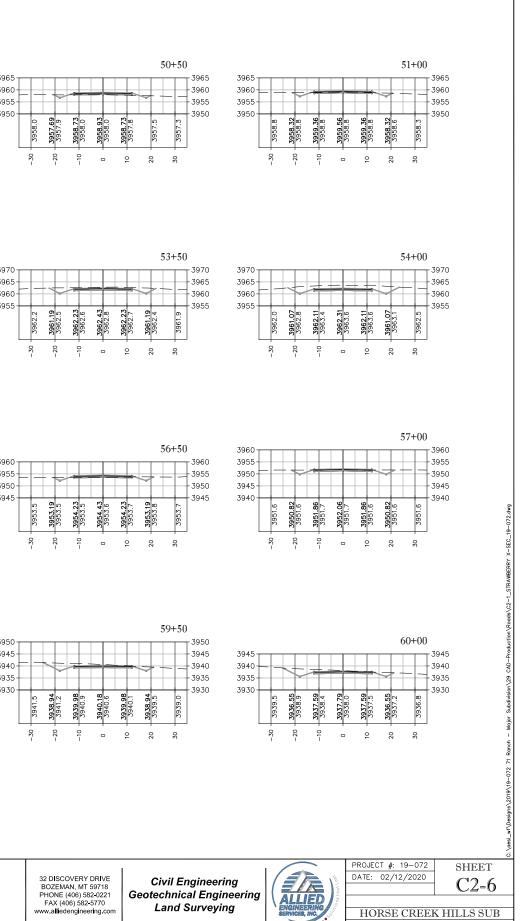
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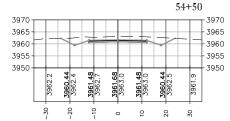
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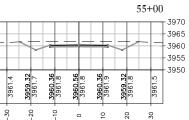
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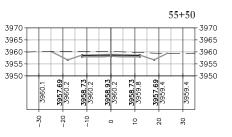


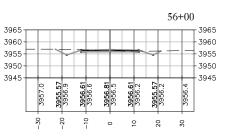


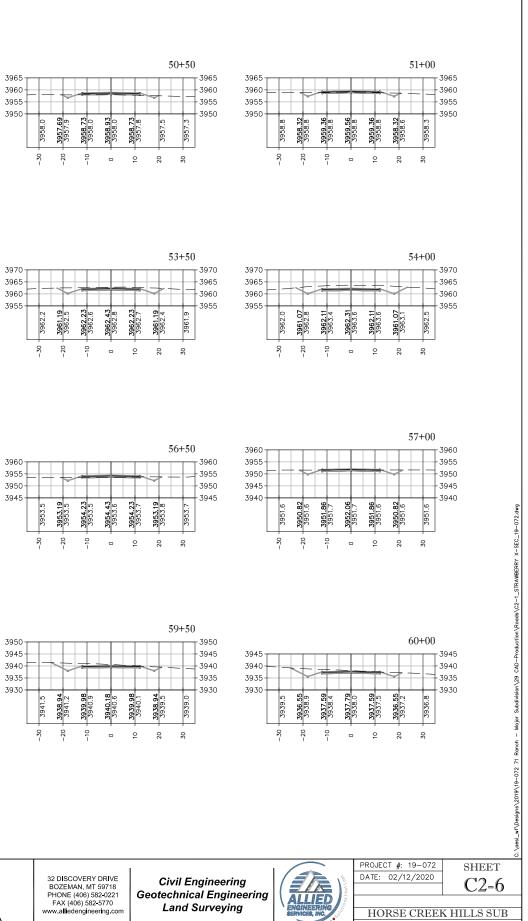


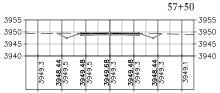












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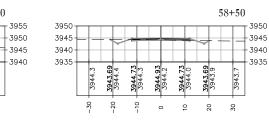
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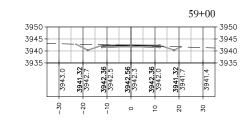
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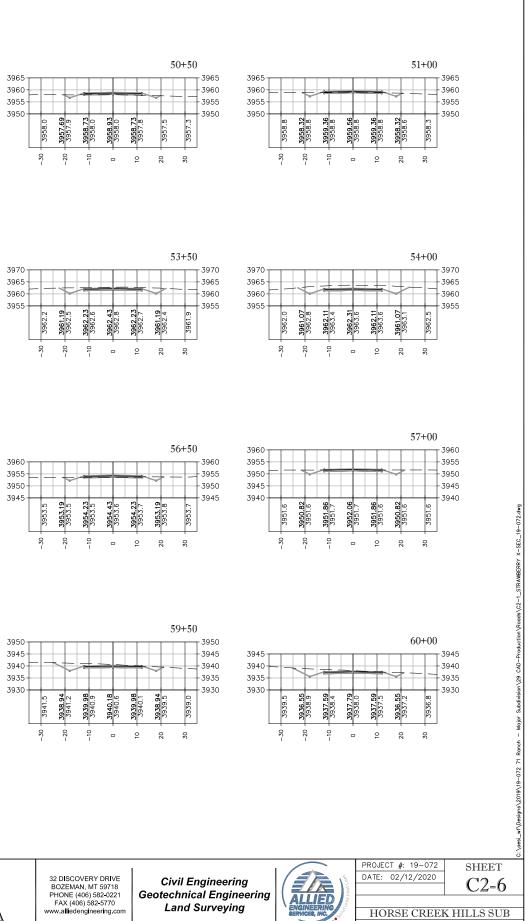
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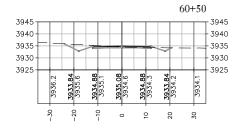
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HORSE CREEK HILLS SUBDIVISION STRAWBERRY ROAN TRAIL CROSS-SECTIONS SEC. 31, T9N, R2E, PMM, BROADWATER COUNTY, MONTANA



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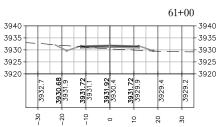
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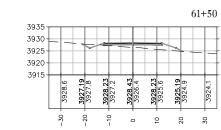
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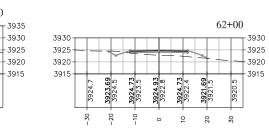
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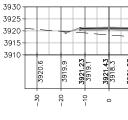
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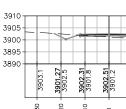
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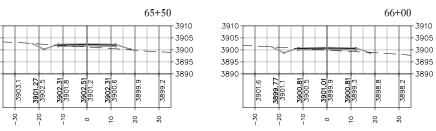
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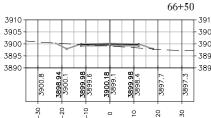
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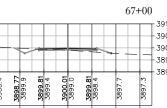
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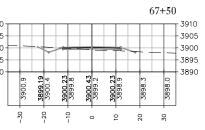
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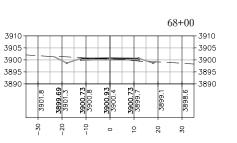
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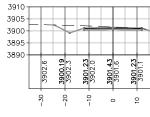
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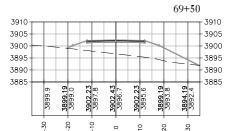
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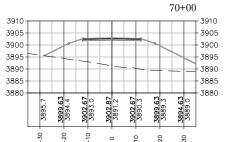
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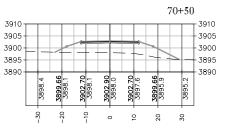
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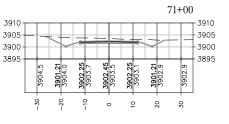


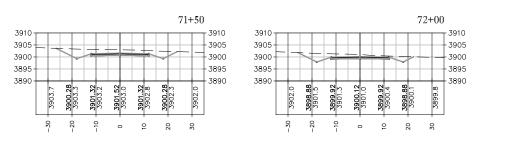


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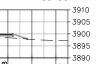






HORSE CREEK HILLS SUBDIVISION STRAWBERRY ROAN TRAIL CROSS-SECTIONS SEC. 31, T9N, R2E, PMM, BROADWATER COUNTY, MONTANA

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.cor



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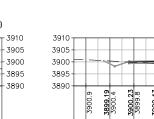
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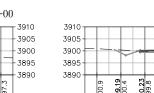
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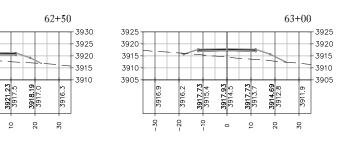
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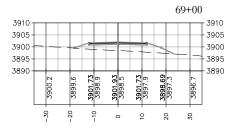
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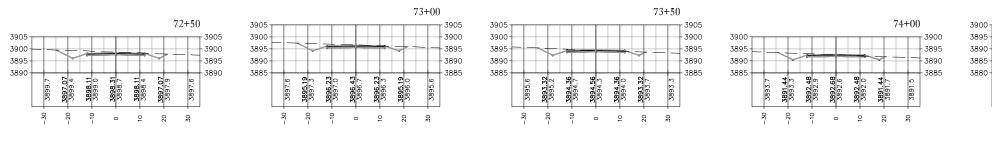
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PROJECT #: 19-072	SHEET
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HORSE CREEK HILLS SUB	
STRAWBERRY ROAN X-SECs	



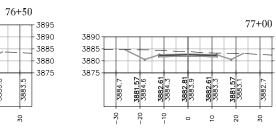
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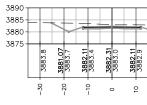
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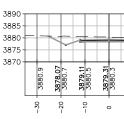
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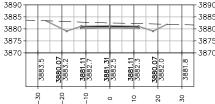
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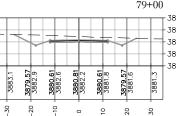
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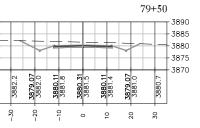


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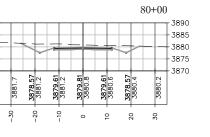


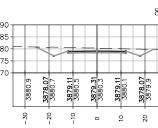
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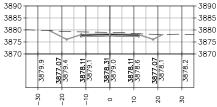
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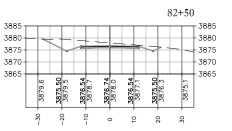
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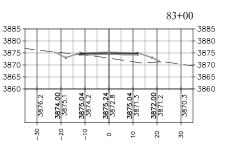
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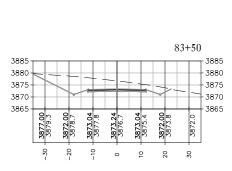
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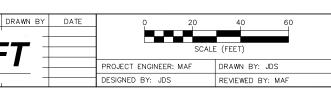




STRAWBERRY ROAN TRAIL CROSS-SECTIONS SEC. 31, T9N, R2E, PMM, BROADWATER COUNTY, MONTANA

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.cor

HORSE CREEK HILLS SUBDIVISION



- 3885 3880 - 3875 3870

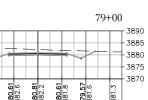
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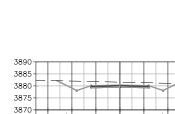
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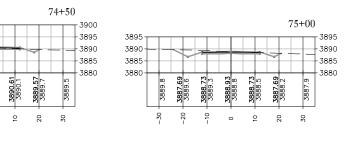


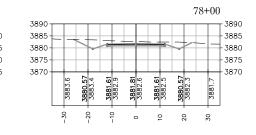
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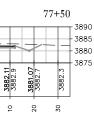
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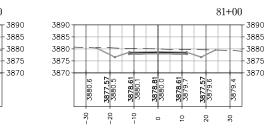


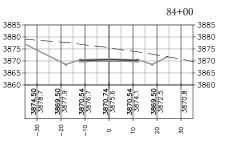
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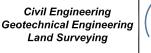
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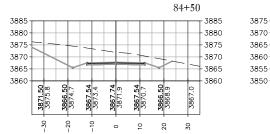


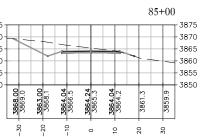


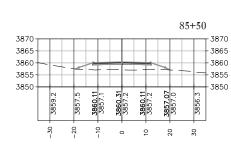


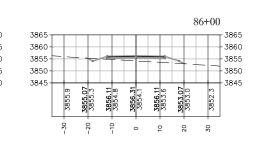


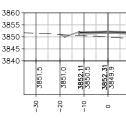
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ROJECT #: 19-072	SHEET
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HORSE CREEF	K HILLS SUB
STRAWBERRY	ROAN X-SECs

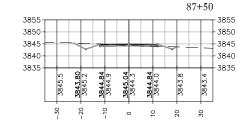




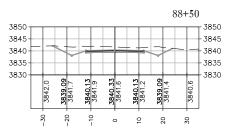


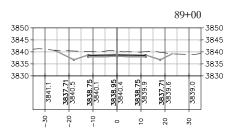


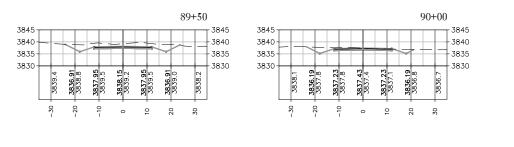


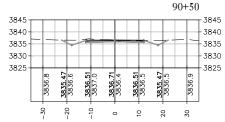


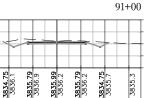
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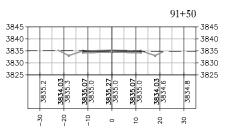
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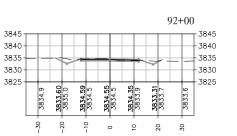
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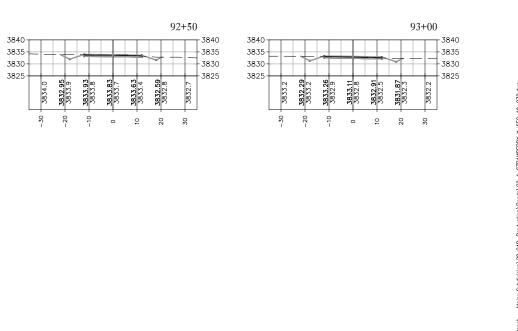
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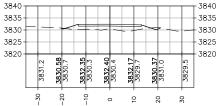
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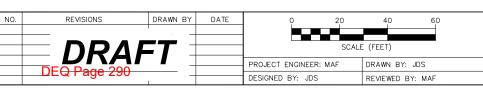
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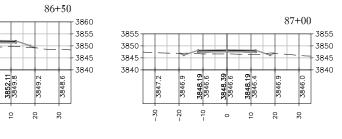


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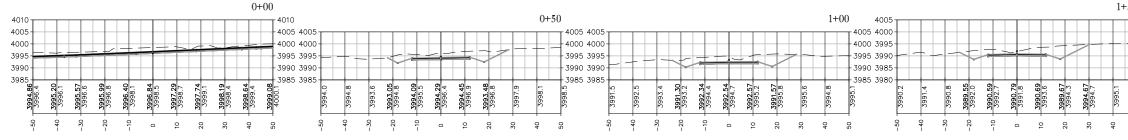
HORSE CREEK HILLS SUBDIVISION STRAWBERRY ROAN TRAIL CROSS-SECTIONS SEC. 31, T9N, R2E, PMM, BROADWATER COUNTY, MONTANA

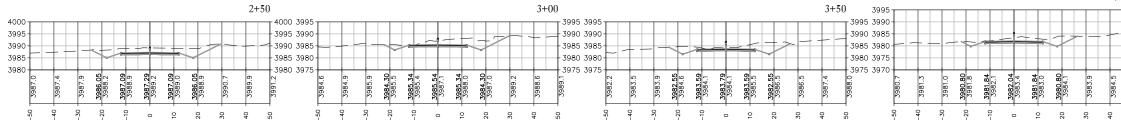
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

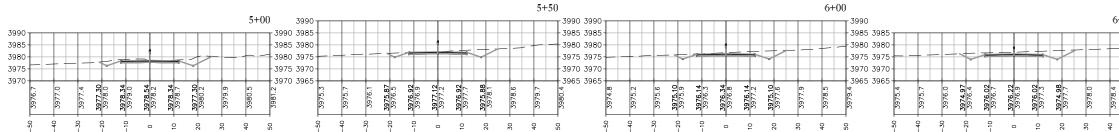


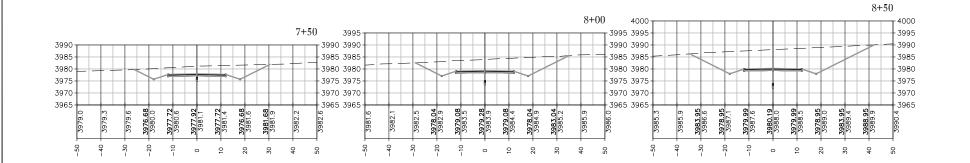


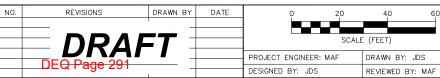
PROJECT #: 19-072	SHEET
DATE: 02/12/2020	C20
	C2-9
HORSE CREEF	K HILLS SUB
STRAWBERRY	ROAN X-SECs





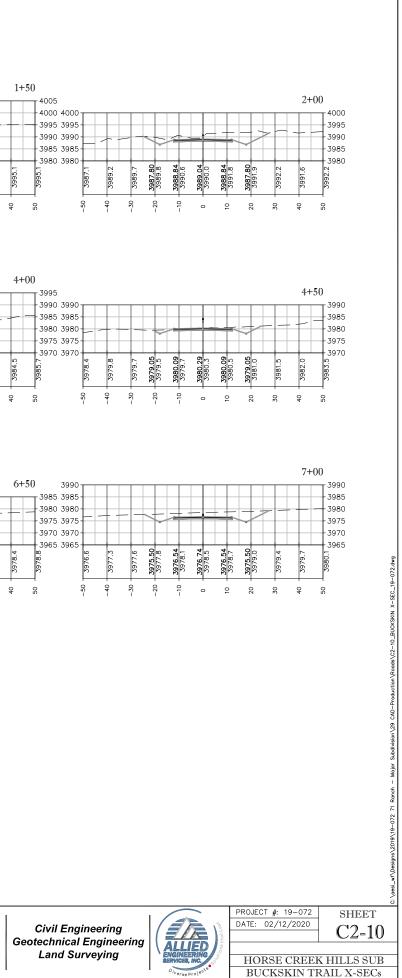


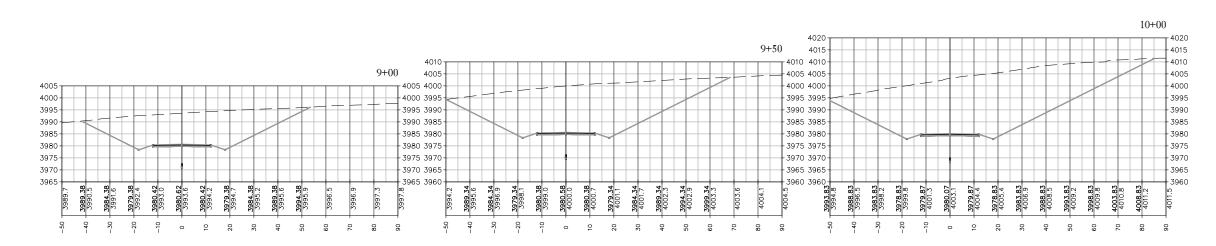


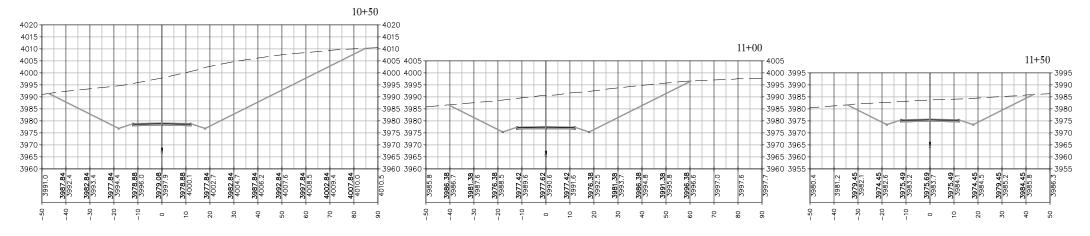


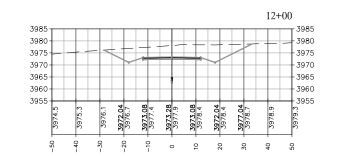
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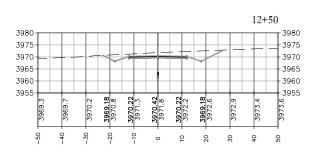
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

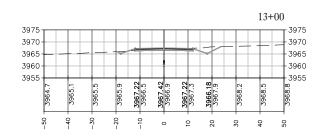


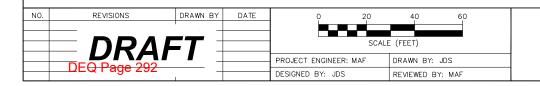










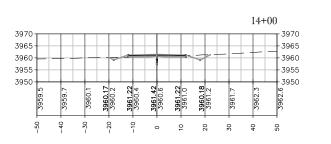


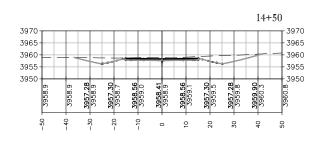
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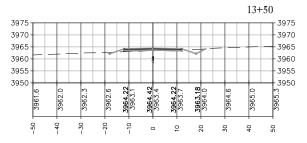
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

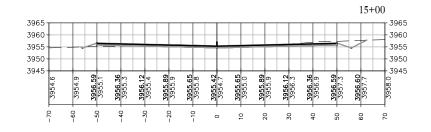


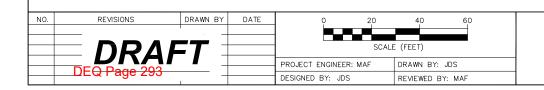
PROJECT #: 19-072	SHEET
DATE: 02/12/2020	CO 11
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HORSE CREEF	K HILLS SUB
BUCKSKIN TI	RAIL X-SECs







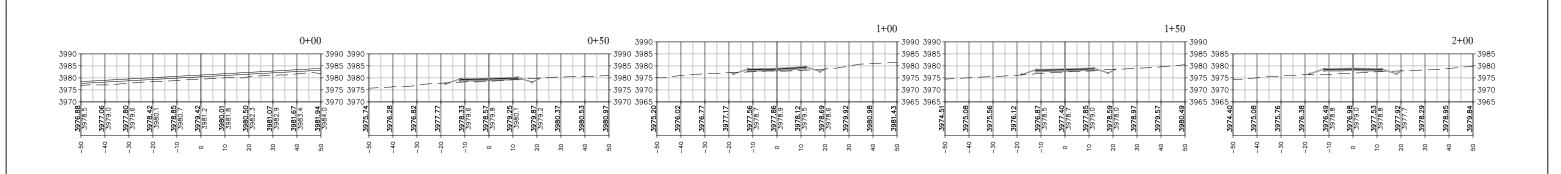


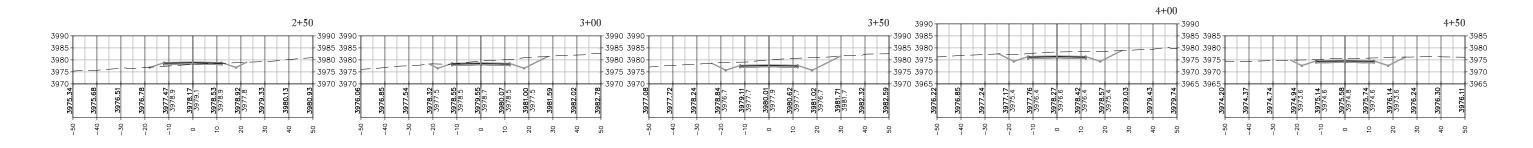


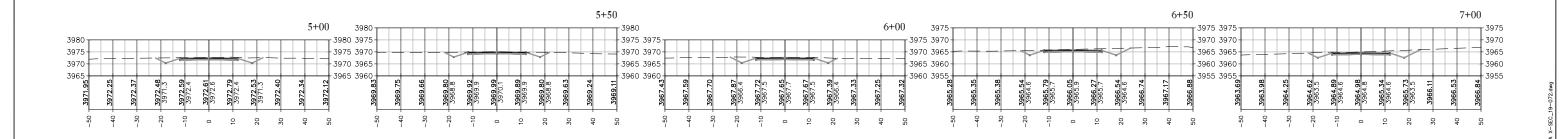
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

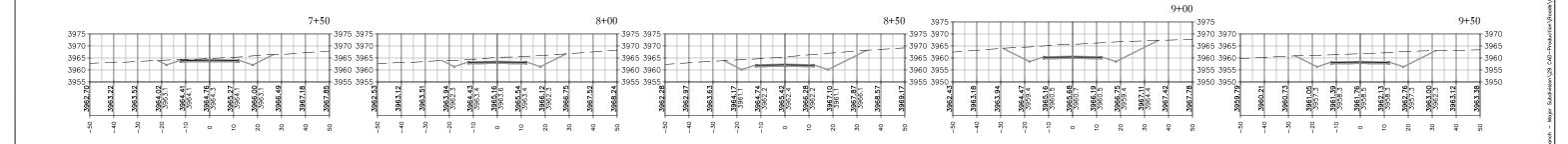


PROJECT #: 19-072	SHEET
DATE: 02/12/2020	CO 10
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HORSE CREEP	K HILLS SUB
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DEQ Page 294	– –		PROJECT ENGINEER	R: MAF	DRAWN BY:	JDS
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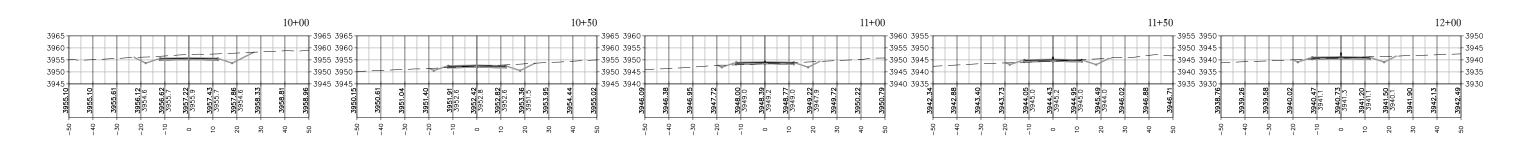
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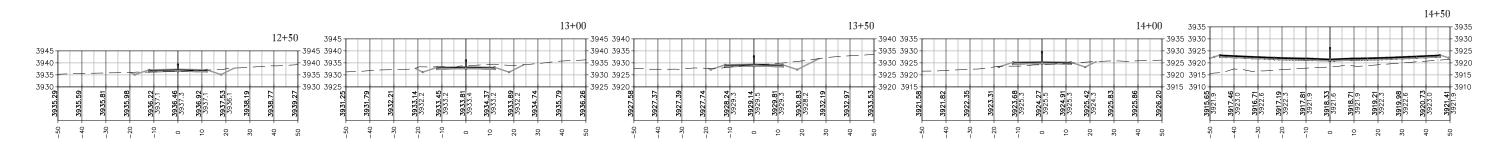
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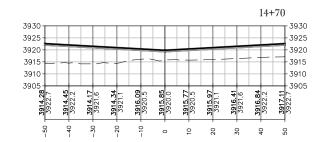
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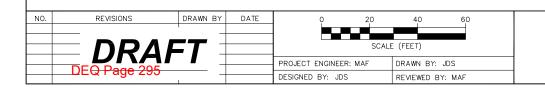


PROJECT #: 19–072 DATE: 02/12/2020 SHEET C2-13 HORSE CREEK HILLS SUB APPALOOSA TRAIL X-SECs









32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

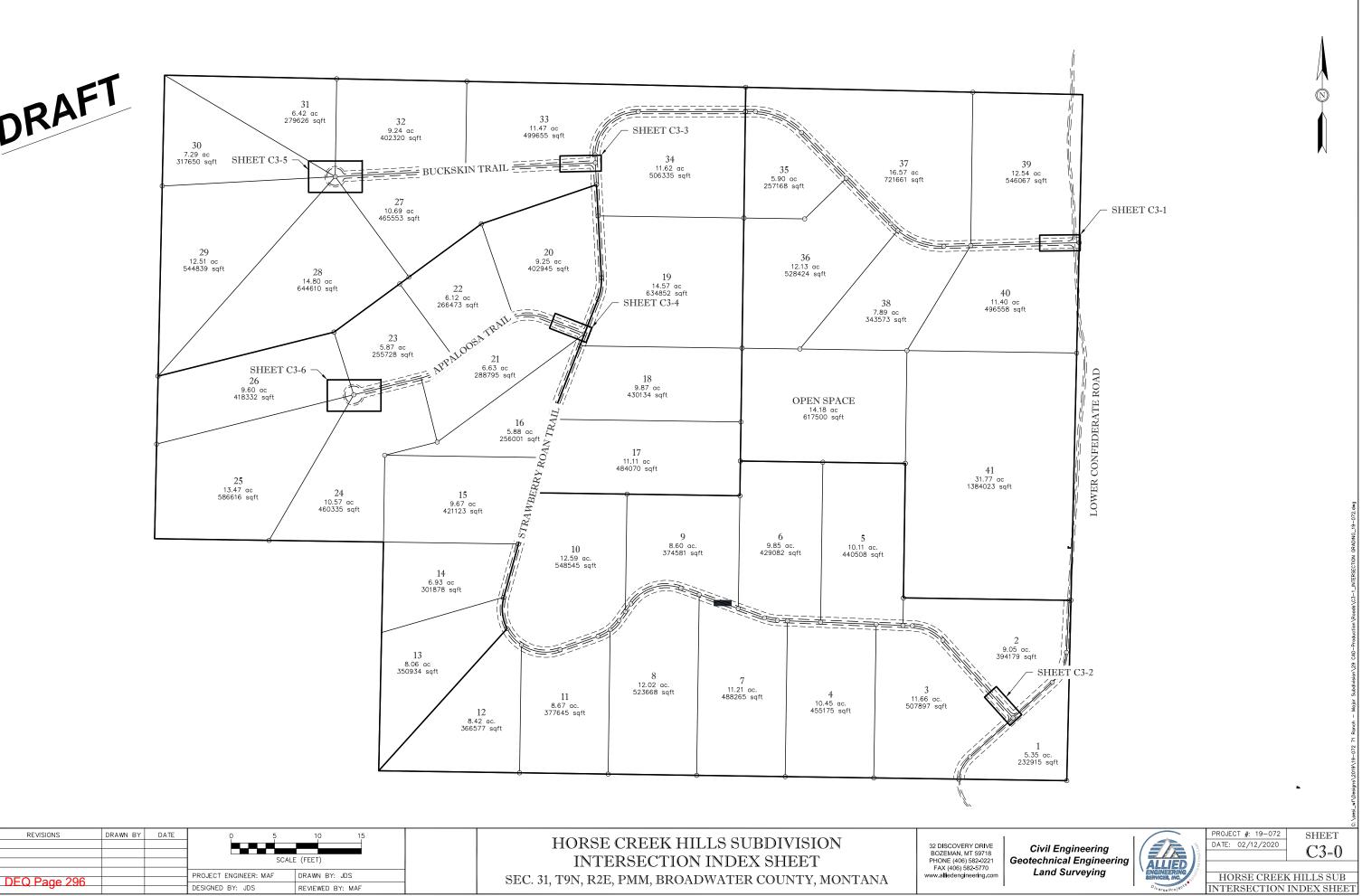


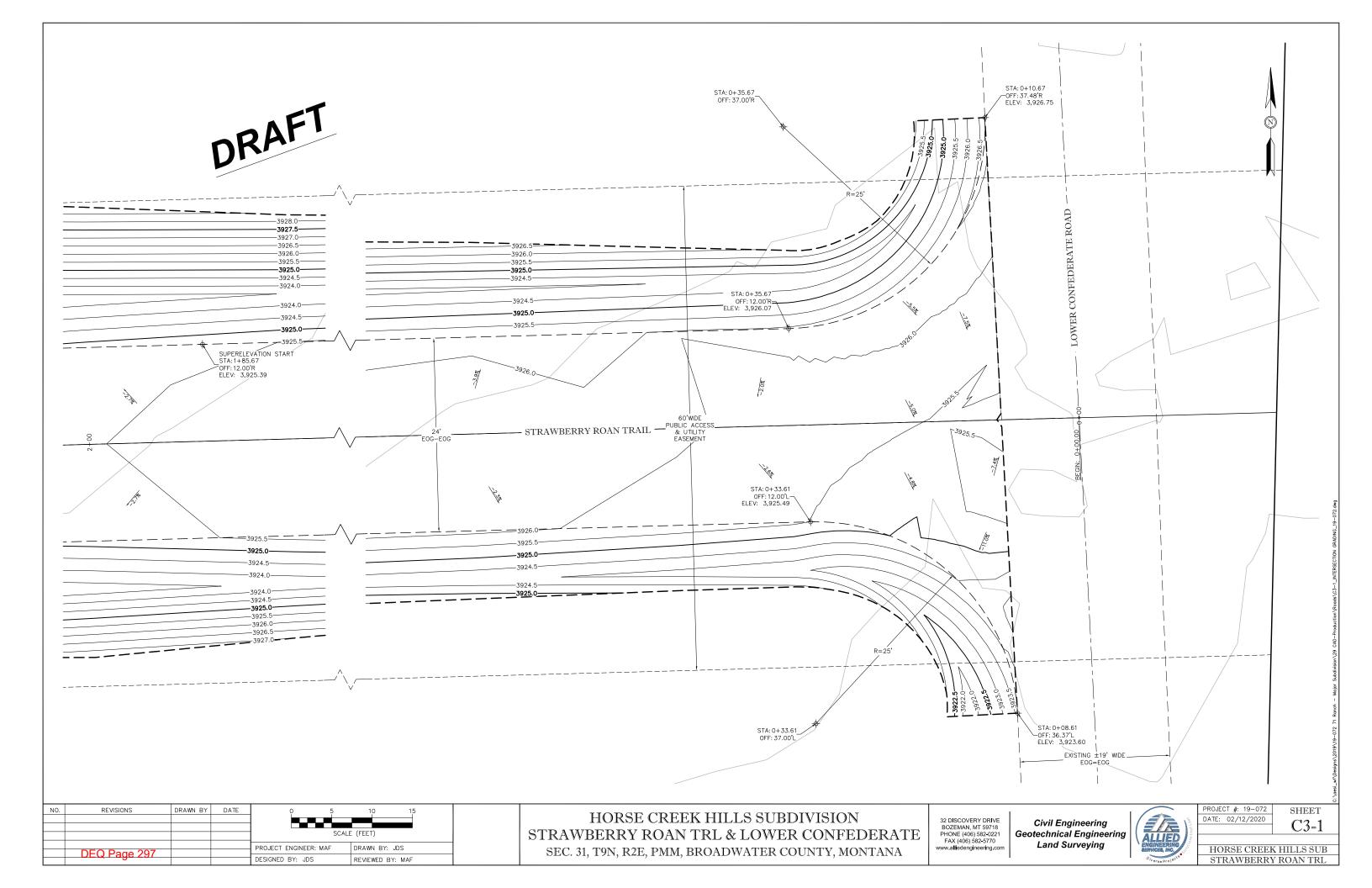
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APPALOOSA T	RAIL X-SECs

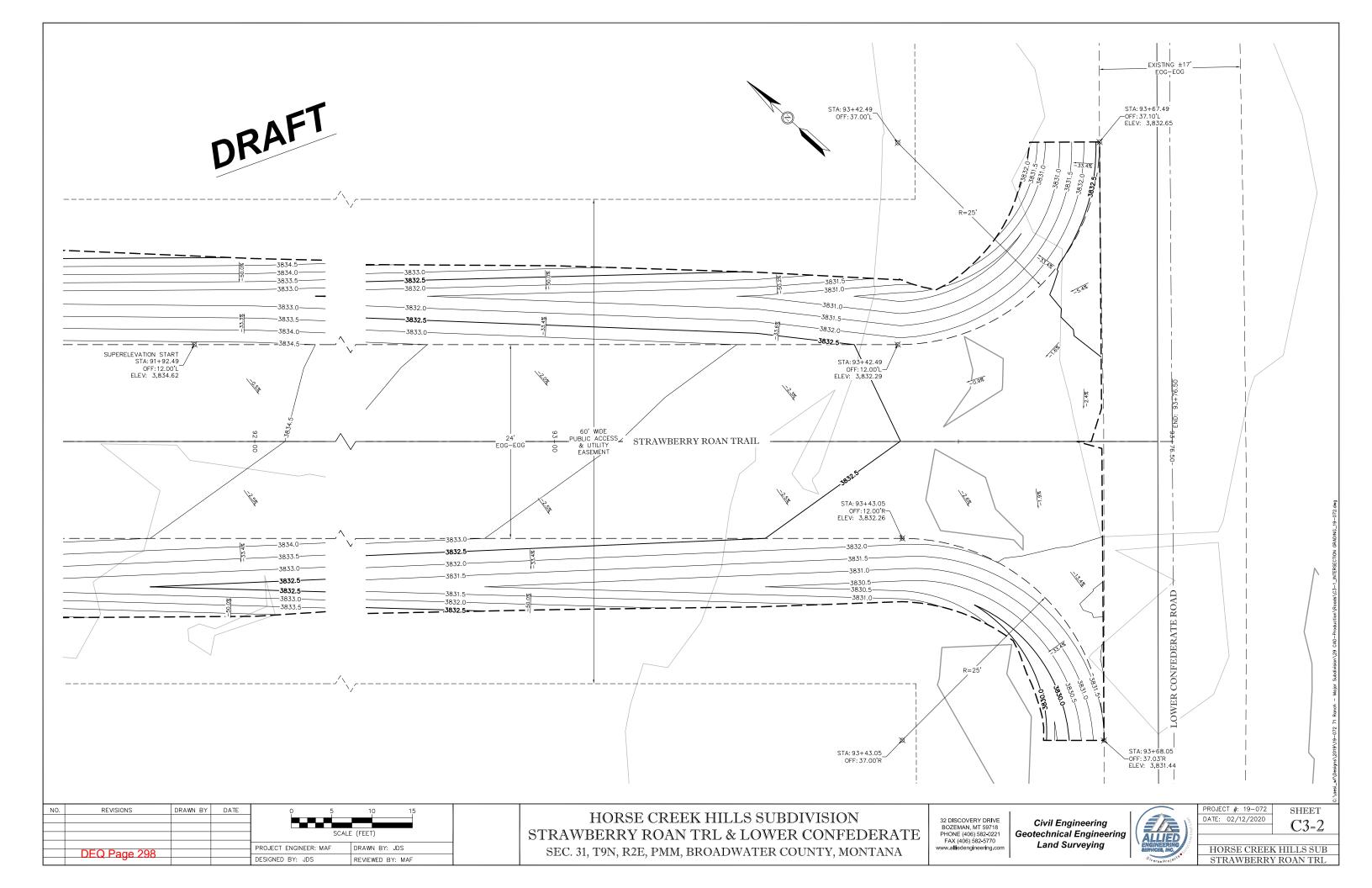


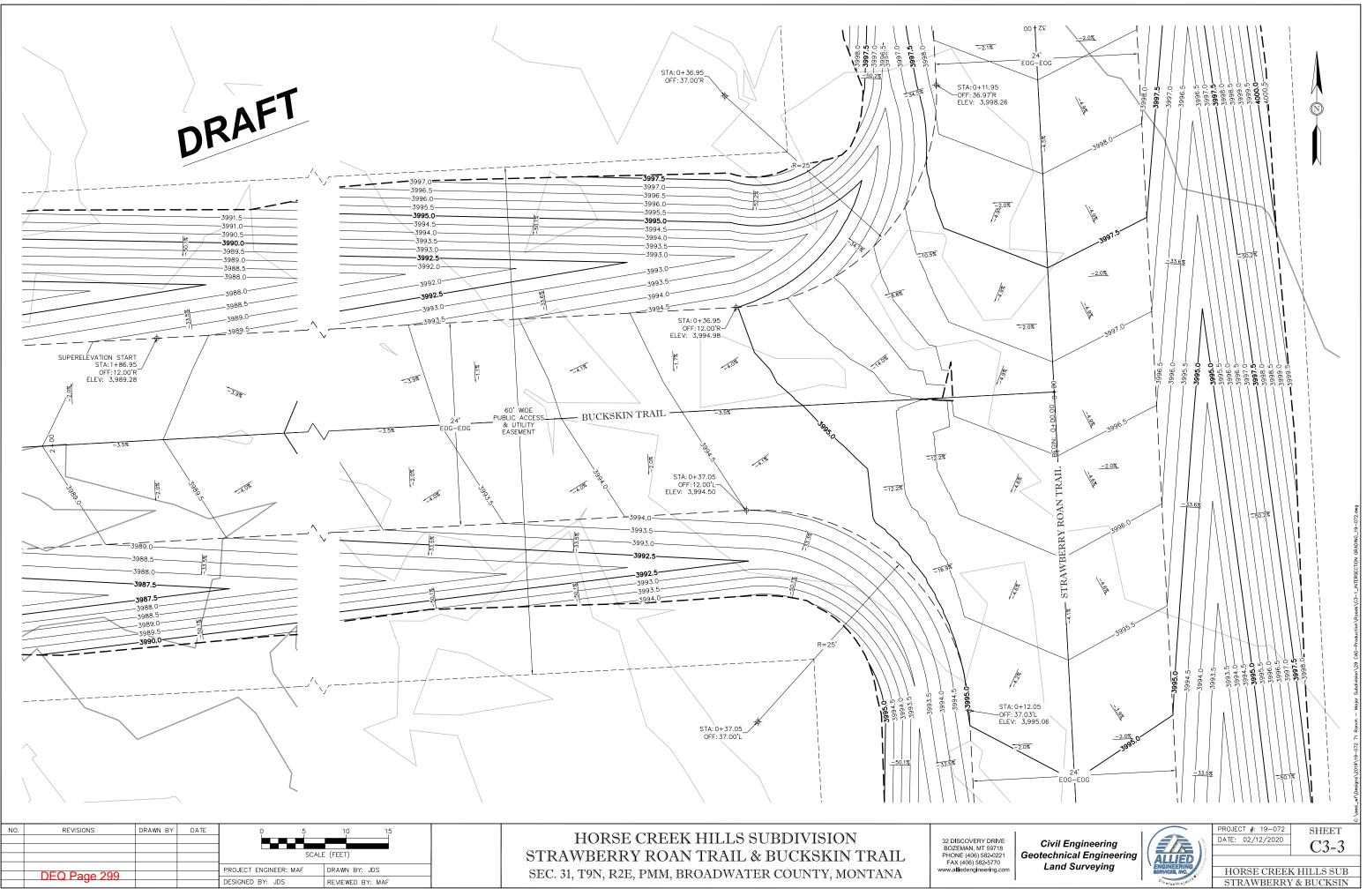
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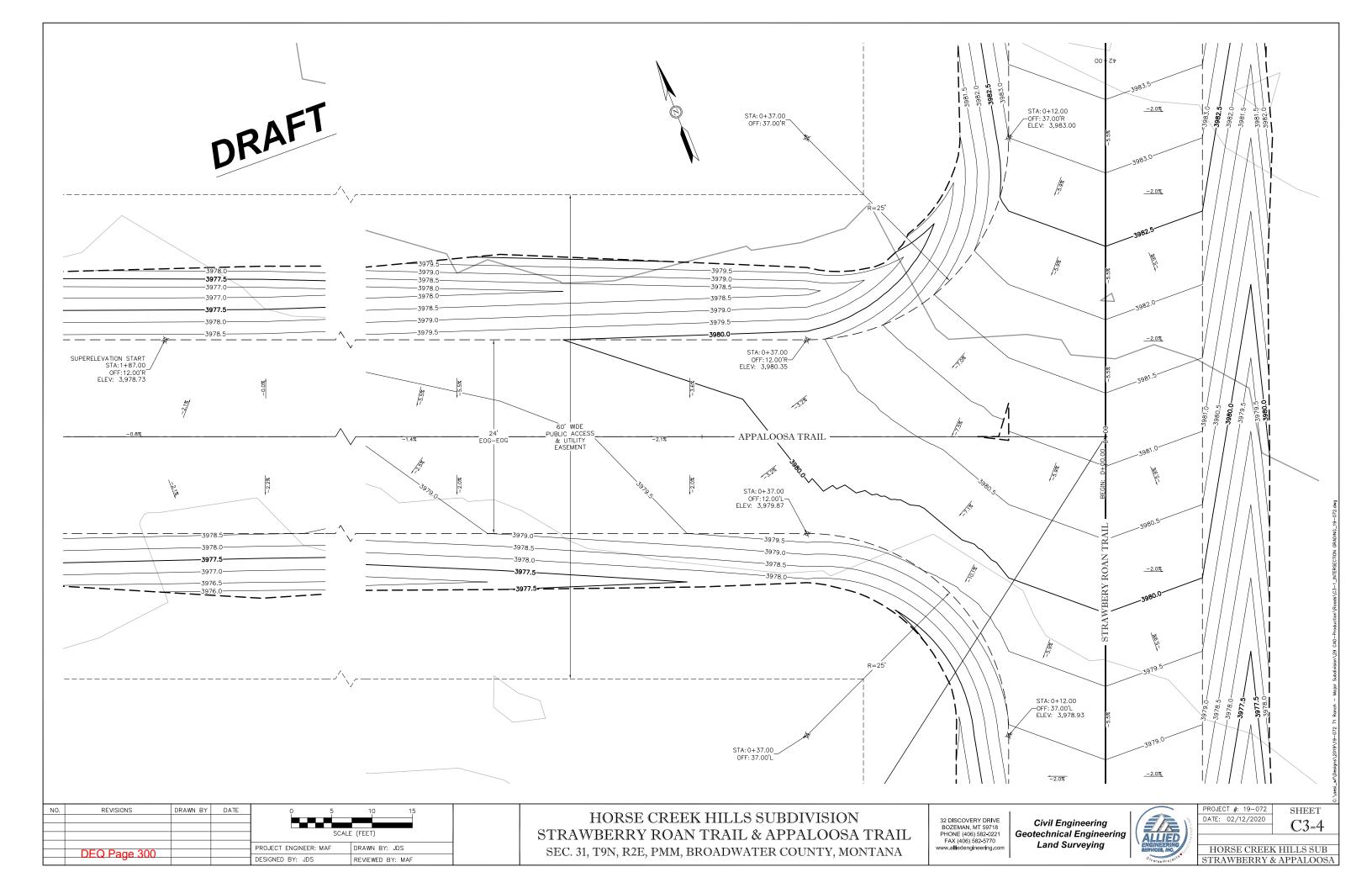


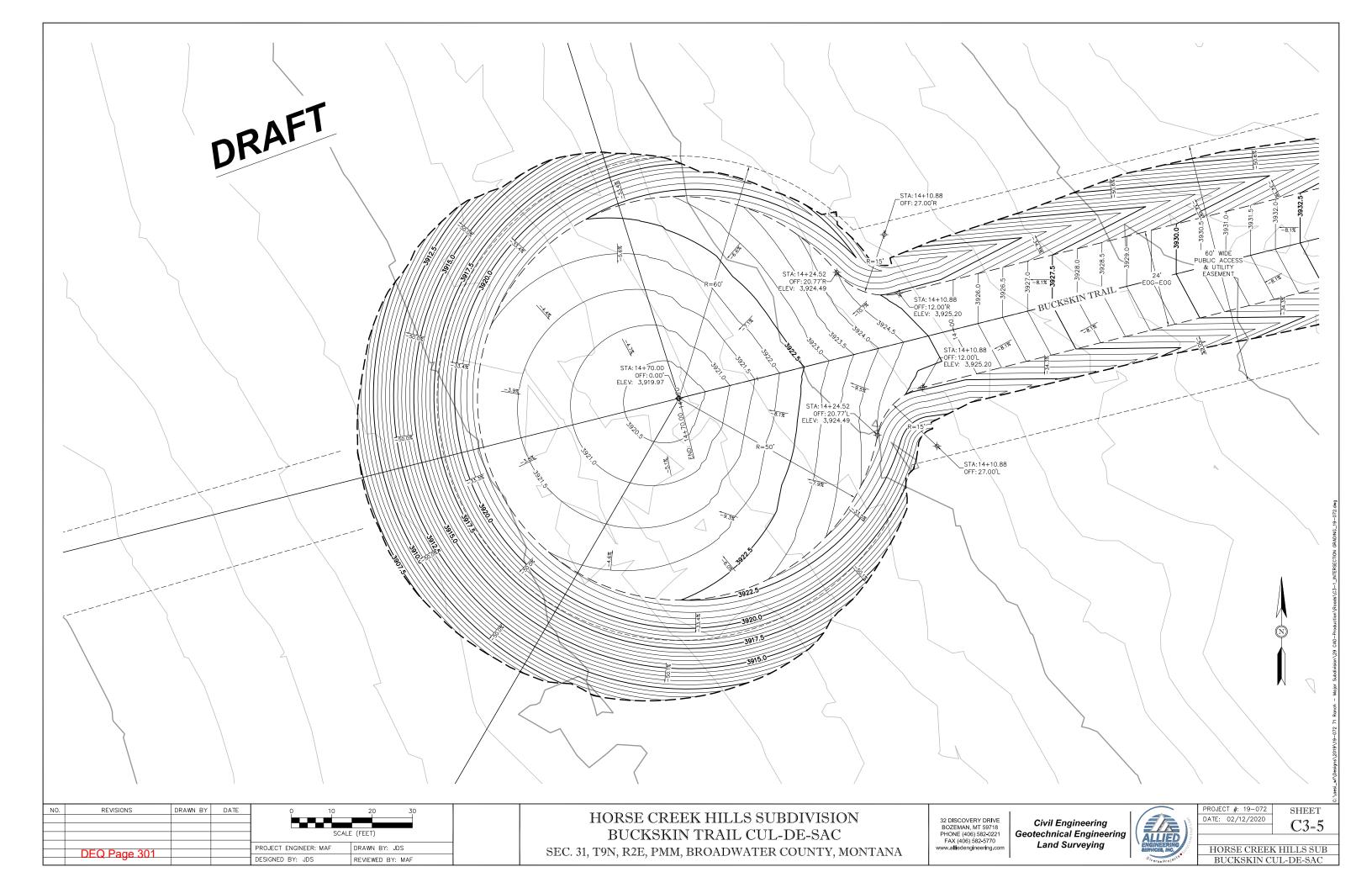


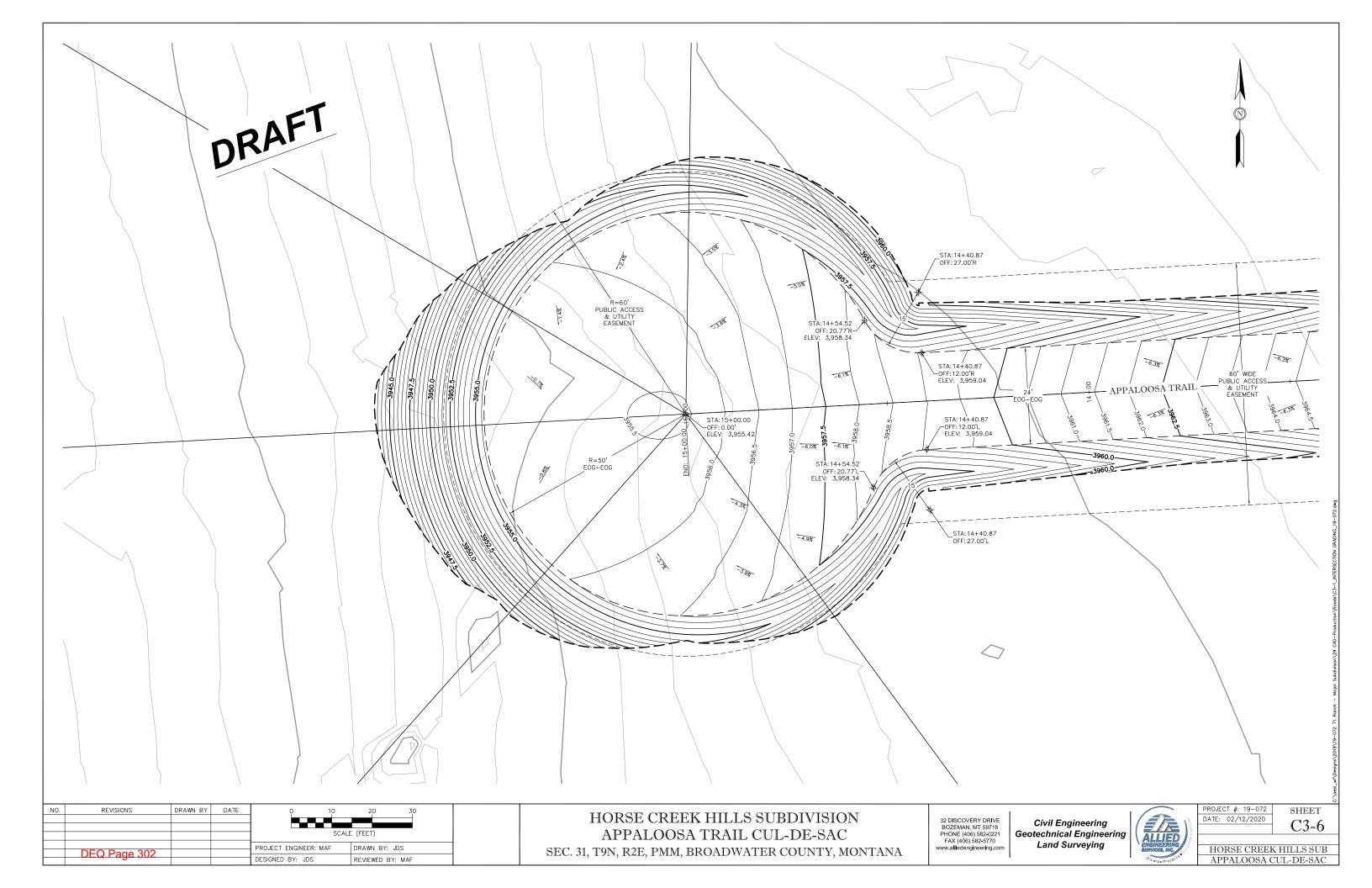




		SCALE (FEET)				
		PROJECT ENGINEER: MAF	DRAWN BY: JDS			
DEQ Page 299						
		DESIGNED BY: JDS	REVIEWED BY MAE			







HORSE CREEK HILLS SUBDIVISION

WASTEWATER AND STORMWATER PLANS

LOCATION: N $\frac{1}{2}$, N $\frac{1}{2}$ of the SE $\frac{1}{4}$, & NE $\frac{1}{4}$ of the SW $\frac{1}{4}$, SEC 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MONTANA

LATITUDE: 46°29'45.6"	LONGITUDE: -111°31'13"
DEVELOPER: 71 RANCH L	P
MARCH, 2020	SET NO.

PROJECT MANAGER: **DESIGN ENGINEER:** PROJECT SURVEYOR: GREG FINCK, PLS

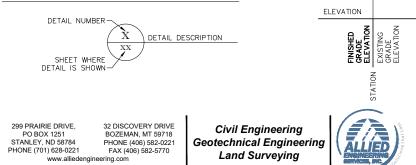
MARK FASTING, PE HUNTER MORRICAL, EI

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WW0.1	EXISTING CONDITIONS AND SURVEY CONTROL			
WW0.2	PROPOSED IMPROVEMENTS			
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PLAN SHEET DETAIL CALLOUTS

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PROPOSED ROADWAY PROFILE LABEL KEY



CIVIL ABBREVIATIONS:

MAXIMUM MANHOLF

MINIMUM

NORTH

RADIUS

SOUTH SCHEDULE STORM DRAIN SECTION

SUBGRADE

SQUARE YARD

UNDERGROUND

WATER MAIN

STREET STATION STANDARD

TYPICAL

VERTICAL

WEST

WITH WITHOUT WATER SERVICE

MID POINT

MECHANICAL JOINT

MONTANA PUBLIC WORKS

POINT OF CURVATURE

POINT OF TANGENCY

POLYVINYL CHLORIDE

RADIUS POINT REINFORCED CONCRETE

SANITARY SEWER MAIN SANITARY SEWER SERVICE

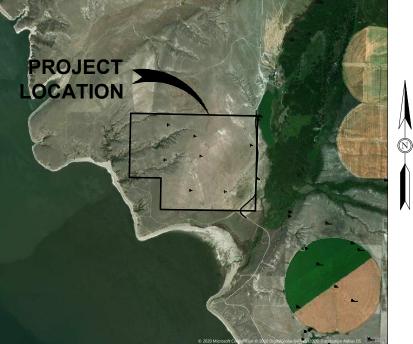
TEMPORARY BENCH MARK TOP BACK OF CURB TOTAL DYNAMIC HEAD

RIGHT-OF-WAY **RIGHT**

STANDARD SPECIFICATIONS

PLAIN END POLYETHYLENE POLYETHYLENE PODYETY LINE PROPERTY LINE POUNDS PER SQUARE INCH

	SERVICES, INC. ACRE AVENUE BUILDING	MAX MH MIN MJ MP MPWSS
BOG	BENCHMARK BACK OF GRATE (GUTTER)	N
CO CONC COB	CENTERLINE CORRUGATED METAL PIPE CLEAN OUT CONCRETE CITY OF BELGRADE CUBIC YARD	PC PE PI PL PSI
	DUCTILE IRON DIAMETER DRAWING	PT PVC
ĒA	EAST EACH EXISTING GRADE	R RP RCP
ELEV EOG EOP	ELEVATION EDGE OF GRAVEL EDGE OF PAVEMENT FXISTING	ROW RT S
FETS FG FHYD FL FL FM	FLARED END TERMINAL SECTION FINISHED GRADE FIRE HYDRANT FLANGE FLOWLINE SEWER FORCE MAIN FEET	SCH SD SECT SG SS SS ST STA STD SY
GV	GALLONS PER MINUTE GATE VALVE	ТВМ ТВС
	HIGH DENSITY POLYETHYLENE HORIZONTAL	TDH TYP
ΗP	HIGH POINT HIGHWAY	UG
N	INVERT ELEVATION INCH INVERT	VERT W W
_P	LINEAR FEET LOW POINT LEFT	w/ W/O WS



AERIAL MAP 2 000 4.000 6,000 SCALE (FEET)

LEGEND

	 PROPERTY LINE
•	FOUND MONUMENT
\triangle	CONTROL POINT
1235	EX. MAJOR CONTOUR (5' IN
	- EX. MINOR CONTOUR (1' IN
	- EX. EDGE OF ROAD
	EX. DRAINAGE CULVERT
— x — x —	- EX. FENCE
	EX. TREE ROW
***	EX. PINE TREE
W	- EX. WATER MAIN
GV	EX. GATE VALVE
ЭС,	EX. FIRE HYDRANT
s	EX. WELL
S	- EX. SEWER MAIN
S	EX. SEWER MANHOLE
OHP	EX. OVERHEAD POWER LINE
	EX. OVERHEAD POWER POL
	EX. ELECTRIC METER
F	EX. UNDERGROUND FIBER C
	EX. TELEPHONE/FIBER OPTI
	AESI S



- AVAILABILITY

- INTERFERE WITH THE WORK.
- PRACTICABLE.

- REQUIREMENTS ARE MET.
- BLOCKS, ETC.), THAT ARE NOT SHOWN ON THESE PLANS.

HORSE	CREEK	HILLS	SUBDIVISION
	WWO.O	COVER	SHEET

CONTAMINATION, SEGREGATION, AND PARTICLE BREAKDOWN. 22. CARRY OUT COVERAGES OF COMPACTION EQUIPMENT SO THAT THE COMPACTIVE EFFORT IS DISTRIBUTED UNIFORMLY AND IN A SYSTEMATIC MANNER OVER THE ENTIRE LIFT. 23. ALL CONSTRUCTION ASSUMES A STABLE COMPACTED SUBGRADE IS ACHIEVED PRIOR TO PLACEMENT OF NEW FACILITIES. 24. COORDINATE WITH UTILITY COMPANIES REGARDING ALL UTILITY CROSSINGS AND ANY POTENTIAL UTILITY CONFLICTS.

25. CONTRACTOR SHALL COORDINATE DRY UTILITY CONDUIT LOCATIONS, DEPTHS, MATERIAL, QUANTITY, ETC. WITH APPLICABLE UTILITY SERVICE PROVIDERS PRIOR TO CONSTRUCTION.

26. IF APPLICABLE, CONTRACTOR SHALL BE RESPONSIBLE FOR ENSURING THAT ALL STORM WATER POLLUTION PREVENTION PLAN (SWPPP)

27. PROJECT SITE DEVELOPMENT MAY REQUIRE ADDITIONAL STORM WATER FACILITY IMPROVEMENTS (SWALES, PONDS, ROADSIDE DITCH

-1235-PROPOSED MAJOR CONTOUR (5' INTERVAL) NTERVAL) -1234 PROPOSED MINOR CONTOUR (1' INTERVAL) TERVAL) PROPOSED ROAD CENTERLINE PROPOSED CURB AND GUTTER PROPOSED SIDEWALK PROPOSED WATER MAIN PROPOSED WATER SERVICE Ň PROPOSED GATE VALVE Ç, PROPOSED FIRE HYDRANT PROPOSED SEWER MAIN PROPOSED SEWER FORCE MAIN FM PROPOSED SEWER SERVICE S PROPOSED SEWER MANHOLE PROPOSED STORM DRAIN LINE SD PROPOSED STORM DRAIN CURB INLET PROPOSED DRAINAGE CULVERT PROPOSED DRAINAGE DIRECTION OPTICS LINE PROPOSED DRAINAGE ARROW PROPOSED SIGN POST TICS PEDESTAL .

PROPOSED LOT LINE

PROPOSED RIGHT-OF-WAY LINE

ROAD DESIGN

- NOISIVIGUN -

HORSE CREEK HILLS

STANDARD BORDER FORMAT

GENERAL NOTES AND SPECIFICATIONS:

1. THE CONTRACTOR MUST ADHERE TO THE PROJECT PLANS AND SPECIFICATIONS. THE CONSTRUCTION COMPANY MUST BE A LICENSED CONTRACTOR WITH THE STATE OF MONTANA AND BE COVERED BY LIABILITY INSURANCE. A TWO-YEAR WRITTEN WARRANTY FROM THE PROJECT CONTRACTOR TO GALLATIN COUNTY IS REQUIRED FOR ALL ONSITE AND OFFSITE ROAD IMPROVEMENTS THE CONTRACTOR WILL BE RESPONSIBLE FOR LOCATING ALL UNDERGROUND UTILITIES BY CALLING THE NATIONAL 811 "CALL BEFORE YOU DIG" TELEPHONE NUMBER PRIOR TO CONSTRUCTION ACTIVITIES.

YOU DIG" TELEPHONE NUMBER PRIOR TO CONSTRUCTION ACTIVITES. ALL ROAD AND STORM DRAINAGE IMPROVEMENTS SHALL BE CONSTRUCTED PER THE ALIGNMENT AND GRADE AS SHOWN ON THE PLANS. CONTRACTOR SHALL FIELD VERIFY LOCATION AND DEPTH OF ALL EXISTING UTILITIES AND STRUCTURES WHERE NEW FACILITIES CROSS OR CONNECT. CONTRACTOR SHALL BE RESPONSIBLE FOR EXPOSING POTENTIAL UTILITY CONFLICTS FAR ENOUGH AHEAD OF CONSTRUCTION TO MAKE NECESSARY GRADE MODIFICATIONS WITHOUT DELAYING THE WORK. ALL UTILITY CROSSINGS SHALL BE POTHOLED OR VACUUMED AS NECESSARY PRIOR TO EXCAVATING OR BORING TO ALLOW THE CONTRACTOR TO PREVENT GRADE OR ALIGNMENT

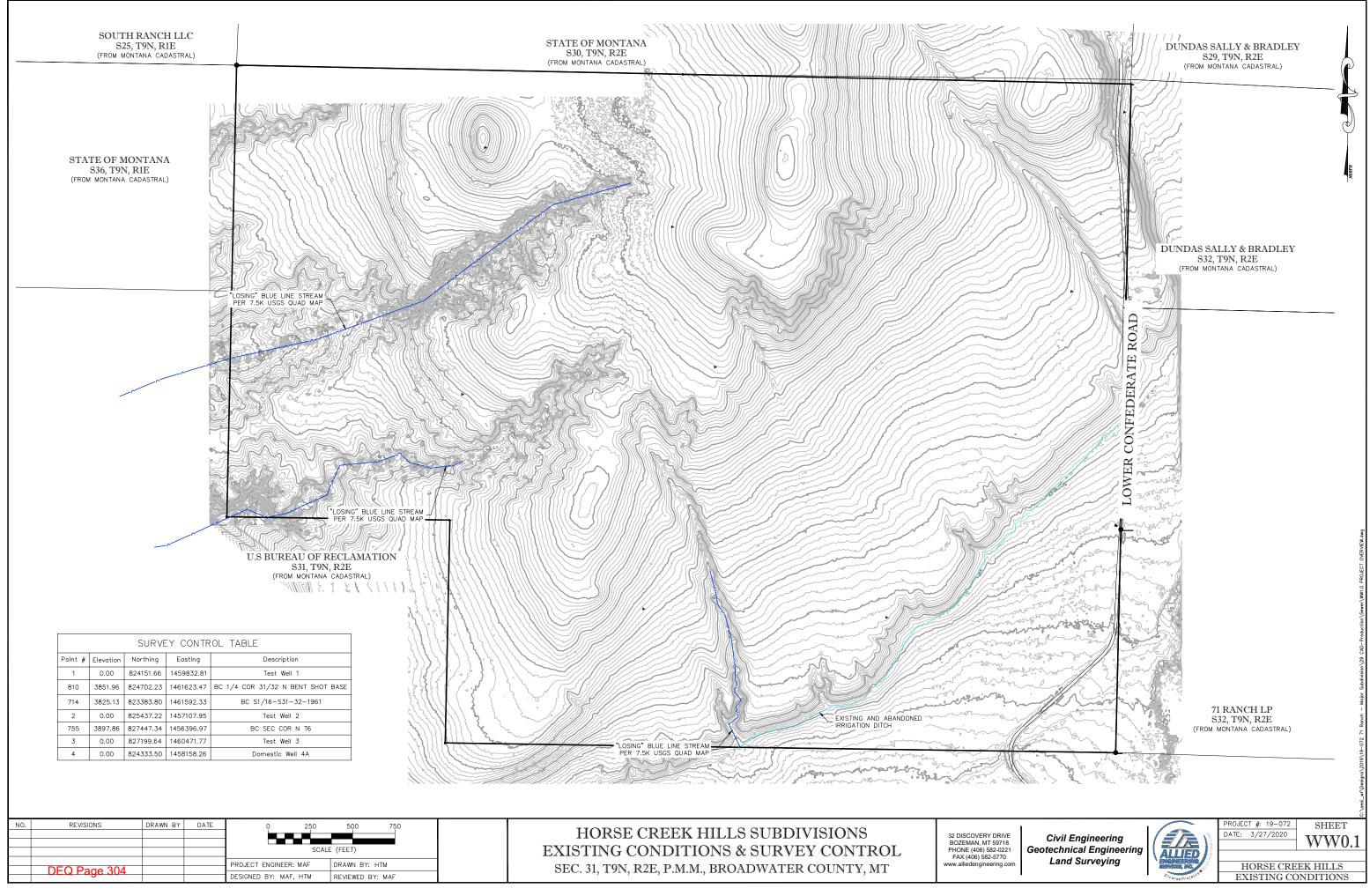
CONFLICTS.
AT LEAST 10 BUSINESS DAYS BEFORE BEGINNING ANY EXCAVATION, THE CONTRACTOR SHALL NOTIFY THE OWNER AND ENGINEER OF UNDERGROUND FACILITIES AND COORDINATE THE WORK WITH THE OWNERS OF SUCH UNDERGROUND FACILITIES. THE INFORMATION SHOWN OR INDICATED IN THE CONTRACT DOCUMENTS WITH RESPECT TO EXISTING UNDERGROUND FACILITIES. THE INFORMATION AND DATA OBTAINED FROM THE OWNERS OF THE FACILITIES WITHOUT FIELD EXPLORATION, AND AS SUCH, OWNER AND ENGINEER ARE NOT RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF SUCH INFORMATION OR DATA.
NO TRENCHES IN ROADS OR DRIVEWAYS SHALL BE LEFT IN AN OPEN CONDITION OVERNIGHT. ALL SUCH TRENCHES SHALL BE BACKFILLED, COMPACTED AND CLOSED BEFORE THE END OF EACH WORK DAY AND NORMAL TRAFFIC FLOWS RESTORED.
IF THE ENGINEER IS CONTRACTED FOR CONSTRUCTION STAKING, ENGINEER SHALL BE CONTACTED PRIOR TO STAKING. PROVIDE ADVANCED NOTICE SUFFICIENT TO ACCOMMODATE CONSTRUCTION, Z WORKING DAYS IS MINIMUM, AND MAY VARY DEPENDING UPON AVAILABILITY.

AVAILABILITY. LIGHTING, ELECTRICAL, NATURAL GAS, COMMUNICATIONS, LANDSCAPING, ETC. ARE TO BE DESIGNED BY OTHERS. FINAL QUANTITIES MAY BE HIGHER OR LOWER THAN THOSE ESTIMATED, PENDING FIELD FINDINGS, SITE CONDITIONS, ETC.). STRIP THE EMBANKMENT FOUNDATION AREA, BORROW AREAS AND ALL AREAS TO RECEIVE FILL TO A MINIMUM DEPTH OF 6 INCHES AND AS REQUIRED TO REMOVE ALL ORGANIC SOILS, VEGETATIVE MATTER, ROOTS, AND OTHER PERISHABLE, LOOSE OR OBJECTIONABLE MATERIAL INCLUDING FROZEN SOIL THAT MIGHT INTERFERE WITH COMPACTION OF EMBANKMENT LIFT OR THE BONDING OF EMBANKMENT TO FOUNDATION. OBJECTIONABLE MATERIAL WILL BE AS DETERMINED BY THE ENGINEER. PERFORM STRIPPING OPERATIONS IN A MANNER TO CONSERVE ALL TOPSOIL THAT CONTAINS ORGANICS. . TRANSPORT STRIPPED MATERIALS TO STOCKPILE AREAS OUTSIDE OF WATERWAYS AND WETLANDS, SUBJECT TO APPROVAL. COORDINATE WITH OWNER TO IDENTIFY STOCKPILE AREAS. LOCATE PILES SO AS NOT TO AFFECT THE OPERATION OF THE EXISTING OPERATIONS, OR INTERFERE WITH THE WORK

TAKE PRECAUTIONS TO PRESERVE, IN A SOUND CONDITION, THE MATERIAL BELOW AND BEYOND THE LINES OF ALL EXCAVATIONS. PERFORM OPERATIONS SO THAT THE EXCAVATIONS WILL YIELD AS MUCH SUITABLE MATERIAL FOR CONSTRUCTION PURPOSES AS

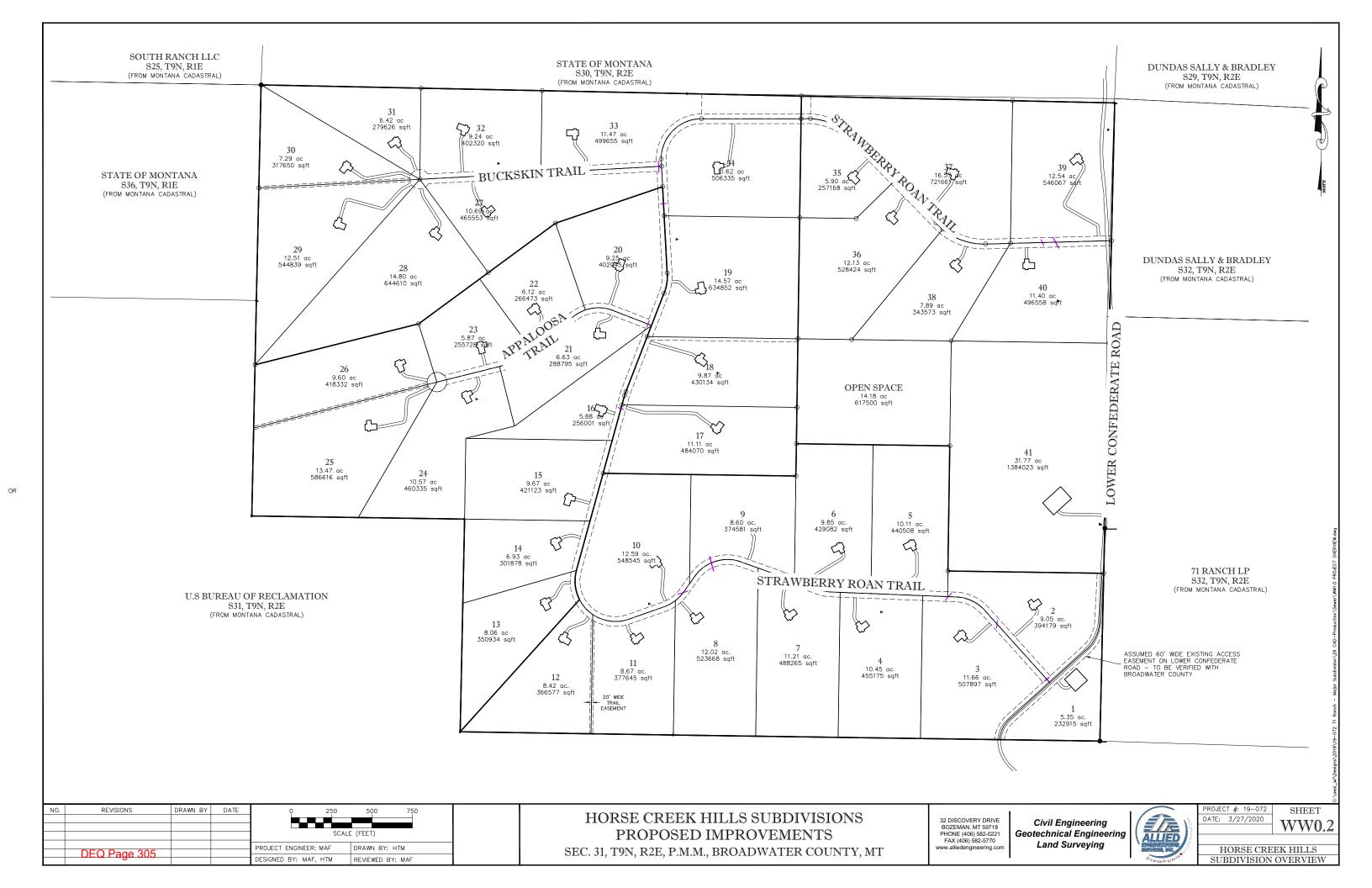
TACTICABLE. 14. REUSE, AS MUCH AS IS PRACTICABLE, ALL SUITABLE MATERIALS FROM REQUIRED EXCAVATION IN THE PERMANENT CONSTRUCTION.

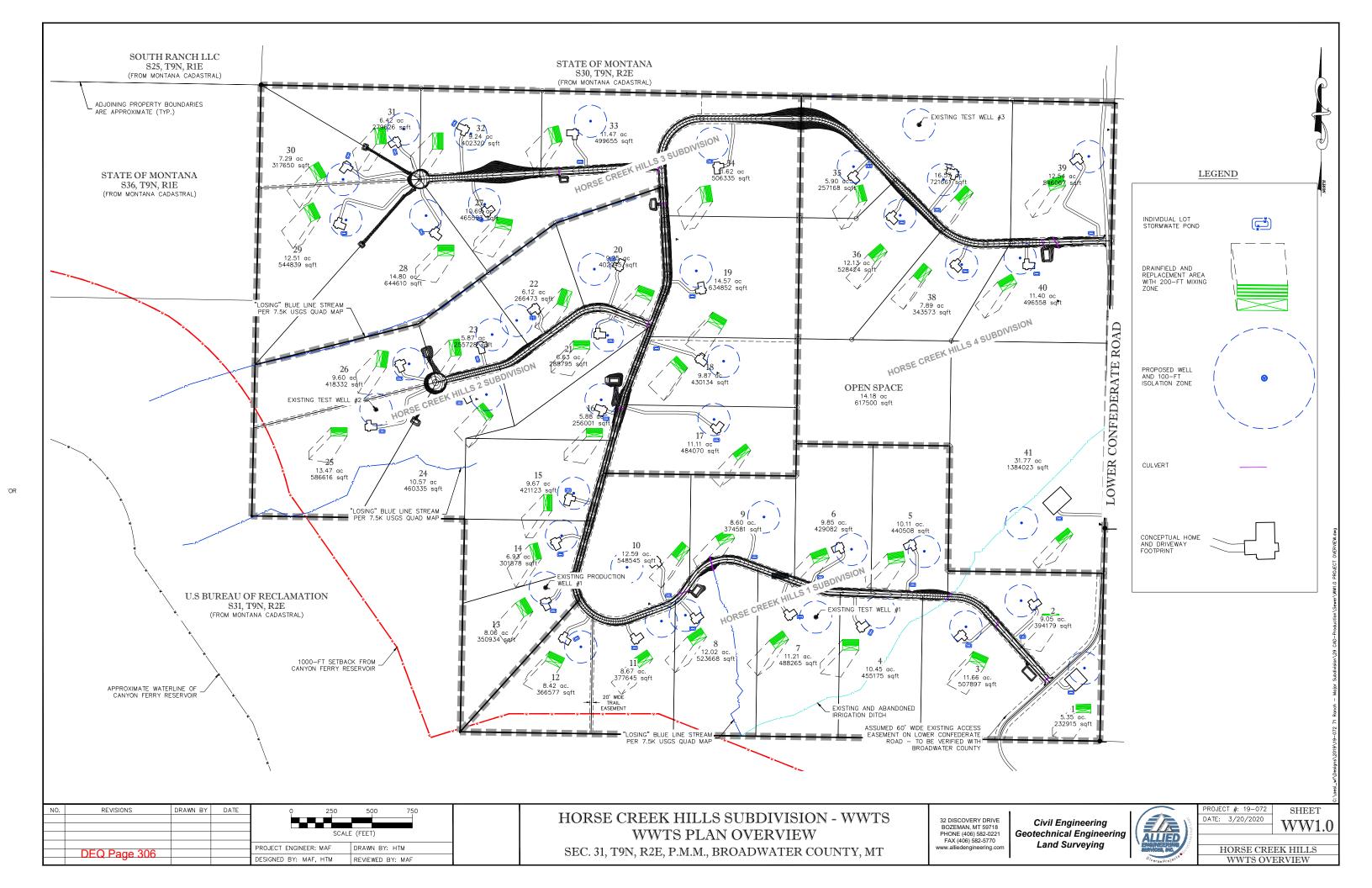
REUSE, AS MUCH AS IS PRACTICABLE, ALL SUITABLE MATERIALS FROM REQUIRED EXCAVATION IN THE PERMANENT CONSTRUCTION. SEPARATE UNSUITABLE MATERIALS AND REMOVE THEM FROM THE WORK AREA AS SOON AS PRACTICABLE.
 SPREAD OUT AND ALLOW MATERIALS TO DRY THAT ARE TOO WET FOR IMMEDIATE COMPACTION UNTIL THE WATER CONTENT IS REDUCED SUFFICIENTLY FOR PLACEMENT IN THE EMBANKMENT. AERATING AND DRYING IS INCIDENTAL TO THE WORK.
 WATER-CONDITION MATERIALS THAT ARE TOO DRY FOR IMMEDIATE COMPACTION. MOISTURE CONDITIONING IS INCIDENTAL TO THE WORK.
 WATER-CONDITION MATERIALS THAT ARE TOO DRY FOR IMMEDIATE COMPACTION. MOISTURE CONDITIONING IS INCIDENTAL TO THE WORK.
 WATER-CONDITION MATERIALS THAT ARE TOO DRY FOR IMMEDIATE COMPACTION. MOISTURE CONDITIONING IS INCIDENTAL TO THE WORK.
 DE-WATER AS NECESSARY TO PREVENT THE ACCUMULATION AGAINST OR THE INTERMINGLING OF WATER WITH THE FILL.
 PERFORM EXCAVATION AND PLACEMENT OPERATIONS SUCH THAT THE EMBANKMENT MATERIALS ARE MIXED AND BLENDED TO PROVIDE THE MOST HOMOGENEOUS SECTION AND BEST DEGREE OF COMPACTION AND STABILITY PRACTICAL. ALL FILL SHOULD BE PLACED IN HORIZONTAL LIFTS AND COMPACTED TO AT LEAST 95% OF ASTM D-698. PROVIDE PRIMARY WATER CONDITIONING, MIXING AND BLENDING IN STOCKPILES AS NEEDED. DISTRIBUTE THE FILL IN A LIFT SUCH THAT IT IS FREE FROM LENSES, POCKETS, STREAKS, OR LAYERS DIFFERING MATERIALLY IN TEXTURE OR GRADATION FROM THE SURROUNDING FILL.
 CONTROL AND CONDUCT ALL TRANSPORTING, STOCKPILING, EXCAVATION, PRODUCTION, AND PLACEMENT OPERATIONS TO MINIMIZE CONTAMINATION, SEGREGATION, AND PARTICLE BREAKDOWM.
 CONTROL AND CONDUCT ALL TRANSPORTING, STOCKPILING, EXCAVATION, PRODUCTION, AND PLACEMENT OPERATIONS TO MINIMIZE CONTAMINATION, SEGREGATION, AND PARTICLE BREAKDOWM.
 CONTROL AND CONDUCT ALL TRANSPORTING STOCKPILING SO THAT THE COMPACTIVE EFFORT IS DISTRIBUTED UNIFORMLY AND IN A

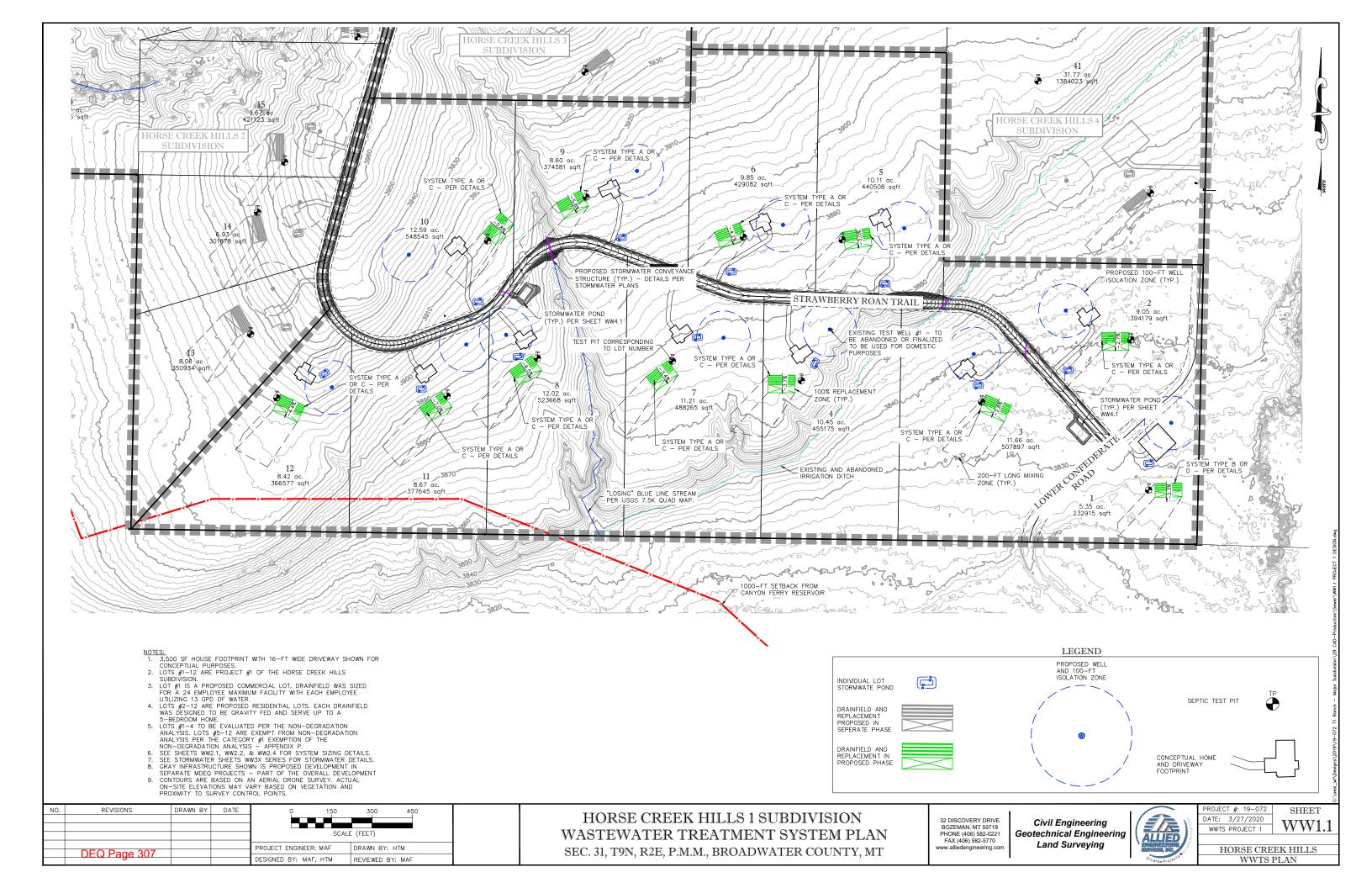


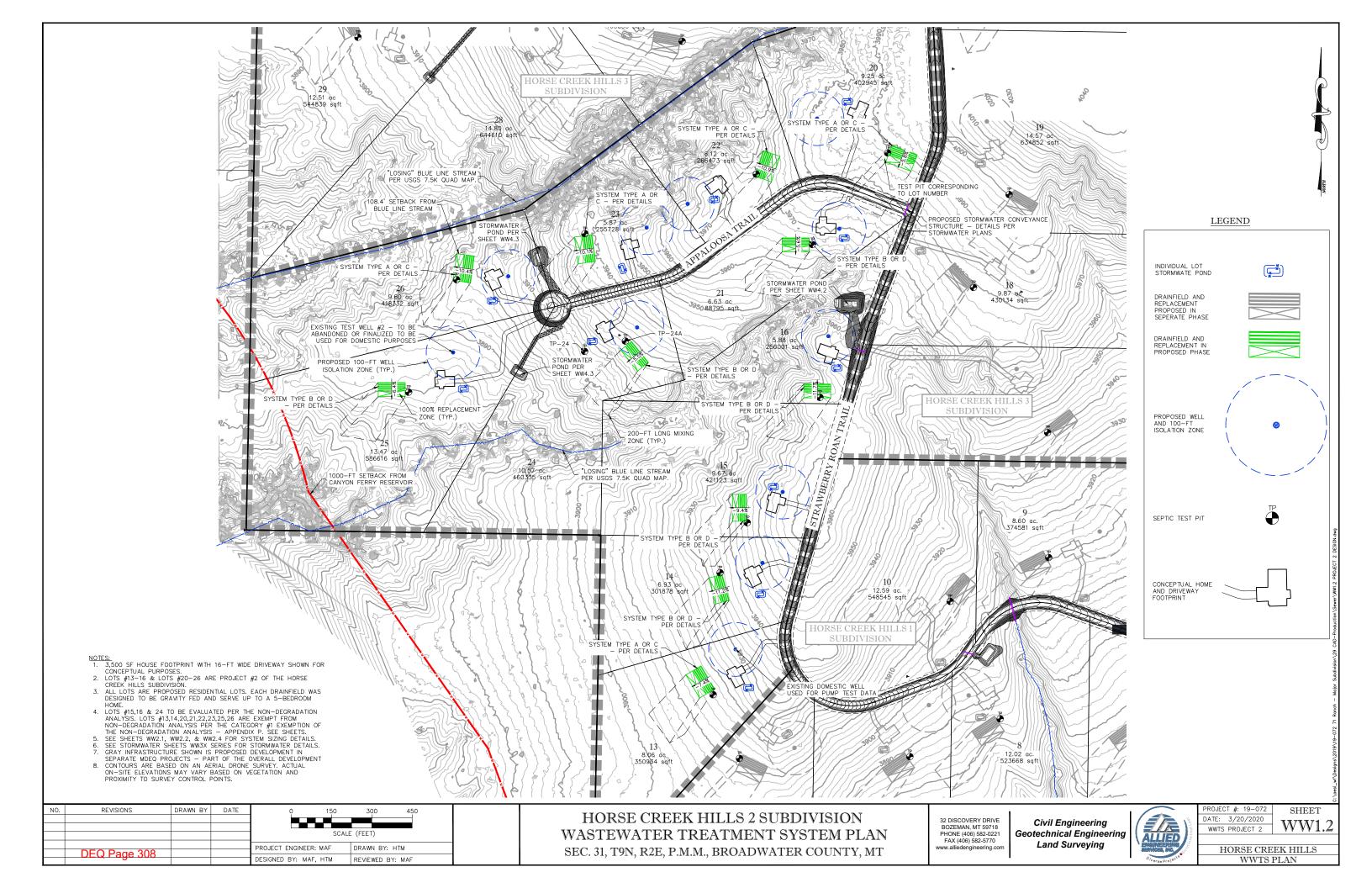
	SCALE	SCALE (FEET)						
	PROJECT ENGINEER: MAF	DRAWN BY: HTM						
	DESIGNED BY MAE HTM	REVIEWED BY MAE						

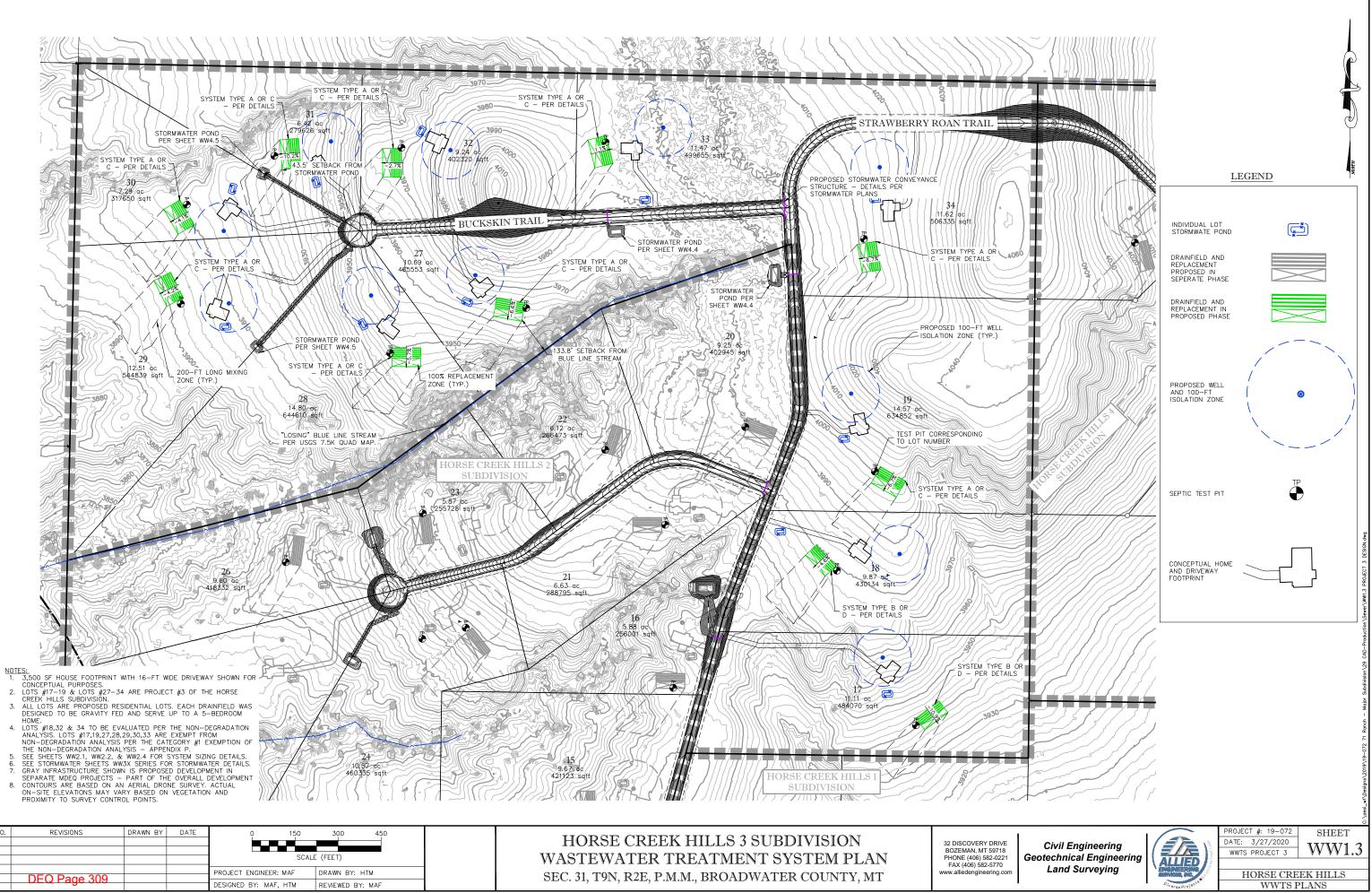
OR









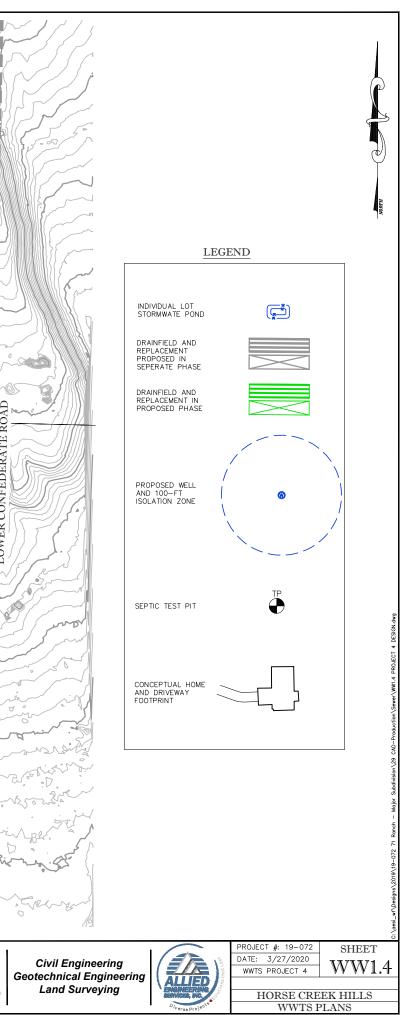


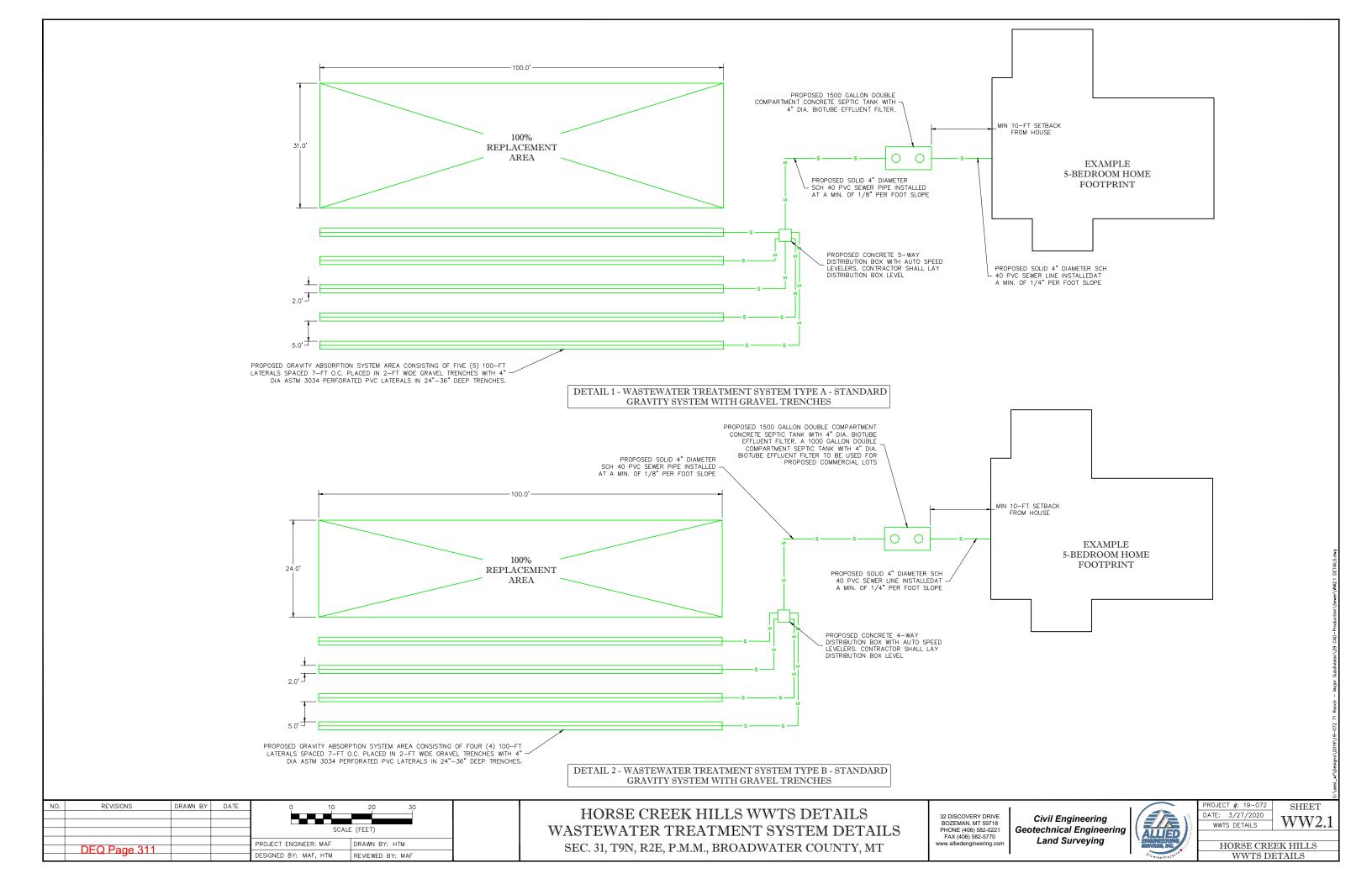
NO.	REVISIONS	DRAWN BY	DATE	Q	150	300	450
				SCALE (FEET)			
				PROJECT ENGINEE	R: MAF	DRAWN BY: H	ТМ
	DEQ Page 309			DESIGNED BY: MA	AF, HTM	REVIEWED BY:	MAF

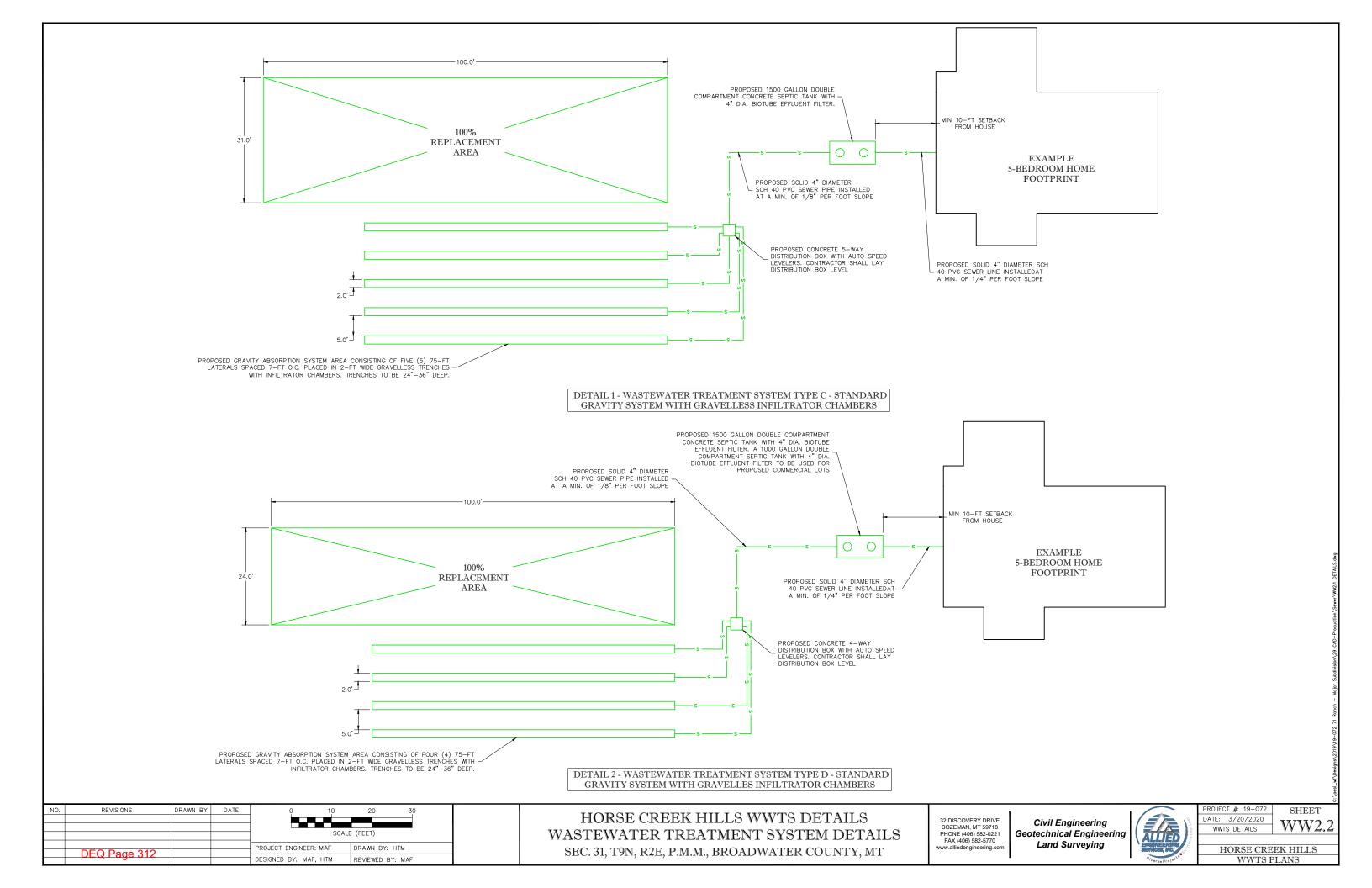
		EXISTING TEST WELL #3 ABANDONED OR FINALIZE USED FOR DOMESTIC PUF	D TO BE	
		SYSTEM TYPE B OR D PER DETAILS SYSTEM TYPE B OR D PER DETAILS SYSTEM TYPE B OR D PER DETAILS SYSTEM TYPE B OR D PER DETAILS	POSED 100-FT WELL ATION ZONE (TYP.) 0 39 12:54:06 3960 546067 sqft ST PIT CORRESPONDING D LOT NUMBER	A OR AILS
	19 14.57 oc 634652 sqft HORSE CREEK HILLS 3 SUBDIVISION	SYSTEM TYPE A OR C - PER DETAILS 36 12:15 oc 528424 isdft 3960 3950 3950 3950 3950 3950 3950 3950	40 11/40 cc 496558 sqft	VATER POND EET WW4.6
	18 9.87 sct 430134 sqtt	3940 3940 00EN SPACE 14.18 oc 617500 sqtt	200-FT LONG MIXING ZONE (TYP.) TP-41A	LOWER CONFEDERATE ROAD
NOTES: 1. 3,500 SF HOUSE FOOTPRINT WITH 16-FT WIDE DRIVEWAY SHOWN FOR CONCEPTUAL PURPOSES. 2. LOTS #35-41 ARE PROJECT #4 OF THE HORSE CREEK HILLS	17 11.11.00 484070 sgH 59.50	HORSE CREEK HILLS 1 SUBDIVISION	EXISTING AND ABANDONED IRRIGATION DITCH	
SUBDIVISION. 3. LOT #41 IS A PROPOSED COMMERCIAL LOT. DRAINFIELD WAS SIZED FOR A 24 EMPLOYEE MAXIMUM FACILITY WITH EACH EMPLOYEE UTILIZING 13 GPD OF WATER. 4. LOTS #35-40 ARE PROPOSED RESIDENTIAL LOTS. EACH DRAINFIELD WAS DESIGNED TO BE GRAVITY FED AND SERVE UP TO A 5-BEDROOM HOME. 5. LOTS #35 & 41 TO BE EVALUATED PER THE NON-DEGRADATION ANALYSIS. LOTS #35, 37, 38, 39, 40 ARE EXEMPT FROM NON-DEGRADATION ANALYSIS PER THE CATEGORY #1 EXEMPTION OF THE NON-DEGRADATION ANALYSIS - APPENDIX P. 6. SEE SHEETS WW2.1, WW2.2, & WW2.4 FOR SYSTEM SIZING DETAILS. 7. SEE STORWWATER SHEETS WW3X SERIES FOR STORWWATER DETAILS. 8. GRAY INFRASTRUCTURE SHOWN IS PROPOSED DEVELOPMENT IN SEPARATE MDEQ PROJECTS - PART OF THE OVERALL DEVELOPMENT 9. CONTOURS ARE BASED ON AN AERIAL DRONE SURVEY. ACTUAL 0N-SITE ELEVATIONS MAY VARY BASED ON VEGETATION AND PROXIMITY TO SURVEY CONTROL POINTS.	8.60 ac. 374581 sqft	6 9.85 ac. 429082 sqft 5590	SYSTEM TYPE B OR D - PER DETAILS	P-410
DEO Page 310	0 150 300 450 SCALE (FEET) NGINEER: MAF DRAWN BY: HTM	HORSE CREEK HILLS 4 SUE WASTEWATER TREATMENT S SEC. 31, T9N, R2E, P.M.M., BROADWAT	BYSTEM PLAN	DISCOVERY DRIVE JZEMAN, MT 59718 ONE (406) 582-0221 AX (406) 582-5770 .alliedengineering.com

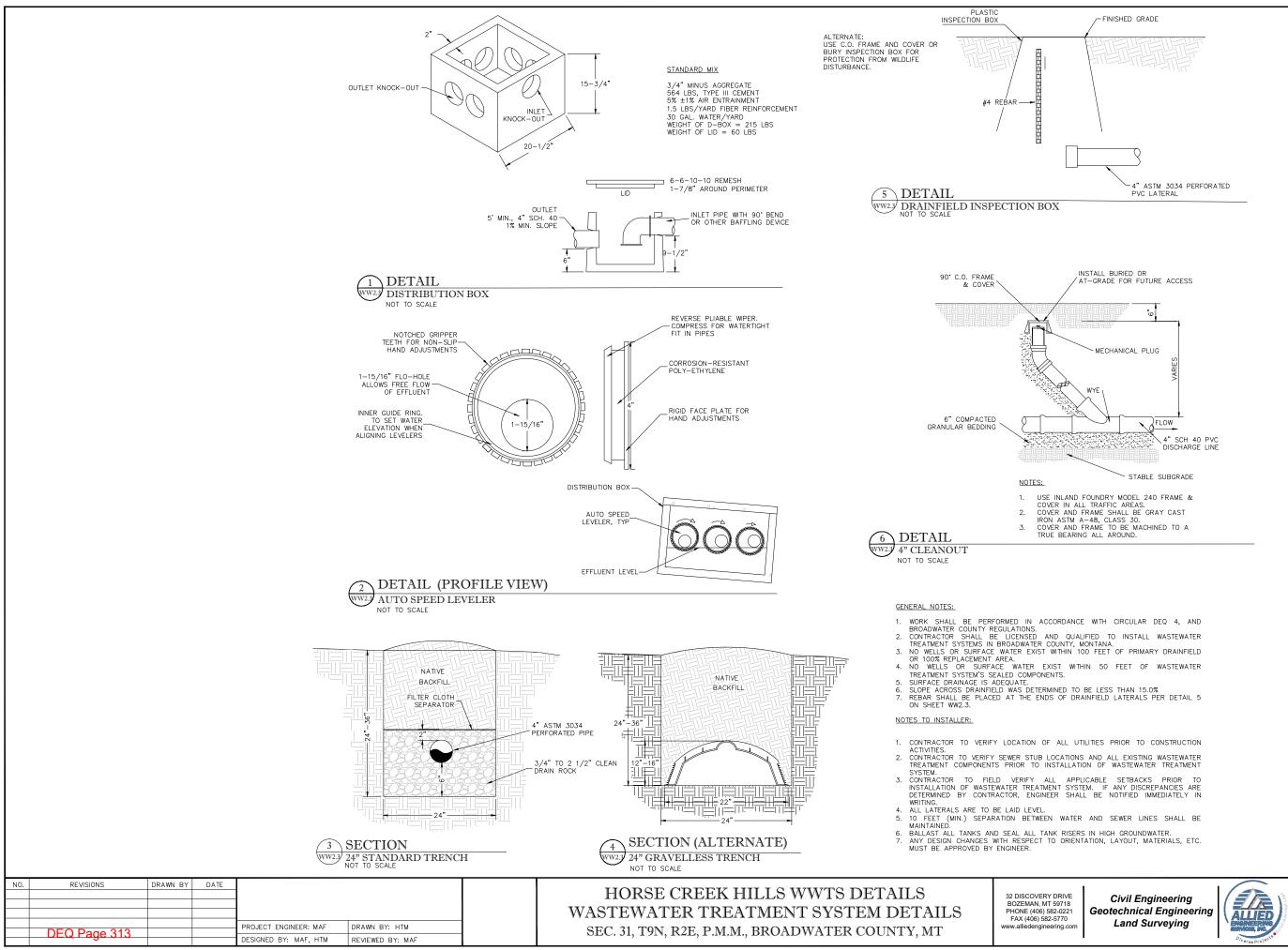
DESIGNED BY: MAF, HTM

REVIEWED BY: MAF

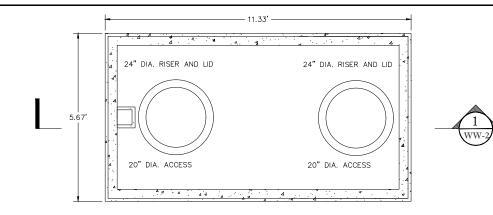








	ö					
ROJECT #: 19-072	SHEET					
ATE: 3/20/2020	11/11/11/20 2					
WWTS DETAILS	WW2.3					
HORSE CREEK HILLS						
WWTS PLANS						



24 HOURS

OR

TANK MUST BE REJECTED.

*INSTALL SAFETY GRATES AT ALL SEPTIC TANK/DOSING TANK OPENINGS. CUT TO FIT AROUND EFFLUENT FILTER HANDLE AND PUMP DISCHARGE PIPING (IF NECESSARY).

<u>ALTERNATE</u> *OWNER MAY INSTALL FIBERGLASS RISERS AND LIDS IN LIEU OF CONCRETE. RISERS AND LIDS (TYPICAL ALL TANKS)

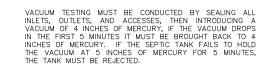
*PRIOR TO PLACEMENT OF TANKS CONTACT ENGINEER IF TANK DEPTHS ARE ANTICIPATED TO EXCEED 4' BURY DEPTH.

MDEQ4 5.1.2.1.:

NOT TO SCALE

DEQ Page 314

LIQUID CONNECTION BETWEEN COMPARTMENTS SHALL CONSIST OF A SINGLE OPENING COMPLETELY ACROSS THE COMPARTMENT WALL OR TWO OR MORE OPENINGS EQUALLY SPACED ACROSS THE WALL THE TOTAL AREA OF THE OPENINGS SHALL BE AT LEAST THREE TIMES THE AREA OF THE INLET PIPE.



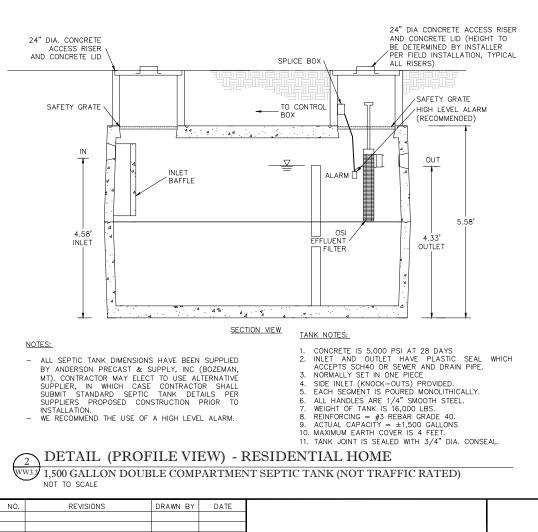
ALL SEPTIC AND DOSING TANKS MUST BE TESTED IN ACCORDANCE WITH MDEQ4 CHAPTER 5 FOR WATERTIGHTNESS.

WATER TESTING MUST BE CONDUCTED BY SEALING THE OUTLETS, FILLING THE SEPTIC TANK TO ITS OPERATIONAL LEVEL, AND ALLOWING THE TANK TO STAND FOR AT LEAST 24 HOURS. IF THERE IS A MEASURABLE LOSS (2 INCHES DEPENDENT OF THE TANK TO STAND FOR ALL AND THE

OR MORE), REFILL THE TANK AND LET STAND FOR ANOTHER

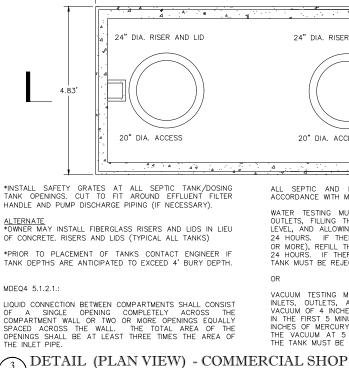
IF THERE IS AGAIN A MEASURABLE LOSS, THE





PROJECT ENGINEER: MAF

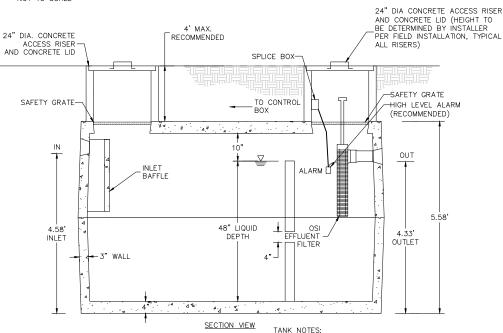
DESIGNED BY: MAF, HTM



9.25

WW24 1,000 GALLON DOUBLE COMPARTMENT SEPTIC TANK (NOT TRAFFIC RATED)





NOTES:	-
	1
 ALL SEPTIC TANK DIMENSIONS HAVE BEEN SUPPLIED 	2
BY ANDERSON PRECAST & SUPPLY, INC (BOZEMAN,	7
MT). CONTRACTOR MAY ELECT TO USE	
ALTERNATIVE SUPPLIER, IN WHICH CASE	4
CONTRACTOR SHALL SUBMIT STANDARD SEPTIC	
TANK DETAILS PER SUPPLIERS PROPOSED	6
CONSTRUCTION PRIOR TO INSTALLATION.	/ E
- WE RECOMMEND THE USE OF A HIGH LEVEL ALARM.	9
 SHALL BE DOUBLE COMPARTMENT 	3 1

(PROFILE VIEW) - COMMERCIAL SHOP

WW24 1,000 GALLON DOUBLE COMPARTMENT SEPTIC TANK (NOT TRAFFIC RATED)

NOT TO SCALE

HORSE CREEK HILLS WWTS DETAILS WASTEWATER TREATMENT SYSTEM DETAILS SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.co



DRAWN BY: HTM

REVIEWED BY: MAF





ALL SEPTIC AND DOSING TANKS MUST BE TESTED IN ACCORDANCE WITH MDEQ4 CHAPTER 5 FOR WATERTIGHTNESS

WATER TESTING MUST BE CONDUCTED BY SEALING THE OUTLETS, FILLING THE SEPTIC TANK TO ITS OPERATIONAL LEVEL, AND ALLOWING THE TANK TO STAND FOR AT LEAST 24 HOURS. IF THERE IS A MEASURABLE LOSS (2 INCHES OR MORE), REFILL THE TANK AND LET STAND FOR ANOTHER 24 HOURS. IF THERE IS AGAIN A MEASURABLE LOSS, THE TANK MUST BE REJECTED.

VACUUM TESTING MUST BE CONDUCTED BY SEALING ALL INLETS, OUTLETS, AND ACCESSES, THEN INTRODUCING A VACUUM OF 4 INCHES OF MERCURY, IF THE VACUUM DROPS IN THE FIRST 5 MINUTES IT MUST BE BROUGHT BACK TO 4 INCHES OF MERCURY. IF THE SEPTIC TANK FAILS TO HOLD THE VACUUM AT 5 INCHES OF MERCURY FOR 5 MINUTES, THE TANK MUST BE REJECTED

CONCRETE IS 5,000 PSI AT 28 DAYS INLET AND OUTLET HAVE PLASTIC SEAL ACCEPTS SCH40 OR SEWER AND DRAIN PIPE. SEAL WHICH NORMALLY SET IN ONE PIECE SIDE INLET (KNOCK-OUTS) PROVIDED. EACH SEGMENT IS POURED MONOLITHICALLY. LACH SEGMENT IS POURED MONOLITICAL
 ALL HANDLES ARE 1/4" SMOOTH STEEL.
 WEIGHT OF TANK IS 10,500 LBS.
 REINFORCING = #3 REBAR GRADE 40.
 ACTUAL CAPACITY = ±1,000 GALLONS
 MAXIMUM EARTH COVER IS 4 FEET. 11. TANK JOINT IS SEALED WITH 3/4" DIA. CONSEAL.



	U				
PROJECT #: 19-072	SHEET				
DATE: 3/20/2020	3373373 4				
WWTS DETAILS	WW2.4				
HORSE CREEK HILLS					
WWTS PLANS					

SUMMARY OF PROPOSED WASTEWATER TREATMENT TYPE CORRESPONDING TO EACH LOT

Lot Numer	# of Bedrooms	GPD of	Texture	Application Rate	Corresponding Percolation Rate	Min. Drainfield	Length of	Min. Drainfield	Infiltrator Size	Min. Drainfield	-	Min. Drainfield	ISVSTem to hel
Lot Numer	# Of Deditioning	Wastewater	Texture	(gpd/ft^2)	(min/inch)	Area (sf)	Lateral (LF)	Dimensions (ft)	Reduction	Area (sf)	Lateral (LF)	Dimensions (ft)	Utilized
1	24 Employees	312	SiL	0.4	16 - <31	780	390	23 X 100 (Type B)	0.75	585	292.5	23 x 75 (Type D)	BorD
2	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
3	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
4	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
5	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
6	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
7	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
8	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
9	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
10	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
11	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
12	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
13	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
14	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)	0.75	600	300	23 x 75 (Type D)	
15	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)		600	300	23 x 75 (Type D)	
16	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)	0.75	600	300	23 x 75 (Type D)	
17	5	400	L	0.5	10 - <16	800	400	23 X 100 (Type B)	0.75	600	300	23 x 75 (Type D)	
18	5	400	L	0.5	10 - <16	800	400	23 X 100 (Type B)		600	300	23 x 75 (Type D)	
19	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
20	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
21	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)	0.75	600	300	23 x 75 (Type D)	1
22	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
23	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
24	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
25	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)	0.75	600	300	23 x 75 (Type D)	
26	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
27	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
28	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
29	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
30	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
31	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
32	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
33	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	1
34	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	1	750	375	30 x 75 (Type C)	
35	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)		600	300	23 x 75 (Type D)	1
36	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	1	750	375	30 x 75 (Type C)	1
37	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
38	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
39	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
40	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
41	24 Employees	312	SiL	0.4	16 - <31	780	390	23 X 100 (Type B)		585	292.5	23 x 75 (Type D)	

1 DETAIL WW2.5 SUMMARY OF DRAINFIELD DIMENSIONS NOT TO SCALE

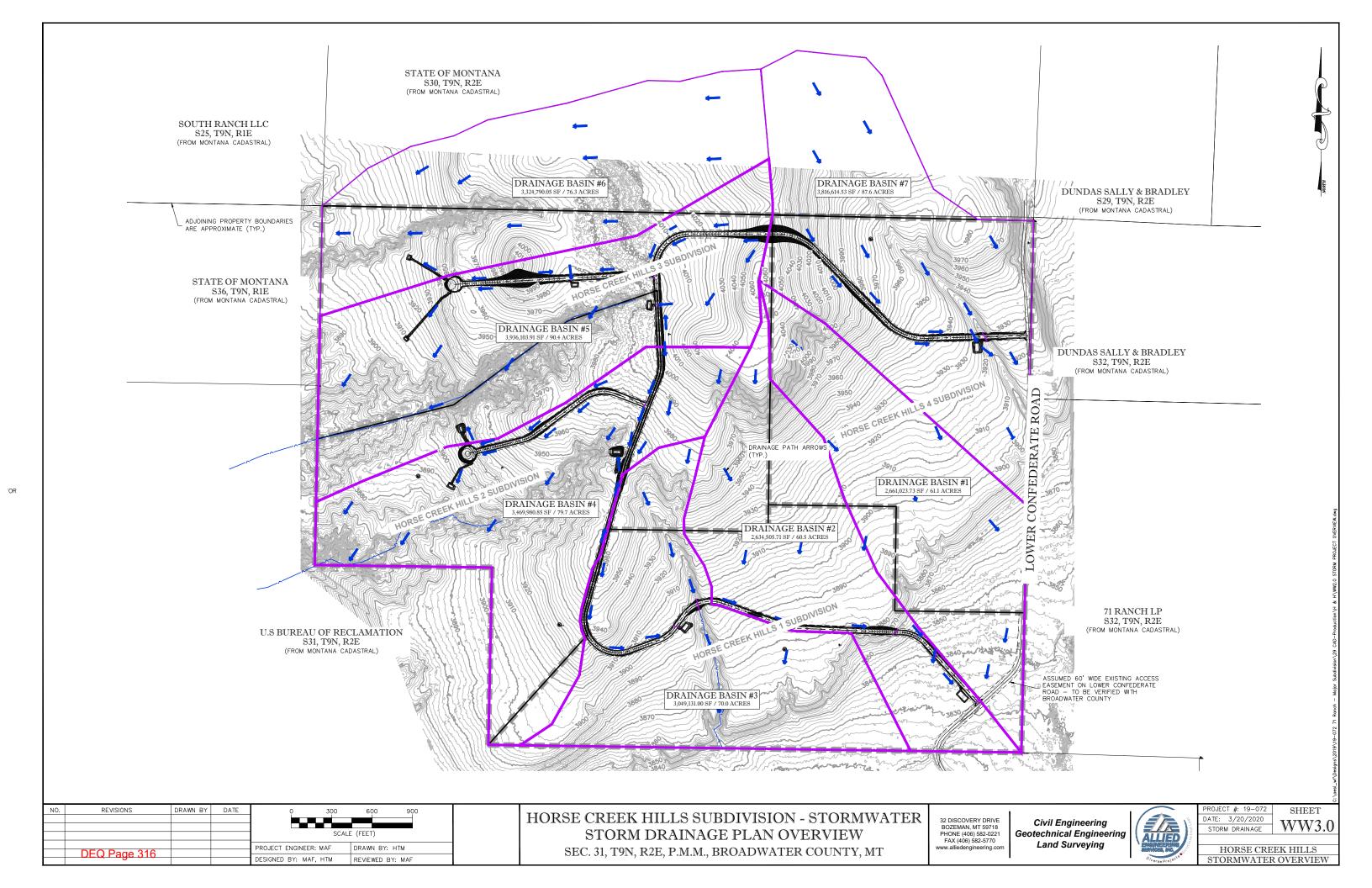
NO.	REVISIONS	DRAWN BY	DATE		
				PROJECT ENGINEER: MAF	DRAWN BY: HTM
	DEQ Page 315			DESIGNED BY: MAF, HTM	REVIEWED BY: MAF
	-			DESIGNED DI. MAL, HIM	INEVIEWED DI. MAP

HORSE CREEK HILLS WWTS DETAILS WASTEWATER TREATMENT SYSTEM SUMMARY SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com



ROJECT #: 19-072	SHEET					
ATE: 3/20/2020						
WWTS DETAILS	WW2.5					
HORSE CREEK HILLS						
WWTS F	PLANS					



		S	FRAWBE	RRY ROA	AN TRAIL			
SEGMENT ID #	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHIN & EASTING
L189	0+00.00	826,482.1902; 1,461,639.8195	N/A	755.72	S88° 27′ 40.34"W	N/A	7+55.72	826,461.8963; 1,460,884.3754
C1	7+55.72	826,461.8963; 1,460,884.3754	400.00	342.99	N66 58 24.92 W	N/A	10+98.71	826,591.9879; 1460578.2912
L190	10+98.71	826,591.9879; 1,460,578.2912	N/A	735.22	N44 19' 15.89"W	N/A	18+33.93	827,117.9894; 1,460,064.6099
C2	18+33.93	827,117.9894; 1,460,064.6099	400.00	298.01	N65 39 52.42"W	N/A	21+31.94	827,237.9727; 1459799.3139
L191	21+31.94	827,237.9727; 1,459,799.3139	N/A	674.27	S89° 58' 32.43"W	N/A	28+06.21	827,237.6864; 1,459,125.0454
C3	28+06.21	827,237.6864; 1,459,125.0454	250.00	391.59	S45' 06' 11.21"W	N/A	31+97.80	826,988.6924; 1458875.1535
L192	31+97.80	826,988.6924; 1,458,875.1535	N/A	708.07	S3 00' 48.58"E	N/A	39+05.86	826,281.6037; 1,458,912.3774
C4	39+05.86	826,281.6037; 1,458,912.3774	300.00	127.11	S9'03'11.56"W	N/A	40+32.97	826,157.0147; 1458892.5259
L193	40+32.97	826,157.0147; 1,458,892.5259	N/A	653.61	S21°11′28.51"W	N/A	46+86.58	825,547.6048; 1,458,656.2583
C5	46+86.58	825,547.6048; 1,458,656.2583	250.00	25.34	S18 17' 13.31"W	N/A	47+11.93	825,523.5509; 1458648.3093
L194	47+11.93	825,523.5509; 1,458,648.3093	N/A	1,123.31	S15°22′58.11"W	N/A	58+35.23	824,440.4879; 1,458,350.3337
C6	58+35.23	824,440.4879; 1,458,350.3337	250.00	544.51	S47 00' 47.37"E	N/A	63+79.74	824,138.3787; 1458674.4553
L195	63+79.74	824,138.3787; 1,458,674.4553	N/A	232.07	N70° 35' 27.16"E	N/A	66+11.81	824,215.4972; 1,458,893.3338
C7	66+11.81	824,215.4972; 1,458,893.3338	250.00	153.67	N52 58 54.92"E	N/A	67+65.47	824,306.5655; 1459014.1063
L196	67+65.47	824,306.5655; 1,459,014.1063	N/A	117.56	N35°22′22.69″E	N/A	68+83.03	824,402.4253; 1,459,082.1623
C8	68+83.03	824,402.4253; 1,459,082.1623	250.00	323.94	N72°29'36.32"E	N/A	72+06.97	824,493.1952; 1459369.9324
L197	72+06.97	824,493.1952; 1,459,369.9324	N/A	511.62	S70° 23' 10.05"E	N/A	77+18.59	824,321.4557; 1,459,851.8638
C9	77+18.59	824,321.4557; 1,459,851.8638	250.00	75.58	S79 02' 48.73"E	N/A	77+94.17	824,307.1498; 1459925.7840
L198	77+94.17	824,307.1498; 1,459,925.7840	N/A	777.91	S87* 42' 27.42"E	N/A	85+72.08	824,276.0342; 1,460,703.0703
C10	85+72.08	824,276.0342; 1,460,703.0703	250.00	199.23	S64 52 38.91"E	N/A	87+71.31	824,193.6704; 1460878.7185
L199	87+71.31	824,193.6704; 1.460.878.7185	N/A	605.19	S42 03 14.75 E	N/A	93+76.50	823,744.3085; 1.461.284.0946

N0.

			APPA	LOOSA	ΓRAIL			
EGMENT ID#	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L200	0+00.00	825,957.8812; 1,458,815.3220	N/A	254.84	N68 48 31.49"W	N/A	2+54.84	826,050.0031; 1,458,577.7099
L203	0+00.00	825,957.8812; 1,458,815.3220	N/A	254.84	N68° 48' 31.49"W	N/A	2+54.84	826,050.0031; 1,458,577.7099
C11	2+54.84	826,050.0031; 1,458,577.7099	250.00	250.90	S82 26' 26.76"W	N/A	5+05.74	826,018.3653; 1458339.3019
C13	2+54.84	826,050.0031; 1,458,577.7099	250.00	250.90	S82 26' 26.76"W	N/A	5+05.74	826,018.3653; 1458339.3019
L201	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53° 41' 25.01"W	N/A	9+64.33	825,746.8117; 1,457,969.7578
L204	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53° 41′ 25.01″W	N/A	9+64.33	825,746.8117; 1,457,969.7578
C12	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64° 49' 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
C14	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64 49 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
L202	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75 57 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
L205	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75° 57′ 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
				1 0337 8 1 1	E NODTH			
EGMENT ID#	START STATION		RADIUS [FT]	LENGTH [FT]	E NORTH LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L207	0+00.00	825,638.2166; 1,457,536.3127	N/A	2.86	N82° 46′ 27.03″W	N/A	0+02.86	825,638.5769; 1,457,533.4707
L208	0+02.86	825,638.5769; 1,457,533.4707	N/A	3.09	N59' 05' 34.29"W	N/A	0+05.95	825,640.1618; 1,457,530.8234
L209	0+05.95	825,640.1618; 1,457,530.8234	N/A	12.89	N43° 59' 30.64"W	N/A	0+18.84	825,649.4369; 1,457,521.8690
L210	0+18.84	825,649.4369; 1,457,521.8690	N/A	3.41	N43° 59' 30.64"W	N/A	0+22.25	825,651.8888; 1,457,519.5019
L211	0+22.25	825,651.8888; 1,457,519.5019	N/A	0.44	N90° 00' 00.00"W	N/A	0+22.69	825,651.8888; 1,457,519.0603
L212	0+22.69	825,651.8888; 1,457,519.0603	N/A	19.42	N57° 58' 04.11"W	N/A	0+42.12	825,662.1907; 1,457,502.5944
L213	0+42.12	825,662.1907; 1,457,502.5944	N/A	106.03	N35°14'27.11"W	N/A	1+48.15	825,748.7927; 1,457,441.4109
L214	1+48.15	825,748.7927; 1,457,441.4109	N/A	86.24	N17' 26' 26.64"W	N/A	2+34.39	825,831.0663; 1,457,415.5637
		Ì	APT PON	D 2 SWA	LE SOUTH			
SEGMENT ID #	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	I LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L215	0+00.00	825,608.4328; 1,457,567.4019	N/A	12.52	S70° 26' 48.72"V	V N/A	0+12.52	825,604.2412; 1,457,555.6000
L216	0+12.52	825,604.2412; 1,457,555.6000	N/A	28.25	S27° 40' 18.04"W	/ N/A	0+40.77	825,579.2224; 1,457,542.4806
L217	0+40.77	825,579.2224; 1,457,542.4806	N/A	19.89	S28' 26' 49.91"V	/ N/A	0+60.66	825,561.7344; 1,457,533.0062
L218	0+60.66	825,561.7344; 1,457,533.0062	N/A	16.83	S40' 09' 35.39"V	V N/A	0+77.50	825,548.8707; 1,457,522.1510
L219	0+77.50	825,548.8707; 1,457,522.1510	N/A	19.21	S39' 58' 28.96"V	V N/A	0+96.70	825,534.1519; 1,457,509.8116
L220	0+96.70	825,534.1519; 1,457,509.8116	N/A	54.21	S64' 59' 00.52"V	V N/A	1+50.92	825,511.2259; 1,457,460.6836
L221	1+50.92	825,511.2259; 1,457,460.6836	N/A	44.40	S66° 03' 31.98"W	/ N/A	1+95.32	825,493.2081; 1,457,420.1029
L222	1+95.32	825,493.2081; 1,457,420.1029	N/A	175.28	S30° 10' 36.13"W	/ N/A	3+70.60	825,341.6834; 1,457,331.9958
				-1			1	1
						1		
		BDIVISIO		-		BOZE	SCOVERY DRIVE MAN, MT 59718	Civil Engin
		ORDINAT				FAX	IE (406) 582-0221 (406) 582-5770 iedengineering.com	Geotechnical E Land Surv
T9N	R2E PMM	BROADWAT	'ER CC	DUNTY.	MT	www.can	icacingineering.com	

			1	LOOSA 7				
EGMENT ID#	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L200	0+00.00	825,957.8812; 1,458,815.3220	N/A	254.84	N68 48 31.49 W	N/A	2+54.84	826,050.0031; 1,458,577.7099
L203	0+00.00	825,957.8812; 1,458,815.3220	N/A	254.84	N68° 48' 31.49"W	N/A	2+54.84	826,050.0031; 1,458,577.7099
C11	2+54.84	826,050.0031; 1,458,577.7099	250.00	250.90	S82 26' 26.76"W	N/A	5+05.74	826,018.3653; 1458339.3019
C13	2+54.84	826,050.0031; 1,458,577.7099	250.00	250.90	S82° 26′ 26.76″W	N/A	5+05.74	826,018.3653; 1458339.3019
L201	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53° 41' 25.01"W	N/A	9+64.33	825,746.8117; 1,457,969.7578
L204	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53° 41′ 25.01″W	N/A	9+64.33	825,746.8117; 1,457,969.7578
C12	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64° 49' 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
C14	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64 49 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
L202	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75 57 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
L205	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75° 57′ 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
		AP	PT POND	1 SWALE	ENORTH			
EGMENT ID #	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L207	0+00.00	825,638.2166; 1,457,536.3127	N/A	2.86	N82 46 27.03 W	N/A	0+02.86	825,638.5769; 1,457,533.4707
L208	0+02.86	825,638.5769; 1,457,533.4707	N/A	3.09	N59'05'34.29"W	N/A	0+05.95	825,640.1618; 1,457,530.8234
L209	0+05.95	825,640.1618; 1,457,530.8234	N/A	12.89	N43 59 30.64"W	N/A	0+18.84	825,649.4369; 1,457,521.8690
L210	0+18.84	825,649.4369; 1,457,521.8690	N/A	3.41	N43°59'30.64"W	N/A	0+22.25	825,651.8888; 1,457,519.5019
L211	0+22.25	825,651.8888; 1,457,519.5019	N/A	0.44	N90° 00' 00.00"W	N/A	0+22.69	825,651.8888; 1,457,519.0603
L212	0+22.69	825,651.8888; 1,457,519.0603	N/A	19.42	N57 58' 04.11"W	N/A	0+42.12	825,662.1907; 1,457,502.5944
L213	0+42.12	825,662.1907; 1,457,502.5944	N/A	106.03	N35°14'27.11"W	N/A	1+48.15	825,748.7927; 1,457,441.4109
L214	1+48.15	825,748.7927; 1,457,441.4109	N/A	86.24	N17° 26' 26.64"W	N/A	2+34.39	825,831.0663; 1,457,415.5637
		·						
		А	PT PON	D 2 SWAI	LE SOUTH			
SEGMENT	START STATION	START NORTHING	RADIUS			A Value	END STATION	END NORTHING
ID #	0+00.00	& EASTING 825,608.4328;	[FT]	[FT] 12.52	DIRECTION \$70° 26' 48.72"W	N/A	0+12.52	& EASTING 825,604.2412;
L210	0+12.52	1,457,567.4019 825,604.2412;	N/A	28.25	S27° 40' 18.04"W		0+40.77	1,457,555.6000 825,579.2224;
		1,457,555.6000 825,579.2224;	N/A					1,457,542.4806 825,561.7344;
L217	0+40.77	1,457,542.4806 825,561.7344;		19.89	S28' 26' 49.91"W	N/A	0+60.66	1,457,533.0062 825,548.8707;
L218	0+60.66	1,457,533.0062 825,548.8707;	N/A	16.83	S40' 09' 35.39"W		0+77.50	1,457,522.1510 825,534.1519;
L219	0+77.50	1,457,522.1510 825,534.1519;	N/A	19.21	S39' 58' 28.96"W		0+96.70	1,457,509.8116 825,511.2259;
L220	0+96.70	1,457,509.8116 825,511.2259;	N/A	54.21	S64' 59' 00.52"W	N/A	1+50.92	1,457,460.6836 825,493.2081;
L221	1+50.92	1,457,460.6836	N/A	44.40	S66' 03' 31.98"W	N/A	1+95.32	1,457,420.1029
	1+95.32	825,493.2081; 1,457,420.1029	N/A	175.28	S30' 10' 36.13"W	N/A	3+70.60	825,341.6834; 1,457,331.9958

EGMENT ID # L200 L203 C11 C13 L201 L204	START STATION 0+00.00 0+00.00 2+54.84	START NORTHING & EASTING 825,957.8812; 1,458,815.3220 825,957.8812; 1,458,815.3220	RADIUS [FT] N/A	LENGTH [FT] 254.84	LINE/CHORD DIRECTION N68' 48' 31.49"W	A Value	END STATION	END NORTHING & EASTING
L203 C11 C13 L201	0+00.00	1,458,815.3220 825,957.8812;	N/A	254.84	N68' 48' 31.49"W			
C11 C13 L201						N/A	2+54.84	826,050.0031; 1,458,577.7099
C13 L201	2+54.84		N/A	254.84	N68 48 31.49"W	N/A	2+54.84	826,050.0031; 1,458,577.7099
L201		826,050.0031; 1,458,577.7099	250.00	250.90	S82 26' 26.76"W	N/A	5+05.74	826,018.3653; 1458339.3019
	2+54.84	826,050.0031; 1,458,577.7099	250.00	250.90	S82* 26' 26.76"W	N/A	5+05.74	826,018.3653; 1458339.3019
1204	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53° 41' 25.01"W	N/A	9+64.33	825,746.8117; 1,457,969.7578
LZOT	5+05.74	826,018.3653; 1,458,339.3019	N/A	458.59	S53° 41′ 25.01″W	N/A	9+64.33	825,746.8117; 1,457,969.7578
C12	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64° 49' 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
C14	9+64.33	825,746.8117; 1,457,969.7578	250.00	97.18	S64° 49' 34.78"W	N/A	10+61.51	825,705.7345; 1457882.3601
L202	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75 57 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
L205	10+61.51	825,705.7345; 1,457,882.3601	N/A	408.49	S75° 57' 44.56"W	N/A	14+70.00	825,606.6509; 1,457,486.0664
					ENORTH			
EGMENT ID#	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L207	0+00.00	825,638.2166; 1,457,536.3127	N/A	2.86	N82 46 27.03 W	N/A	0+02.86	825,638.5769; 1,457,533.4707
L208	0+02.86	825,638.5769; 1,457,533.4707	N/A	3.09	N59'05'34.29"W	N/A	0+05.95	825,640.1618; 1,457,530.8234
L209	0+05.95	825,640.1618; 1,457,530.8234	N/A	12.89	N43 59 30.64"W	N/A	0+18.84	825,649.4369; 1,457,521.8690
L210	0+18.84	825,649.4369; 1,457,521.8690	N/A	3.41	N43 59' 30.64"W	N/A	0+22.25	825,651.8888; 1,457,519.5019
L211	0+22.25	825,651.8888; 1,457,519.5019	N/A	0.44	N90°00'00.00"W	N/A	0+22.69	825,651.8888; 1,457,519.0603
L212	0+22.69	825,651.8888; 1,457,519.0603	N/A	19.42	N57 58 04.11"W	N/A	0+42.12	825,662.1907; 1,457,502.5944
L213	0+42.12	825,662.1907; 1,457,502.5944	N/A	106.03	N35°14'27.11"W	N/A	1+48.15	825,748.7927; 1,457,441.4109
L214	1+48.15	825,748.7927; 1,457,441.4109	N/A	86.24	N17' 26' 26.64"W	N/A	2+34.39	825,831.0663; 1,457,415.5637
		A	PT PON	D 2 SWAI	LE SOUTH			
SEGMEN ID #	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L215	0+00.00	825,608.4328;	N/A	12.52	S70' 26' 48.72"W	/ N/A	0+12.52	825,604.2412;
L216	0+12.52	1,457,567.4019 825,604.2412;	N/A	28.25	S27° 40' 18.04"W	+	0+40.77	1,457,555.6000 825,579.2224;
L210	0+40.77	1,457,555.6000 825,579.2224;	N/A	19.89	S28' 26' 49.91"W		0+60.66	1,457,542.4806 825,561.7344;
L217	0+60.66	1,457,542.4806 825,561.7344;	N/A	16.83	S40° 09' 35.39"W		0+77.50	1,457,533.0062 825,548.8707;
		1,457,533.0062 825,548.8707;						1,457,522.1510 825,534.1519;
L219	0+77.50	1,457,522.1510 825,534.1519;	N/A	19.21	S39' 58' 28.96"W		0+96.70	1,457,509.8116 825,511.2259;
L220	0+96.70	1,457,509.8116 825,511.2259;	N/A	54.21	S64' 59' 00.52"W		1+50.92	1,457,460.6836 825,493.2081;
L221	1+50.92	825,493.2081;	N/A	44.40	S66°03'31.98"W	+	1+95.32	825,341.6834;
L222	1+95.32	1,457,420.1029	N/A	175.28	S30' 10' 36.13"W	N/A	3+70.60	1,457,331.9958

REVISIONS	DRAWN BY	DATE				
					HORSE CREEK HILLS SUBDIVISION - STORMWATER	32 DISCO
					ALIGNMENT COORDINATE TABLES	BOZEMA PHONE (4
				1	ALIGINMENT COORDINATE TABLES	FAX (40
DEQ Page 317			PROJECT ENGINEER: MAF	DRAWN BY: HTM	SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT	www.alliede
DEQPAGEST			DESIGNED BY: MAF, HTM	REVIEWED BY: MAF		

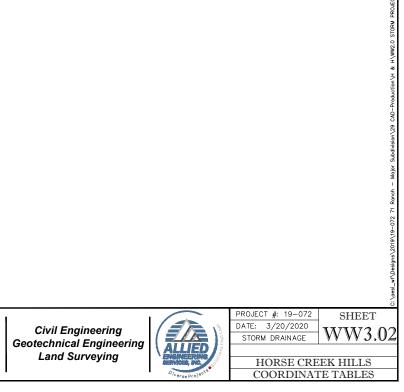


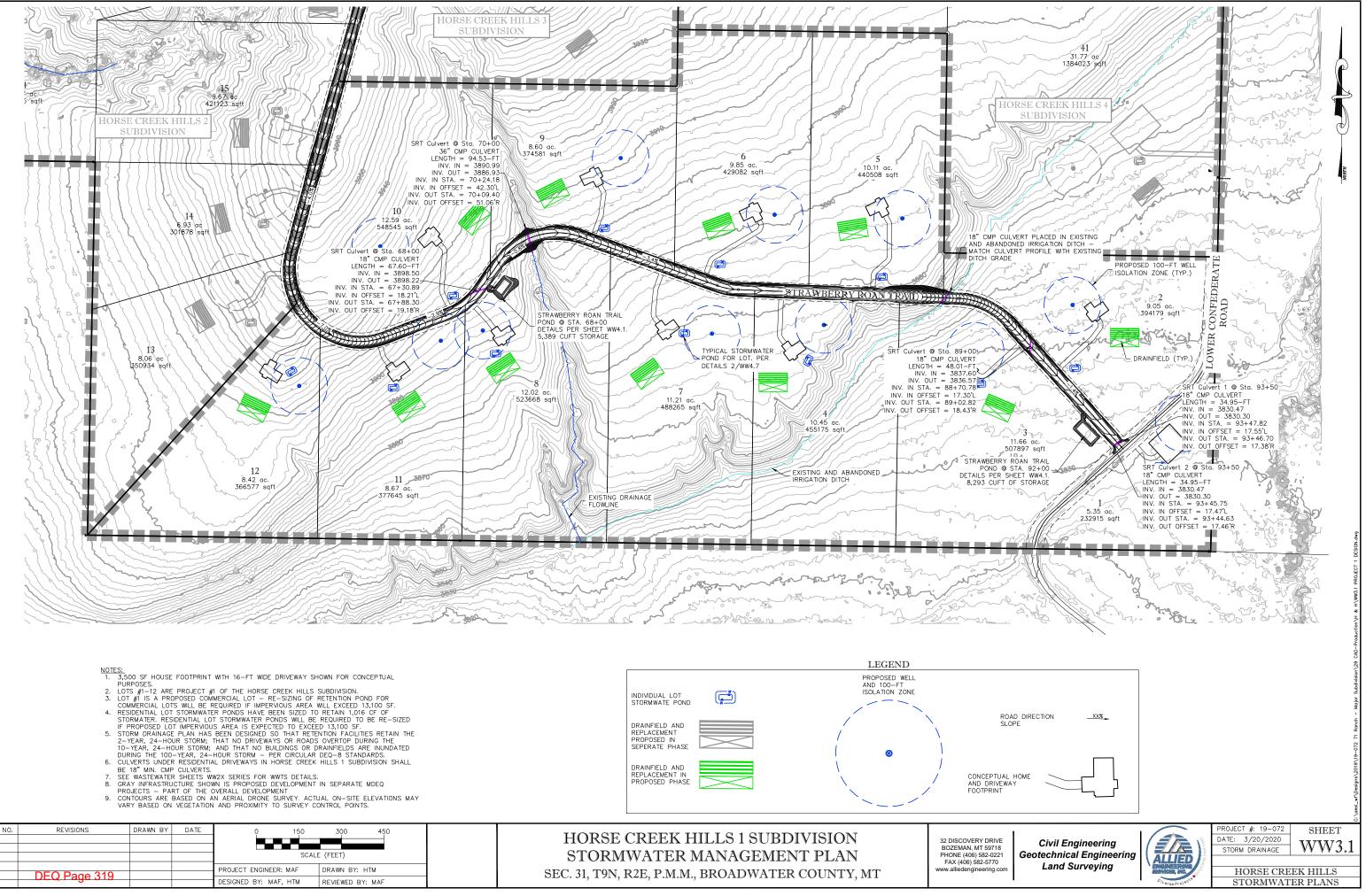
	BUCKSKIN TRAIL												
SEGMENT ID#	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHIN & EASTING					
L206	0+00.00	826,943.5358; 1,458,877.5307	N/A	1,500.00	S86° 54' 54.60"W	N/A	15+00.00	826,862.8140; 1,457,379.704					

		B	ST PONI	D1SWAL	E NORTH			
SEGMENT ID #	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING
L223	0+00.00	826,916.6624; 1,457,395.0411	N/A	8.39	N78 12' 17.64"W	N/A	0+08.39	826,918.3775; 1,457,386.8280
L224	0+08.39	826,918.3775; 1,457,386.8280	N/A	11.53	N90°00'00.00"W	N/A	0+19.92	826,918.3775; 1,457,375.2971
L225	0+19.92	826,918.3775; 1,457,375.2971	N/A	21.41	S73° 52' 32.96"W	N/A	0+41.33	826,912.4322; 1,457,354.7319
L226	0+41.33	826,912.4322; 1,457,354.7319	N/A	25.82	S70°28'32.42"W	N/A	0+67.14	826,903.8045; 1,457,330.4009
L227	0+67.14	826,903.8045; 1,457,330.4009	N/A	16.40	S83 03' 39.63"W	N/A	0+83.54	826,901.8231; 1,457,314.1204
L228	0+83.54	826,901.8231; 1,457,314.1204	N/A	84.22	N59'15'21.41"W	N/A	1+67.77	826,944.8775; 1,457,241.7354
L229	1+67.77	826,944.8775; 1,457,241.7354	N/A	207.23	N59 15' 21.41"W	N/A	3+74.99	827,050.8137; 1,457,063.6305
L230	3+74.99	827,050.8137; 1,457,063.6305	N/A	51.57	N59°15'21.41"W	N/A	4+26.57	827,077.1785; 1,457,019.3048

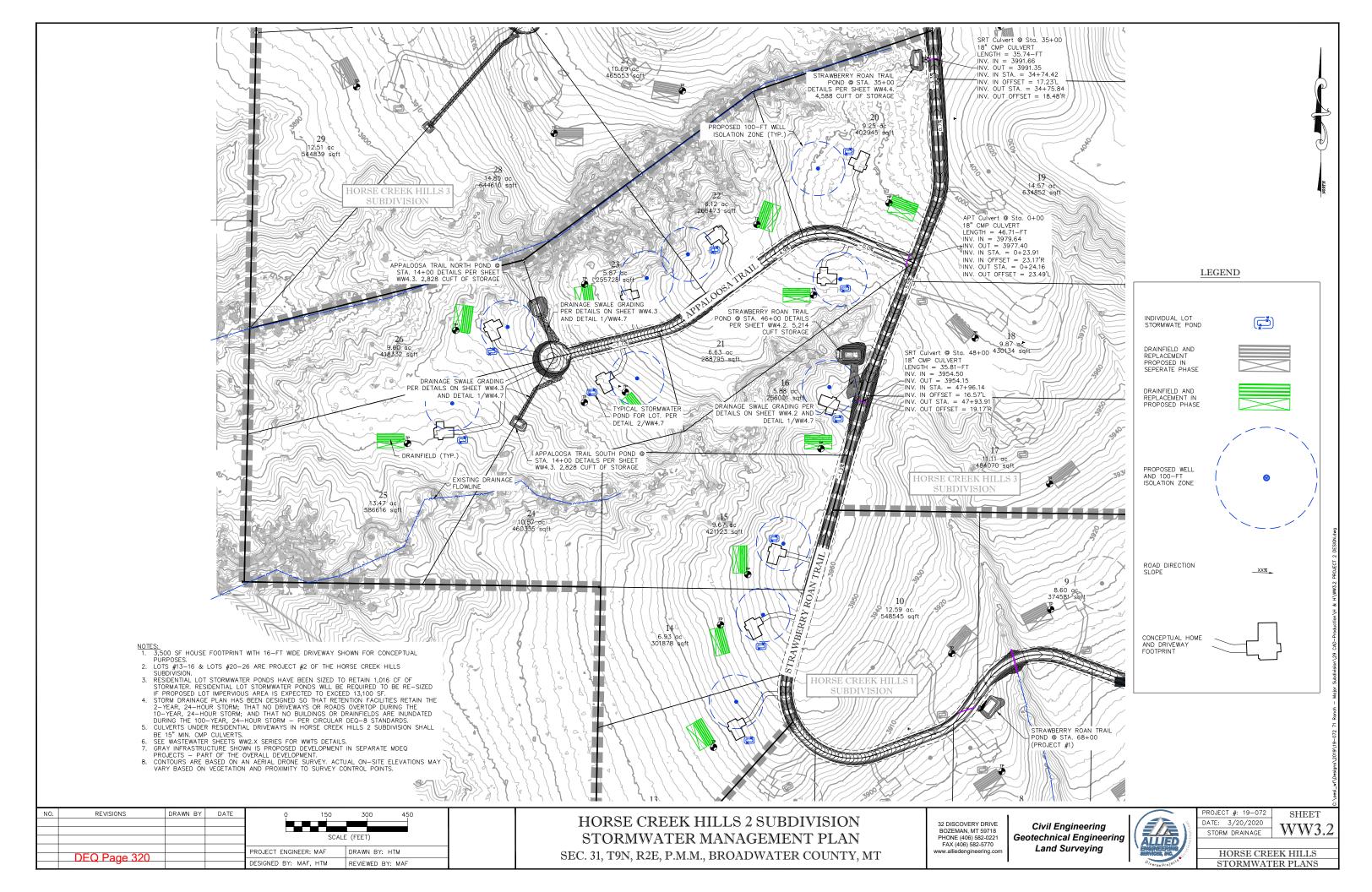
BST POND 2 SWALE SOUTH												
SEGMENT ID#	START STATION	START NORTHING & EASTING	RADIUS [FT]	LENGTH [FT]	LINE/CHORD DIRECTION	A Value	END STATION	END NORTHING & EASTING				
L231	0+00.00	826,810.9266; 1,457,400.7388	N/A	7.82	S70°49'15.53"W	N/A	0+07.82	826,808.3590; 1,457,393.3570				
L232	0+07.82	826,808.3590; 1,457,393.3570	N/A	9.05	S82°41'22.27"W	N/A	0+16.87	826,807.2071; 1,457,384.3780				
L233	0+16.87	826,807.2071; 1,457,384.3780	N/A	40.98	S77° 54' 37.00"W	N/A	0+57.85	826,798.6231; 1,457,344.3023				
L234	0+57.85	826,798.6231; 1,457,344.3023	N/A	65.90	S55 49'18.34"W	N/A	1+23.75	826,761.6045; 1,457,289.7866				
L235	1+23.75	826,761.6045; 1,457,289.7866	N/A	444.76	S41° 37' 08.04"W	N/A	5+68.51	826,429.1084; 1,456,994.3865				

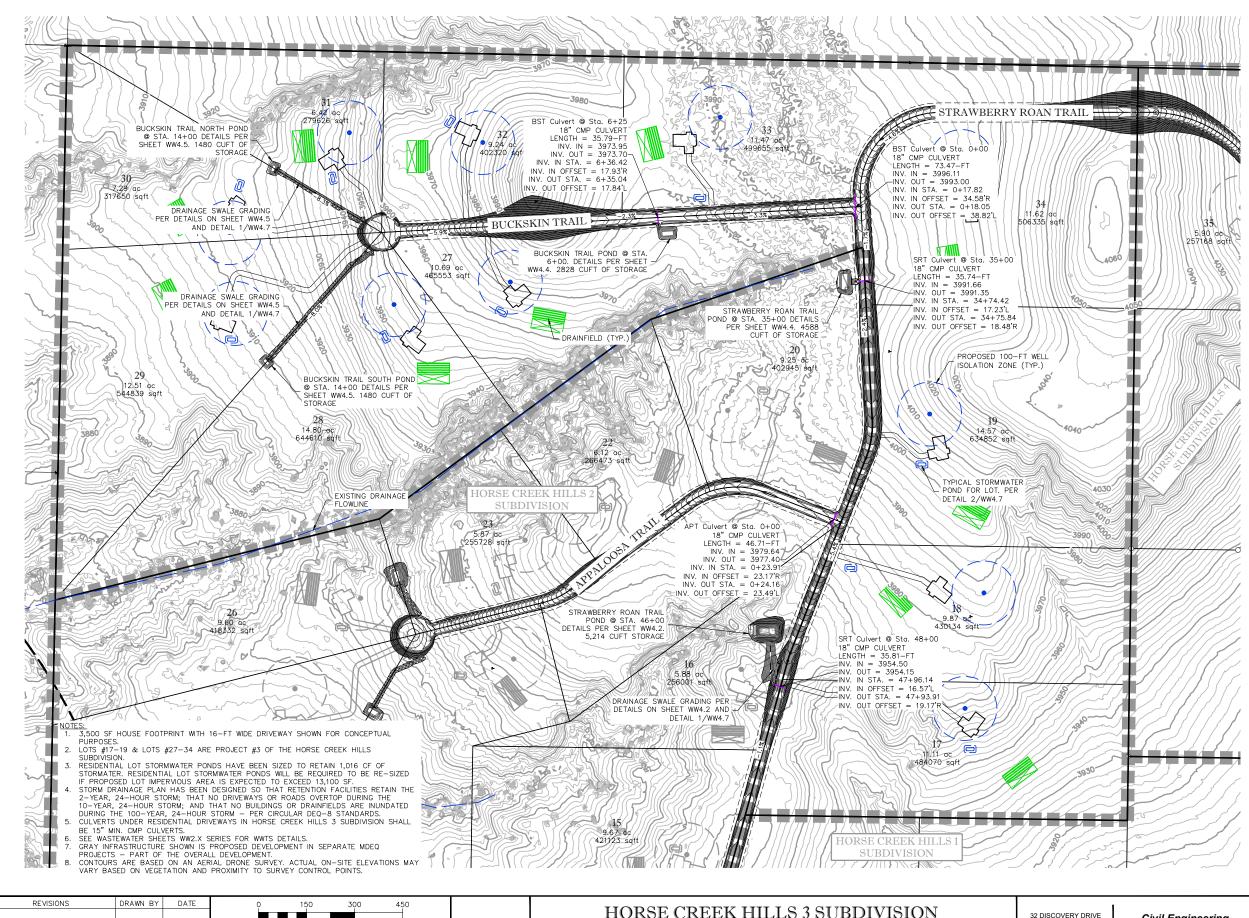
NO.	REVISIONS	DRAWN BY	DATE	PROJECT ENGINEER' MAE	DRAWN BY- HTM	HORSE CREEK HILLS SUBDIVISION - STORMWATER ALIGNMENT COORDINATE TABLES	32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.elliedengineering.com
				PROJECT ENGINEER: MAF	DRAWN BY: HTM	SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT	FAX (406) 582-5770 www.alliedengineering.com
	DEQ Page 318			DESIGNED BY: MAF, HTM	REVIEWED BY: MAF	SLC. 31, 1911, N2L, 1. MMA, BROMD WITTER COURT 1, MI	





NOTES:	LEGEND
 3,500 SF HOUSE FOOTPRINT WITH 16-FT WIDE DRIVEWAY SHOWN FOR CONCEPTUAL PURPOSES. LOTS #1-12 ARE PROJECT #1 OF THE HORSE CREEK HILLS SUBDIVISION. LOTS #1-12 ARE PROJECT #1 OF THE HORSE CREEK HILLS SUBDIVISION. LOT #1 IS A PROPOSED COMMERCIAL LOT - RE-SIZING OF RETENTION POND FOR COMMERCIAL LOTS WILL BE REQUIRED IF IMPERVIOUS AREA WILL EXCEED 13,100 SF. RESIDENTIAL LOT STORMWATER PONDS HAVE BEEN SIZED TO RETAIN 1,016 CF OF STORMATER. RESIDENTIAL LOT STORMWATER PONDS WILL BE REQUIRED TO BE RE-SIZED IF PROPOSED LOT IMPERVIOUS AREA IS EXPECTED TO EXCEED 13,100 SF. STORM DRAINAGE PLAN HAS BEEN DESIGNED SO THAT RETENTION FACLUITES RETAIN THE 2-YEAR, 24-HOUR STORM; AND THAT NO DUILDINGS OR DRAINFIELDS ARE INUNDATED DURING THE 100-YEAR, 24-HOUR STORM - PER CIRCULAR DEQ-8 STANDARDS. CULVERTS UNDER RESIDENTIAL DRIVEWAYS IN HORSE CREEK HILLS 1 SUBDIVISION SHALL BE 18" MIN. CMP CULVERTS. SEE WASTEWATER SHEETS WW2X SERIES FOR WWTS DETAILS. REASTRUCTURE SHOWN IS PROPOSED DEVELOPMENT IN SEPARATE MDEQ PROJECTS - PART OF THE OVERALL DEVELOPMENT IN SEPARATE MDEQ PROJECTS - PART OF THE OVERALL DEVELOPMENT IN SEPARATE MDEQ PROJECTS - PART OF THE OVERALL DEVELOPMENT IN SEPARATE MDEQ PROJECTS - PART OF THE OVERALL DEVELOPMENT IN SEPARATE MDEQ PROJECTS - PART OF THE OVERALL DEVELOPMENT CONTOURS ARE BASED ON AN AERIAL DRONE SURVEY. ACTUAL ON-SITE ELEVATIONS MAY VARY BASED ON VEGETATION AND PROXIMITY TO SURVEY CONTROL POINTS. 	INDIVIDUAL LOT STORWWATE POND DRAINFIELD AND REPLACEMENT PROPOSED IN SEPERATE PHASE DRAINFIELD AND REPLACEMENT IN PROPOSED PHASE CONCEPTUAL HOW AND DRIVEWAY FOOTPRINT
REVISIONS DRAWN BY DATE 0 150 300 450 SCALE (FEET) SCALE (FEET)	HORSE CREEK HILLS 1 SUBDIVISION STORMWATER MANAGEMENT PLAN

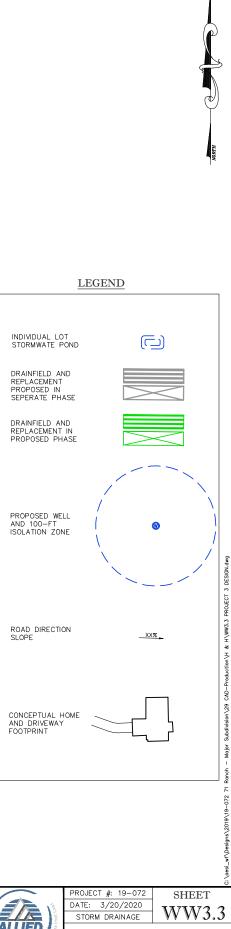




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				SCALE (FEET)				
				PROJECT ENGINEER: M	۵F	DRAWN BY: HTM	<u>,</u>	
	DEQ Page 321							
				DESIGNED BY: MAE. H	TM	REVIEWED BY'N	JAF	

HORSE CREEK HILLS 3 SUBDIVISION STORMWATER MANAGEMENT PLAN SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT

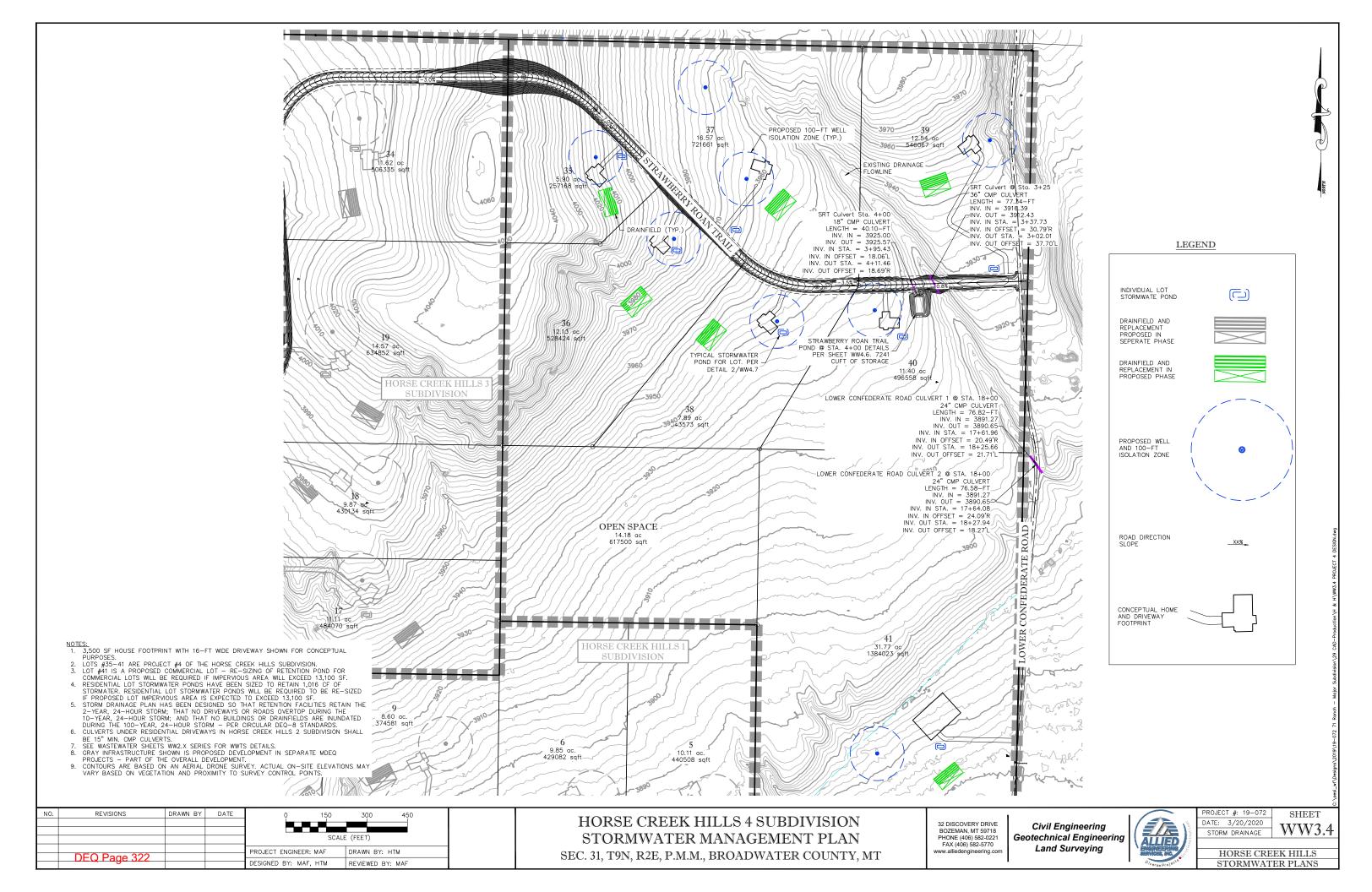
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

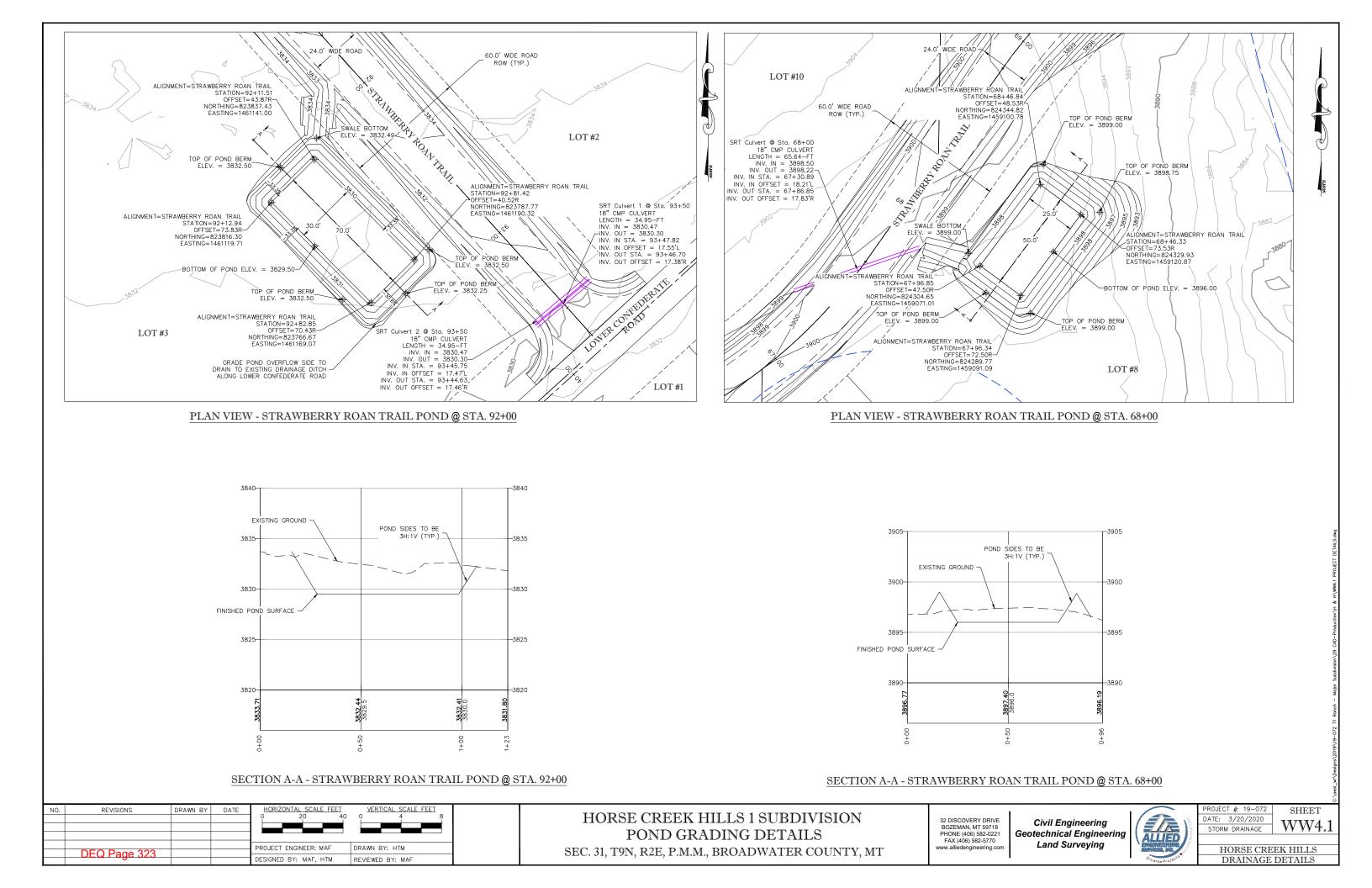


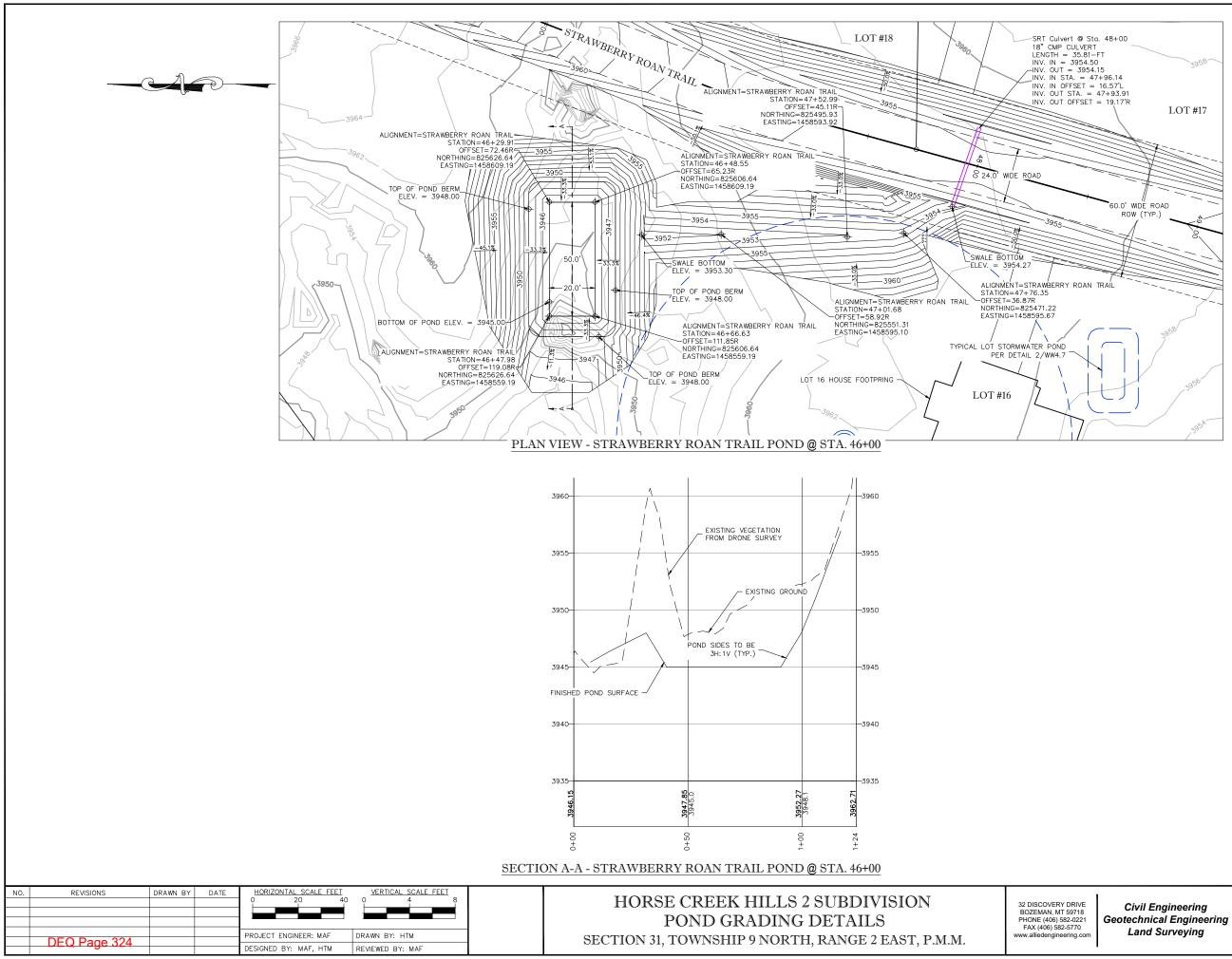
HORSE CREEK HILLS

STORMWATER PLANS



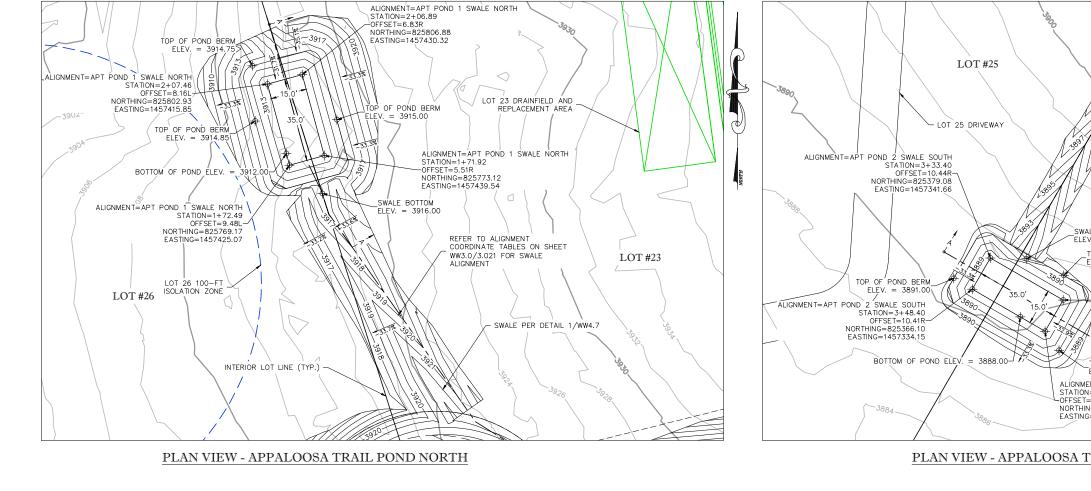


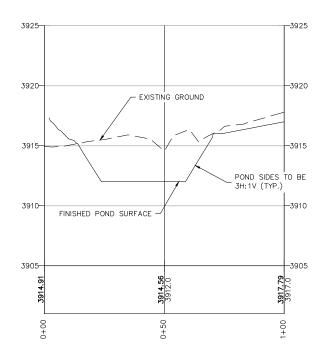




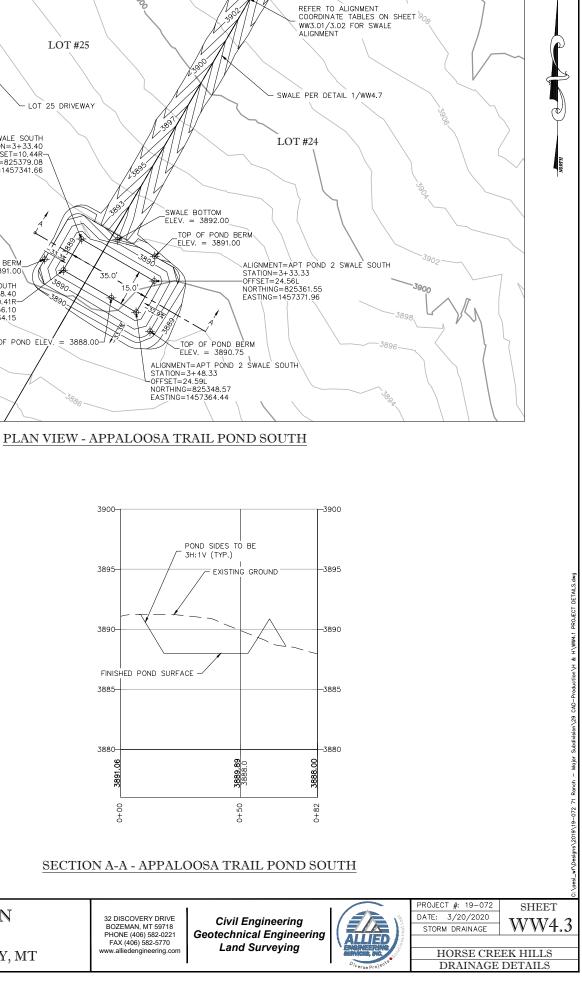






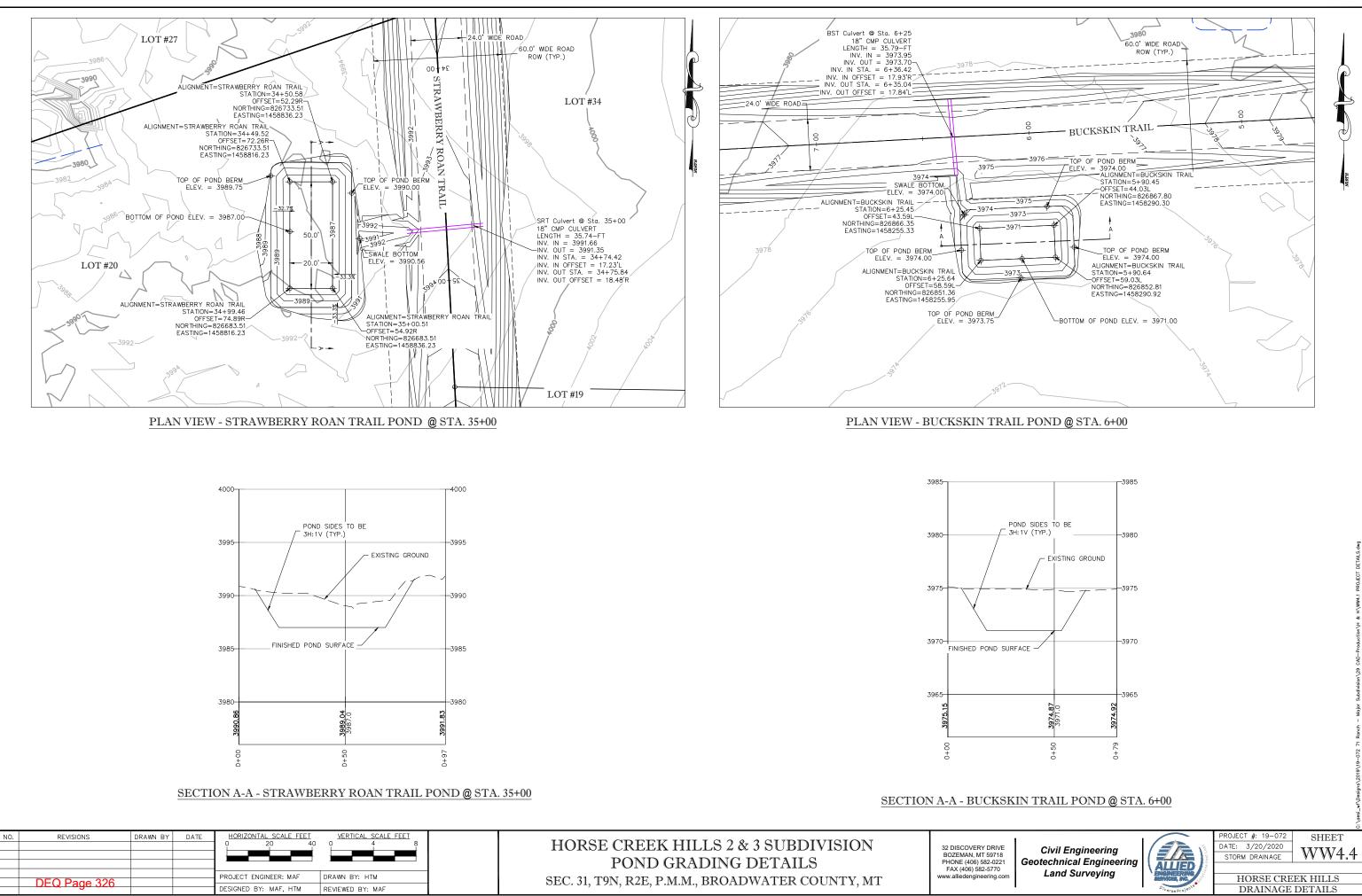


SECTION A-A - APPALOOSA TRAIL POND NORTH

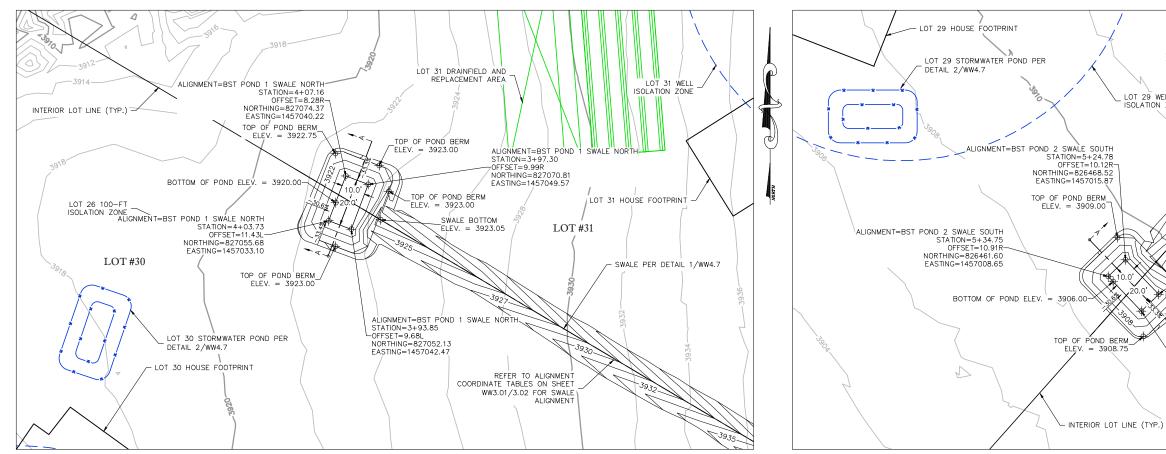


HORSE CREEK HILLS 2 SUBDIVISION	
POND GRADING DETAILS	
SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT	

NO.	REVISIONS	DRAWN BY	DATE	HORIZONTAL SCALE FEET	VERTICAL SCALE FEET	
				0 20 40	0 4 8	
				DDD FOT FNON FED NAF		1
	DEQ Page 325			PROJECT ENGINEER: MAF	DRAWN BY: HTM	
	DLQ Fage 323			DESIGNED BY: MAF, HTM	REVIEWED BY: MAF	

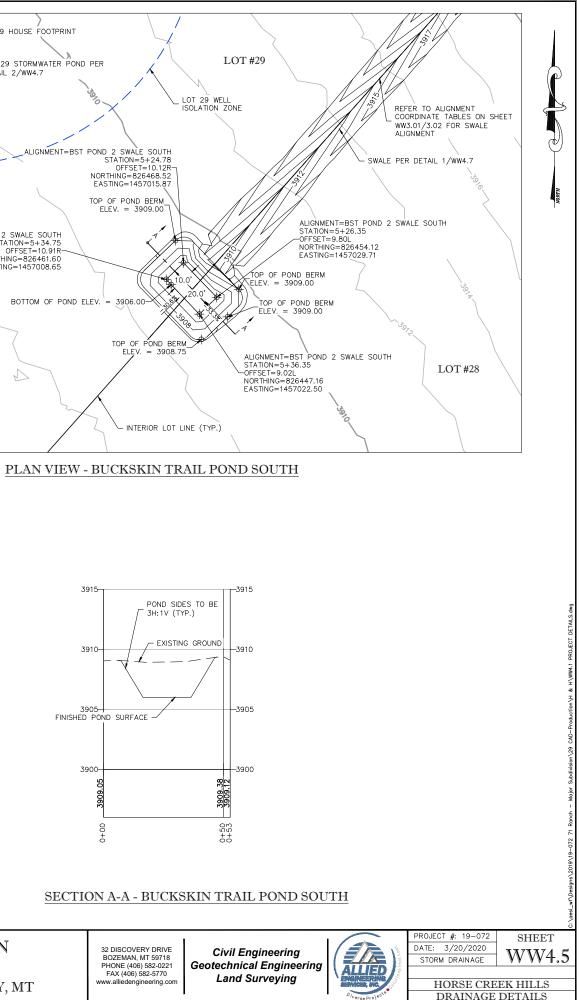


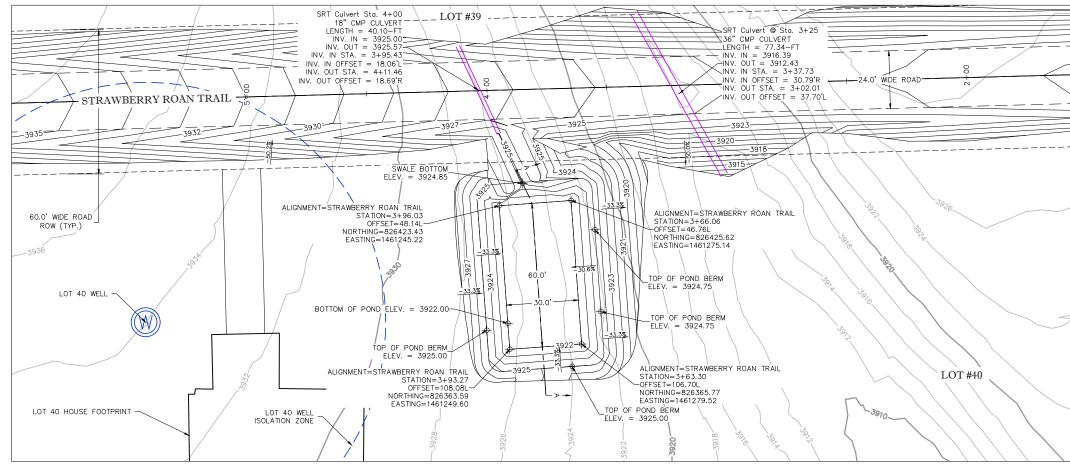
3930		
POND SIDES TO BE 3H: 1V (TYP.) 3925 EXISTING GROUND 3925	3915	POND SIDES TO BE
3920 FINISHED POND SURFACE	3910	
3915	3905 FINISHED PO	OND SURFACE
3910 3910 3910 3910 3910 3910 3910 3910	3900	390.90 2300.90 2300.95 2300.95 2300.95 2300.95 2300.95 20 20 20 20 20 20 20 20 20 20 20 20 20
		0+00
SECTION A-A - BUCKSKIN TRAIL PONI	<u>D NORTH</u>	N A-A - BUCKSKIN TI
RAWN BY DATE HORIZONTAL SCALE FEET 0 20 40 4 8 PROJECT ENGINEER: MAF DRAWN BY: HTM DESIGNED BY: MAF, HTM REVIEWED BY: MAF	HORSE CREEK HILLS 3 SUBDIVISION POND GRADING DETAILS SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT	32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-5770 FAX (406) 582-5770 www.alliedengineering.com



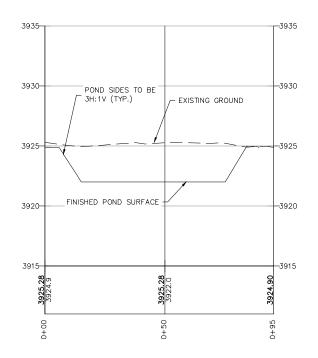
PLAN VIEW - BUCKSKIN TRAIL POND NORTH

N0.	REVISIONS	DRAWN BY	DATE	HORIZONTAL SCALE FEET VERTICAL SCALE FEET	
				0 20 40 0 4 8	
				PROJECT ENGINEER: MAF DRAWN BY: HTM	
	DEQ Page 327				
				DESIGNED BY: MAF, HTM REVIEWED BY: MAF	





PLAN VIEW - STRAWBERRY ROAN TRAIL POND @ STA. 4+00



SECTION A-A - STRAWBERRY ROAN TRAIL POND @ STA. 4+00

NO.	REVISIONS	DRAWN BY	DATE	HORIZONTAL SCALE FEET	VERTICAL SCALE FEET	
				0 20 40	0 4 8	
				DDO FOT FNONFED MAE		1
	DEQ Page 328			PROJECT ENGINEER: MAF	DRAWN BY: HTM	
	DEQTAGE 520			DESIGNED BY: MAF, HTM	REVIEWED BY: MAF	

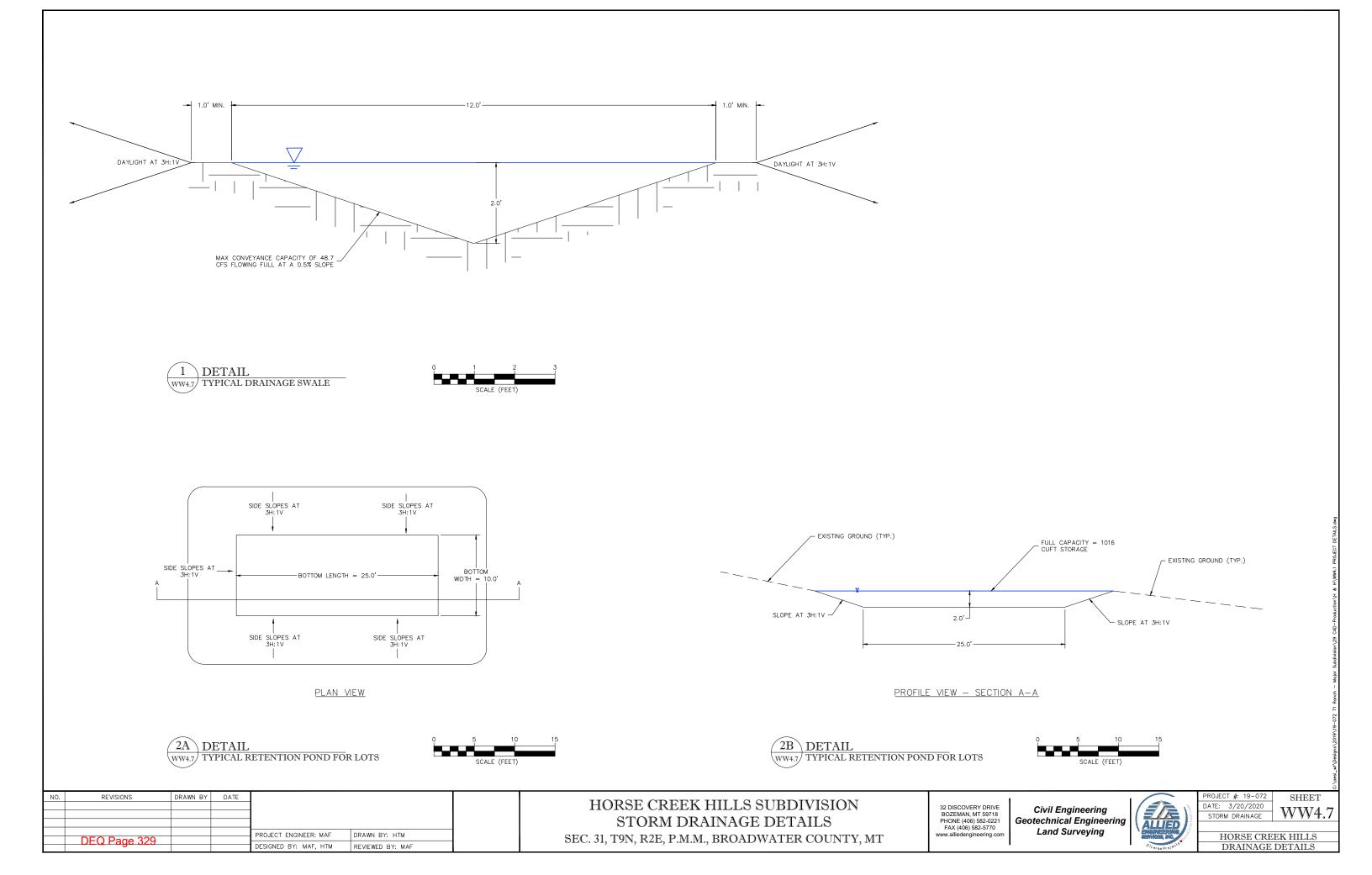
HORSE CREEK HILLS 4 SUBDIVISION POND GRADING DETAILS SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT

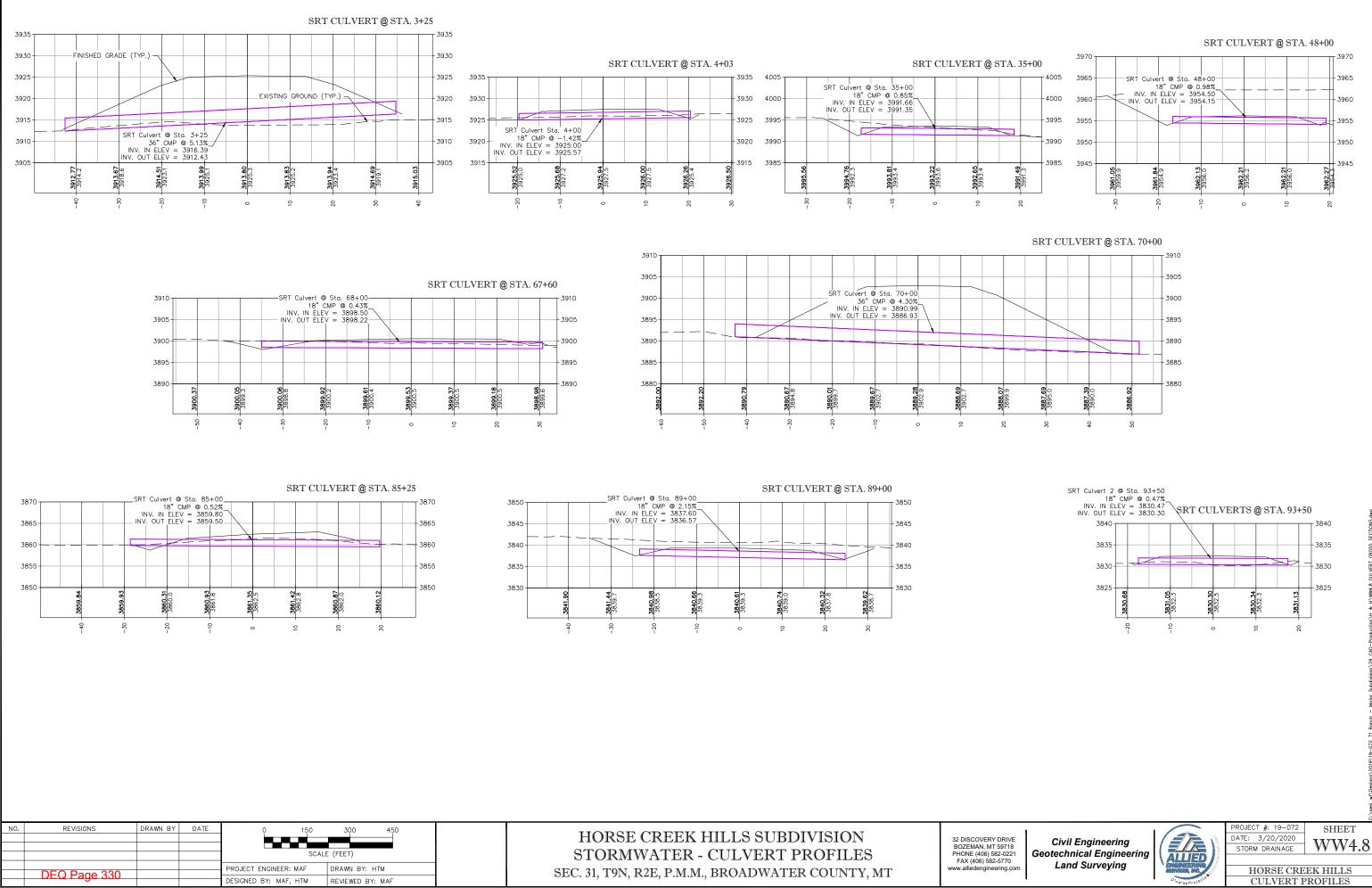
32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

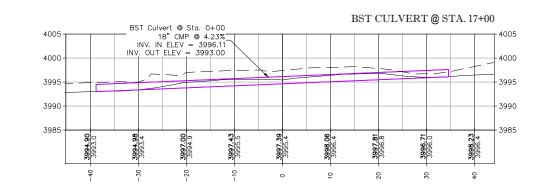




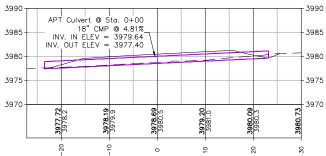


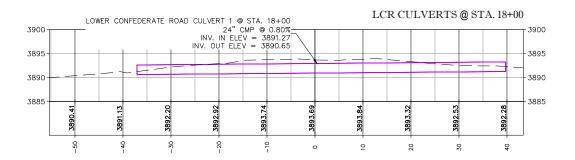






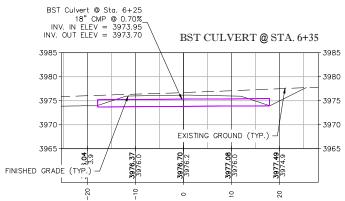






HORSE CREEK HILLS SUBDIVISION
STORMWATER - CULVERT PROFILES
SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT

NO.	REVISIÓNS	DRAWN BY	DATE	0	150	300	450	
						()		
				SCALE (FEET)				
				PROJECT ENGINEER	R. MAF	DRAWN BY: H	ТМ	
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Civil Engineering Geotechnical Engineering Land Surveying

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com



ROJECT #: 19-072	SHEET
ATE: 3/20/2020	****
STORM DRAINAGE	WW4.9
HORSE CRE	EK HILLS
CULVERT F	PROFILES

Appendix H

Wastewater System

- Drainfield Sizing Calculations
- Biotube Effluent Filter Sizing
- Lot Layout (4 Copies)
- Details (4 Copies)

SUMMARY OF PROPOSED WASTEWATER TREATMENT TYPE CORRESPONDING TO EACH LOT

1 24 Employees 312 Sit. 0.4 1031 780 390 391 0.75 586 222.5 23.75 (Type 0) 0.6 2 5 400 Sit. 0.4 16-31 1000 500 20.100 (Type A) 0.75 790 375 30.75 (Type 0) 0.6 4 5 400 Sit. 0.4 16-31 1000 500 20.100 (Type A) 0.75 790 375 30.75 (Type 0) 0.6 5 400 Sit. 0.4 16-31 1000 500 20.100 (Type A) 0.75 790 375 30.75 (Type 0) A 6 5 400 Sit. 0.4 16-31 1000 500 20.100 (Type A) 0.75 790 375 30.75 (Type C) A 9 5 400 Sit. 0.4 16-31 1000 500 30.200 (Type A) 0.75 790 375 30.75 (Type C) A 110 5 400<	Lot Numer	#of Bedrooms	GPD of Wastewater	Texture	Application Rate (gpd/ft^2)	Corresponding Percolation Rate (min/inch)	Min. Drainfield Area (sf)	Length of Lateral (LF)	Min. Drainfield Dimensions (ft)	Infiltrator Size Reduction	Min. Drainfield Area (sf)	-	Min. Drainfield Dimensions (ft)	ISystem to hel
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1 DETAIL WW2.5 SUMMARY OF DRAINFIELD DIMENSIONS NOT TO SCALE

NO.	REVISIONS	DRAWN BY	DATE		
				PROJECT ENGINEER: MAF	DRAWN BY: HTM
	DEQ Page 333			DESIGNED BY: MAF, HTM	REVIEWED BY: MAF
				DESIGNED DT. MIXI, TTM	REVIEWED DI. MAI

HORSE CREEK HILLS WWTS DETAILS WASTEWATER TREATMENT SYSTEM SUMMARY SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.com

Summary of Drainfield Sizing Calculations



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OJECT #: 19-072	SHEET
TE: 3/20/2020	
WWTS DETAILS	WW2.5
HORSE CRE	EK HILLS
WWTS F	PLANS



Orenco has developed guidelines for calculating the correct sizing of and cleaning frequencies for effluent filters, based on decades of experience as well as monitoring data from thousands of effluent filter installations.*

While these guidelines may not be accurate for every wastewater system, they will be relevant to most situations. (See "Filter Facts," AFL-FT-2, for more information.)

Guidelines were based on the following criteria:

Watertightness

A completely watertight septic tank must be used. If either infiltration or exfiltration is present, there is no way to accurately determine filter sizing.

Hydraulic Retention Time

<u>Residential flows</u> — A septic tank capacity of at least 1000 gallons is used for systems handling flows from a single-family residence of three bedrooms or less. A septic tank capacity of at least 1500 gallons is used for 3-bedroom homes with garbage disposals and for systems handling flows from a single-family residence with more than three bedrooms, up to flows of 600 gpd.

<u>Larger flows</u> — Adequate septic tankage will anaerobically digest organic material, remove settleable and floatable solids, help modulate flow, and consistently discharge effluent that meets "primary treatment" standards.

A septic tank capacity of at least three times the daily design flow is used for systems handling flows greater than those of a single-family home.

After conducting extensive research on septic tankage, Orenco has found that smaller tankage will result in suboptimal effluent quality and more frequent septage pumping. For Orenco's tank sizing recommendations for various applications, see "Primary Tank Sizing," NDA-TNK-1 and "Septic Tank Sizes for Large Flows," NTP-TNK-TRB-2.

Waste Strength

Residential strength wastewater that has been through primary treatment is used. This is equivalent to what Crites and Tchobanoglous describe as "expected effluent wastewater characteristics from a residential septic tank without ... effluent filter" (*Small and Decentralized Wastewater Management* Systems, Table 4-16, p. 183). Here are the parameters:

BOD = 180 mg/L TSS = 80 mg/L Oil & Grease = 25 mg/L

Sizing Equations

 $A_F = C_f (Q) (MTBC)$

where:

 $A_F = Filter$ area required (ft²)

 $C_f = Filter coefficient \left(\frac{ft^2}{gpd \cdot yr}\right)$

Q = Daily flow in gallons (gpd)

MTBC = Mean time between filter cleaning (years)

The filter coefficient, C_f , is equal to 0.0044 when actual or true daily flow rates are used. A value of 0.002 is applicable if design flow is used. The design flow is defined as a peak flow that allows for a safety margin and is typically about twice the actual flow. All values are based on a filter surface area with approximately 30% or more open or "flow" area.

Actual Flow Equation:

 $A_F = 0.0044$ (Q) (MTBC) (for calculations based on "actual flows")

Design Flow Equation:

A_F = 0.002 (Q) (MTBC) (for calculations based on "design flow" as defined above)

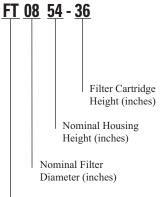
If a kitchen garbage disposal is used, more frequent filter maintenance may be required, due to the additional solids loading. Kitchen garbage disposals contribute an additional 36% (approximately) to the level of solids loading. Increasing the filter area by 36% gives better approximations for sizing and cleaning frequencies when garbage disposals are used.

Sizing filters for systems larger than single family dwellings is more complicated. For systems larger than single family dwellings, utilizing proper tankage and not exceeding residential strength wastewater, filter sizing using the given equations is valid. Systems having less than three times the daily design flow in storage require more conservative filter sizing to prevent the need for frequent cleaning.

*Orenco's effluent filter performance data is so extensive that Dr. George Tchobanoglous, co-author of <u>Small and Decentralized Wastewater</u> <u>Management Systems</u>, used that data to help develop his findings on effluent filters. Wastewater from restaurants, industrial plants, and other higher waste strength sources needs more detailed analysis of the wastewater characteristics for proper tank and filter sizing and configurations. Multiple filters may be required. Please call to discuss these applications.

Model Nomenclature

Example:



Biotube Effluent Filter Designation

Modulating Orifices and Peak Flows

Effluent filters must also be able to handle situations in which the majority of the daily flow will enter the septic tank over a relatively short period of time. Modulating plates with orifices are often used to limit the flow rate through a tank during peak flow to prevent the flushing out of solids. However, modulating plates and orifices should be used only when the tank has sufficient surge capacity. Simple high liquid level alarms can be added to any Orenco effluent filter.

Filter Surface Area vs. Flow Area

When comparing filters, be sure to note how filter area is being reported. It's important to compare both the Total Filter Surface Area and the Total Flow Area, because *Flow Area is as important as Filter Surface Area.* The surface area of a filter is important, because that's where solids are caught. But the flow area (the area of the "holes" in the filter) is equally important, because that's what prevents the filter from premature clogging.

Selecting A Biotube® Effluent Filter

Filter and Flow Area Chart								
Series	Filter Area (ft²)	Flow Area (ft²)						
FT15-36	50.5	15.2						
FT12-36	30.0	9.0						
FT08-36	14.6	4.4						
FT04-36	5.1	1.5						

Design Example:

A 12-unit condominium has a "design flow" of 3600 gallons per day (12 units at 300 gallons per day per unit). If a minimum 3year cleaning frequency is desired, how much filter area is necessary? Which Biotube Effluent Filter should be selected?

Answer: In this case, the equation for design flow is applicable.

Therefore, $A_F = (0.002)(3600)(3) = 21.6 \text{ ft}^2$

Referring to the Filter and Flow Area Chart, an FT1200 Series filter, with a filter area of 30.0 ft^2 , is required to satisfy the minimum design criteria.

Using the 30 ft² filter area, the design flow equation can be solved for MTBC, giving a cleaning frequency of 4.2 years.

MTBC = 30.0/(3600)(0.002) = 4.2 years.

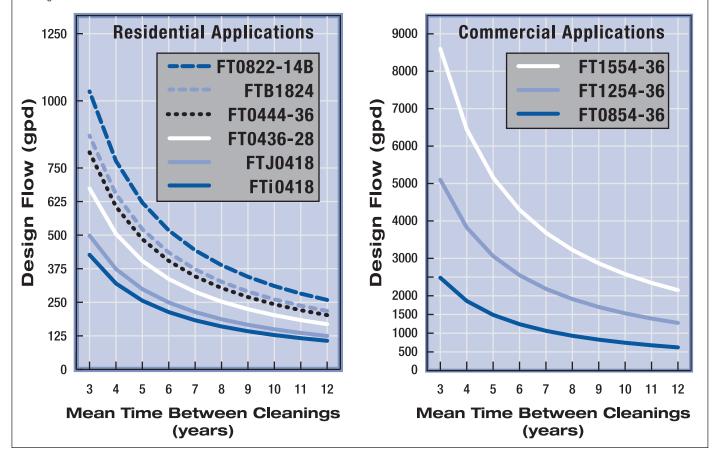
If the units will include garbage grinders, the filter area is increased by 36% to account for additional solids loading.

Therefore, $A_F = (1.36)(21.6) = 29.4 \text{ ft}^2$ And MTBC = 30.0/(3600)(0.002)(1.36) = 3.1 years.

Sizing Biotube[®] Effluent Filters

FIGURE 4. SIZING BIOTUBE EFFLUENT FILTERS

These charts show the relationship between Biotube filter size (diameter), design flow, and mean time between cleanings. The larger the filter and the smaller the flow, the longer you can go between cleanings. For example, a typical three-year cleaning frequency would require an 8-in. filter for up to 2,500 gpd, a 12-in. filter for up to 5,000 gpd, and a 15-in. filter for up to 8,500 gpd. Assumes a properly sized watertight tank and residential strength waste. See Orenco document *NDA-FT-FT-1* for more information.



HORSE CREEK HILLS SUBDIVISION

PROPOSED ROADWAY PROFILE LABEL KEY

WASTEWATER AND STORMWATER PLANS

LOCATION: N $\frac{1}{2}$, N $\frac{1}{2}$ of the SE $\frac{1}{4}$, & NE $\frac{1}{4}$ of the SW $\frac{1}{4}$, SEC 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MONTANA

LATITUDE: 46°29'45.6"	LONGITUDE: -111°31'13"
DEVELOPER: 71 RANCH L	.P
MARCH, 2020	SET NO.

PROJECT MANAGER: **DESIGN ENGINEER:** PROJECT SURVEYOR: GREG FINCK, PLS

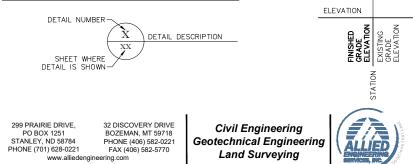
MARK FASTING, PE HUNTER MORRICAL, EI

SHEET INDEX

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WW0.2	PROPOSED IMPROVEMENTS
WASTEW	VATER DESIGN SHEETS
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WW1.2	HORSE CREEK HILLS 2 SUBDIVISION WASTEWATER TREATMENT SYSTEM PLAN
WW1.3	HORSE CREEK HILLS 3 SUBDIVISION WASTEWATER TREATMENT SYSTEM PLAN
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WW4.3	HORSE CREEK HILLS 2 SUBDIVISION POND GRADING DETAILS
WW4.4	HORSE CREEK HILLS 2&3 SUBDIVISION POND GRADING DETAILS
WW4.5	HORSE CREEK HILLS 3 SUBDIVISION POND GRADING DETAILS
WW4.6	HORSE CREEK HILLS 4 SUBDIVISION POND GRADING DETAILS
WW4.7	HORSE CREEK HILLS SUBDIVISION GENERAL STORM DETAILS
WW4.8	HORSE CREEK HILLS SUBDIVISION STORM CULVERT CROSS SECTIONS
WW4.9	HORSE CREEK HILLS SUBDIVISION STORM CULVERT CROSS SECTIONS

PLAN SHEET DETAIL CALLOUTS

DEQ Page 337



CL CMP CO CONC COB CY CLEAN OUT CONCRETE CITY OF BELGRADE CUBIC YARD DI DIA DUCTILE IRON DIAMETER DWG DRAWING

ALLIED ENGINEERING

BACK OF GRATE (GUTTER)

CORRUGATED METAL PIPE

SERVICES, INC.

AVENUE

BUILDING

BENCHMARK

CENTERLINE

AESI

AC AVE

BLDG

BOG

EA EG ELEV EOG EOP	EAST EACH EXISTING GRADE ELEVATION EDGE OF GRAVEL EDGE OF PAVEMENT EXISTING
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	GALLONS PER MINUTE GATE VALVE
HORZ HP	HIGH DENSITY POLYETHYLENE HORIZONTAL HIGH POINT HIGHWAY
	INVERT ELEVATION INCH INVERT
LP	LINEAR FEET LOW POINT LEFT



AERIAL MAP 2 000 4.000 6,000

SCALE (FEET)

CIVIL ABBREVIATIONS:

MA

MI

R0 R1

SC SD SE SG

Sì

ТВ ТВ

UC

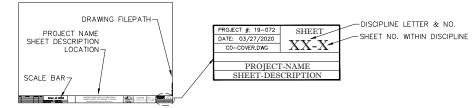
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SP DW	RADIUS RADIUS POINT REINFORCED CONCRETE PIPE RIGHT-OF-WAY RIGHT
CH CCT	SOUTH SCHEDULE STORM DRAIN SECTION SUBGRADE SANITARY SEWER MAIN SANITARY SEWER SERVICE STRET STATION STANDARD SQUARE YARD
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3	UNDERGROUND
RT	VERTICAL
/ /0	WATER MAIN WEST WITH WITHOUT WATER SERVICE

LEGEND

•	FOUND MONUMENT
<u>A</u>	CONTROL POINT
1235	EX. MAJOR CONTOUR (5' II
	EX. MINOR CONTOUR (1' IN
	EX. EDGE OF ROAD
	EX. DRAINAGE CULVERT
— x — x —	EX. FENCE
	EX. TREE ROW
***	EX. PINE TREE
W	EX. WATER MAIN
GV	EX. GATE VALVE
ЪС,	EX. FIRE HYDRANT
Ŵ	EX. WELL
S	EX. SEWER MAIN
S	EX. SEWER MANHOLE
OHP	EX. OVERHEAD POWER LINE
	EX. OVERHEAD POWER POL
	EX. ELECTRIC METER
—— F ——	EX. UNDERGROUND FIBER (
	EX. TELEPHONE/FIBER OPT
	AESI

PROPERTY LINE

FOUND MONUMENT



- AVAILABILITY

- INTERFERE WITH THE WORK.
- PRACTICABLE.

- REQUIREMENTS ARE MET.
- BLOCKS, ETC.), THAT ARE NOT SHOWN ON THESE PLANS.

HORSE	CREEK	HILLS	SUBDIVISION
	WWO.O	COVER	SHEET

CONTAMINATION, SEGREGATION, AND PARTICLE BREAKDOWN. 22. CARRY OUT COVERAGES OF COMPACTION EQUIPMENT SO THAT THE COMPACTIVE EFFORT IS DISTRIBUTED UNIFORMLY AND IN A SYSTEMATIC MANNER OVER THE ENTIRE LIFT. 23. ALL CONSTRUCTION ASSUMES A STABLE COMPACTED SUBGRADE IS ACHIEVED PRIOR TO PLACEMENT OF NEW FACILITIES. 24. COORDINATE WITH UTILITY COMPANIES REGARDING ALL UTILITY CROSSINGS AND ANY POTENTIAL UTILITY CONFLICTS.

25. CONTRACTOR SHALL COORDINATE DRY UTILITY CONDUIT LOCATIONS, DEPTHS, MATERIAL, QUANTITY, ETC. WITH APPLICABLE UTILITY SERVICE PROVIDERS PRIOR TO CONSTRUCTION.

26. IF APPLICABLE, CONTRACTOR SHALL BE RESPONSIBLE FOR ENSURING THAT ALL STORM WATER POLLUTION PREVENTION PLAN (SWPPP)

27. PROJECT SITE DEVELOPMENT MAY REQUIRE ADDITIONAL STORM WATER FACILITY IMPROVEMENTS (SWALES, PONDS, ROADSIDE DITCH

PROPOSED MAJOR CONTOUR (5' INTERVAL) -1235-INTERVAL) -1234 PROPOSED MINOR CONTOUR (1' INTERVAL) NTERVAL) PROPOSED ROAD CENTERLINE PROPOSED CURB AND GUTTER PROPOSED SIDEWALK PROPOSED WATER MAIN PROPOSED WATER SERVICE Ň PROPOSED GATE VALVE Ç, PROPOSED FIRE HYDRANT PROPOSED SEWER MAIN PROPOSED SEWER FORCE MAIN FM PROPOSED SEWER SERVICE ഭ PROPOSED SEWER MANHOLE PROPOSED STORM DRAIN LINE SD PROPOSED STORM DRAIN CURB INLET PROPOSED DRAINAGE CULVERT PROPOSED DRAINAGE DIRECTION OPTICS LINE PROPOSED DRAINAGE ARROW PROPOSED SIGN POST TICS PEDESTAL

PROPOSED LOT LINE

PROPOSED RIGHT-OF-WAY LINE

ROAD DESIGN

- NOISIVIGUN -

HORSE CREEK HILLS

STANDARD BORDER FORMAT

GENERAL NOTES AND SPECIFICATIONS:

1. THE CONTRACTOR MUST ADHERE TO THE PROJECT PLANS AND SPECIFICATIONS. THE CONSTRUCTION COMPANY MUST BE A LICENSED CONTRACTOR WITH THE STATE OF MONTANA AND BE COVERED BY LIABILITY INSURANCE. A TWO-YEAR WRITTEN WARRANTY FROM THE PROJECT CONTRACTOR TO GALLATIN COUNTY IS REQUIRED FOR ALL ONSITE AND OFFSITE ROAD IMPROVEMENTS THE CONTRACTOR WILL BE RESPONSIBLE FOR LOCATING ALL UNDERGROUND UTILITIES BY CALLING THE NATIONAL 811 "CALL BEFORE YOU DIG" TELEPHONE NUMBER PRIOR TO CONSTRUCTION ACTIVITIES.

YOU DIG" TELEPHONE NUMBER PRIOR TO CONSTRUCTION ACTIVITES. ALL ROAD AND STORM DRAINAGE IMPROVEMENTS SHALL BE CONSTRUCTED PER THE ALIGNMENT AND GRADE AS SHOWN ON THE PLANS. CONTRACTOR SHALL FIELD VERIFY LOCATION AND DEPTH OF ALL EXISTING UTILITIES AND STRUCTURES WHERE NEW FACILITIES CROSS OR CONNECT. CONTRACTOR SHALL BE RESPONSIBLE FOR EXPOSING POTENTIAL UTILITY CONFLICTS FAR ENOUGH AHEAD OF CONSTRUCTION TO MAKE NECESSARY GRADE MODIFICATIONS WITHOUT DELAYING THE WORK. ALL UTILITY CROSSINGS SHALL BE POTHOLED OR VACUUMED AS NECESSARY PRIOR TO EXCAVATING OR BORING TO ALLOW THE CONTRACTOR TO PREVENT GRADE OR ALIGNMENT

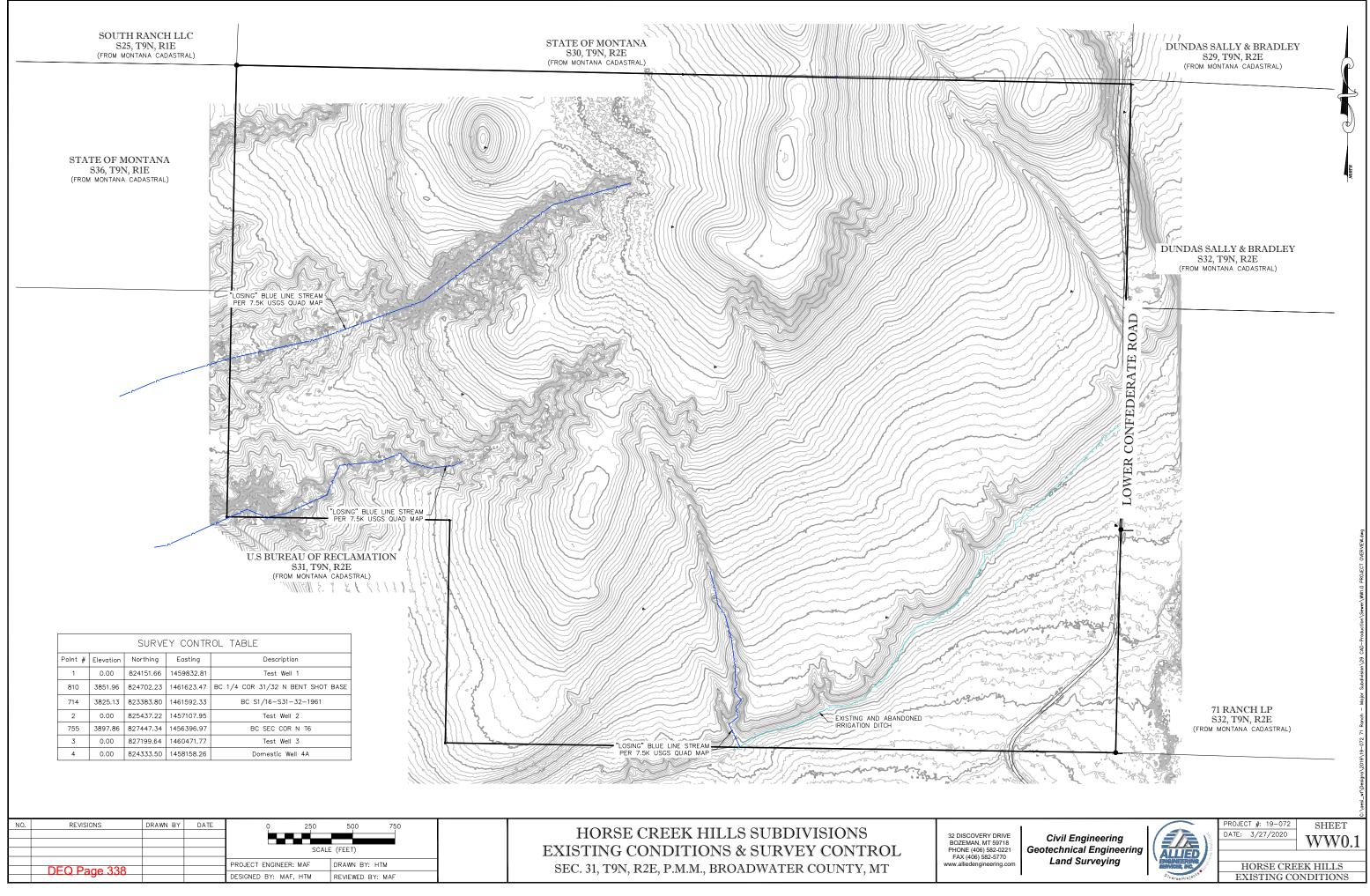
CONFLICTS. AT LEAST 10 BUSINESS DAYS BEFORE BEGINNING ANY EXCAVATION, THE CONTRACTOR SHALL NOTIFY THE OWNER AND ENGINEER OF UNDERGROUND FACILITIES AND COORDINATE THE WORK WITH THE OWNERS OF SUCH UNDERGROUND FACILITIES. THE INFORMATION SHOWN OR INDICATED IN THE CONTRACT DOCUMENTS WITH RESPECT TO EXISTING UNDERGROUND FACILITIES. THE INFORMATION AND DATA OBTAINED FROM THE OWNERS OF THE FACILITIES WITHOUT FIELD EXPLORATION, AND AS SUCH, OWNER AND ENGINEER ARE NOT RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF SUCH INFORMATION OR DATA. NO TRENCHES IN ROADS OR DRIVEWAYS SHALL BE LEFT IN AN OPEN CONDITION OVERNIGHT. ALL SUCH TRENCHES SHALL BE BACKFILLED, COMPACTED AND CLOSED BEFORE THE END OF EACH WORK DAY AND NORMAL TRAFFIC FLOWS RESTORED. 7. IF THE ENGINEER IS CONTRACTED FOR CONSTRUCTION STAKING, ENGINEER SHALL BE CONTACTED PRIOR TO STAKING. PROVIDE ADVANCED NOTICE SUFFICIENT TO ACCOMMODATE CONSTRUCTION, <u>Z WORKING DAYS IS MINIMUM</u>, AND MAY VARY DEPENDING UPON AVAILABILITY.

AVAILABILITY. LIGHTING, ELECTRICAL, NATURAL GAS, COMMUNICATIONS, LANDSCAPING, ETC. ARE TO BE DESIGNED BY OTHERS. FINAL QUANTITIES MAY BE HIGHER OR LOWER THAN THOSE ESTIMATED, PENDING FIELD FINDINGS, SITE CONDITIONS, ETC.). STRIP THE EMBANKMENT FOUNDATION AREA, BORROW AREAS AND ALL AREAS TO RECEIVE FILL TO A MINIMUM DEPTH OF 6 INCHES AND AS REQUIRED TO REMOVE ALL ORGANIC SOILS, VEGETATIVE MATTER, ROOTS, AND OTHER PERISHABLE, LOOSE OR OBJECTIONABLE MATERIAL INCLUDING FROZEN SOIL THAT MIGHT INTERFERE WITH COMPACTION OF EMBANKMENT LIFT OR THE BONDING OF EMBANKMENT TO FOUNDATION. OBJECTIONABLE MATERIAL WILL BE AS DETERMINED BY THE ENGINEER. PERFORM STRIPPING OPERATIONS IN A MANNER TO CONSERVE ALL TOPSOIL THAT CONTAINS ORGANICS. . TRANSPORT STRIPPED MATERIALS TO STOCKPILE AREAS UJUSIDE OF WATERWAYS AND WETLANDS, SUBJECT TO APPROVAL. COORDINATE WITH OWNER TO IDENTIFY STOCKPILE AREAS. LOCATE PILES SO AS NOT TO AFFECT THE OPERATION OF THE EXISTING OPERATIONS, OR INTERFERFE WITH THE WORK

TAKE PRECAUTIONS TO PRESERVE, IN A SOUND CONDITION, THE MATERIAL BELOW AND BEYOND THE LINES OF ALL EXCAVATIONS. PERFORM OPERATIONS SO THAT THE EXCAVATIONS WILL YIELD AS MUCH SUITABLE MATERIAL FOR CONSTRUCTION PURPOSES AS

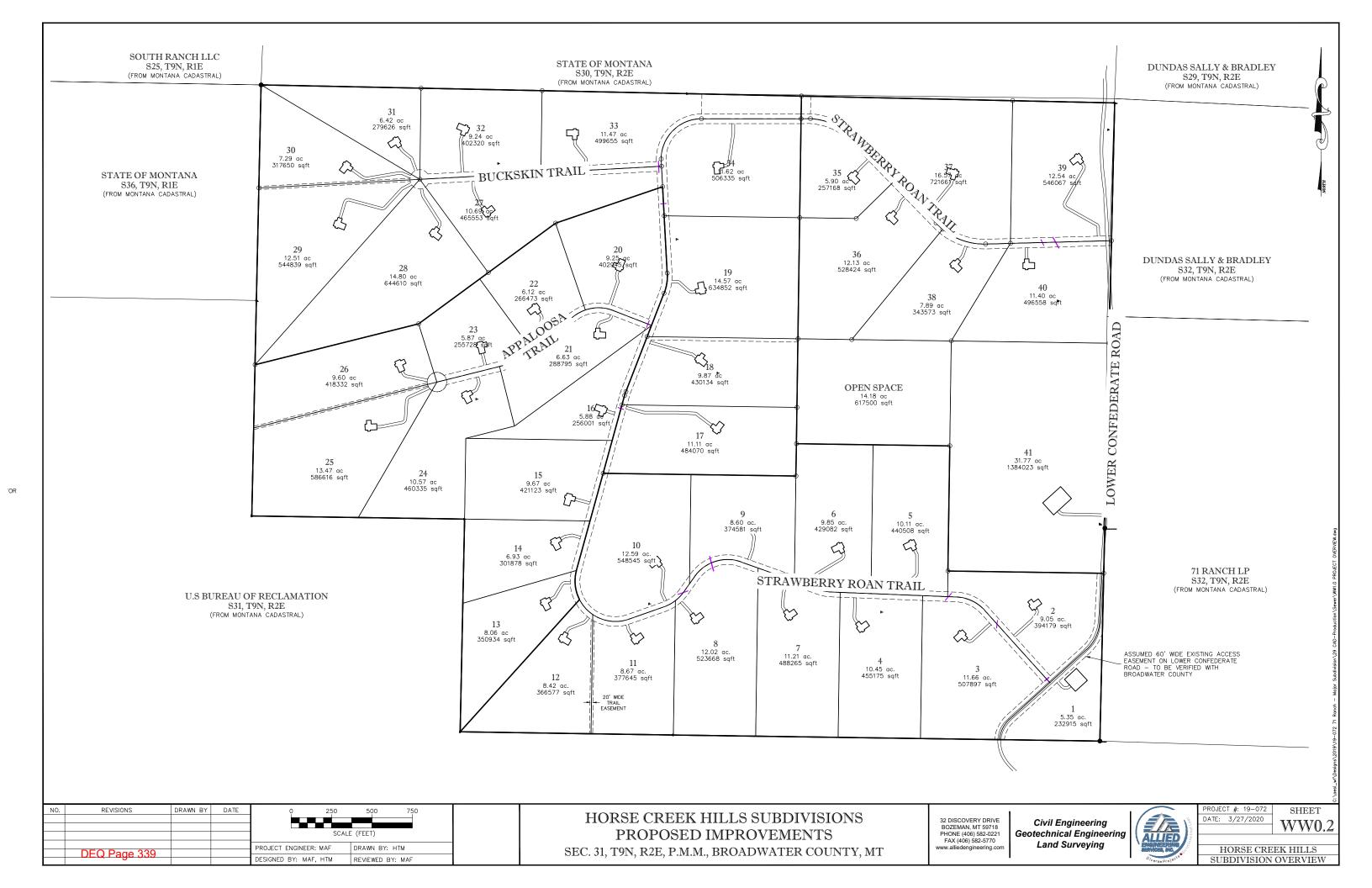
TACTICABLE. 14. REUSE, AS MUCH AS IS PRACTICABLE, ALL SUITABLE MATERIALS FROM REQUIRED EXCAVATION IN THE PERMANENT CONSTRUCTION.

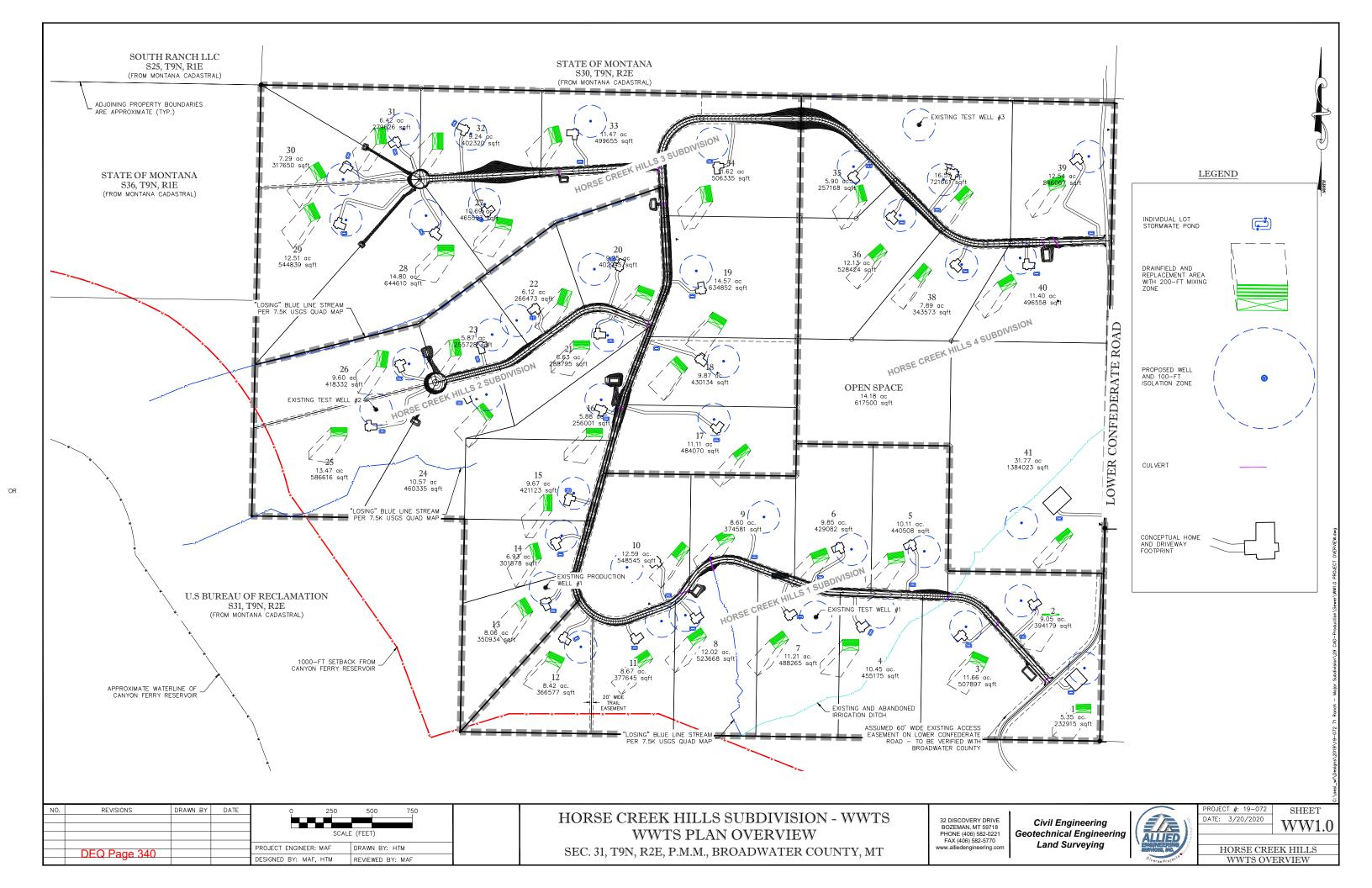
REUSE, AS MUCH AS IS PRACTICABLE, ALL SUITABLE MATERIALS FROM REQUIRED EXCAVATION IN THE PERMANENT CONSTRUCTION. SEPARATE UNSUITABLE MATERIALS AND REMOVE THEM FROM THE WORK AREA AS SOON AS PRACTICABLE.
 SPREAD OUT AND ALLOW MATERIALS TO DRY THAT ARE TOO WET FOR IMMEDIATE COMPACTION UNTIL THE WATER CONTENT IS REDUCED SUFFICIENTLY FOR PLACEMENT IN THE EMBANKMENT. AERATING AND DRYING IS INCIDENTAL TO THE WORK.
 WATER-CONDITION MATERIALS THAT ARE TOO DRY FOR IMMEDIATE COMPACTION. MOISTURE CONDITIONING IS INCIDENTAL TO THE WORK.
 WATER-CONDITION MATERIALS THAT ARE TOO DRY FOR IMMEDIATE COMPACTION. MOISTURE CONDITIONING IS INCIDENTAL TO THE WORK.
 WATER-CONDITION MATERIALS THAT ARE TOO DRY FOR IMMEDIATE COMPACTION. MOISTURE CONDITIONING IS INCIDENTAL TO THE WORK.
 DE-WATER AS NECESSARY TO PREVENT THE ACCUMULATION AGAINST OR THE INTERMINGLING OF WATER WITH THE FILL.
 PERFORM EXCAVATION AND PLACEMENT OPERATIONS SUCH THAT THE EMBANKMENT MATERIALS ARE MIXED AND BLENDED TO PROVIDE THE MOST HOMOGENEOUS SECTION AND BEST DEGREE OF COMPACTION AND STABILITY PRACTICAL. ALL FILL SHOULD BE PLACED IN HORIZONTAL LIFTS AND COMPACTED TO AT LEAST 95% OF ASTM D-698. PROVIDE PRIMARY WATER CONDITIONING, MIXING AND BLENDING IN STOCKPILES AS NEEDED. DISTRIBUTE THE FILL IN A LIFT SUCH THAT IT IS FREE FROM LENSES, POCKETS, STREAKS, OR LAYERS DIFFERING MATERIALLY IN TEXTURE OR GRADATION FROM THE SURROUNDING FILL.
 CONTROL AND CONDUCT ALL TRANSPORTING, STOCKPILING, EXCAVATION, PRODUCTION, AND PLACEMENT OPERATIONS TO MINIMIZE CONTAMINATION, SEGREGATION, AND PARTICLE BREAKDOWM.
 CONTROL AND CONDUCT ALL TRANSPORTING, STOCKPILING, EXCAVATION, PRODUCTION, AND PLACEMENT OPERATIONS TO MINIMIZE CONTAMINATION, SEGREGATION, AND PARTICLE BREAKDOWM.
 CONTROL AND CONDUCT ALL TRANSPORTING STOCKPILING SO THAT THE COMPACTIVE EFFORT IS DISTRIBUTED UNIFORMLY AND IN A

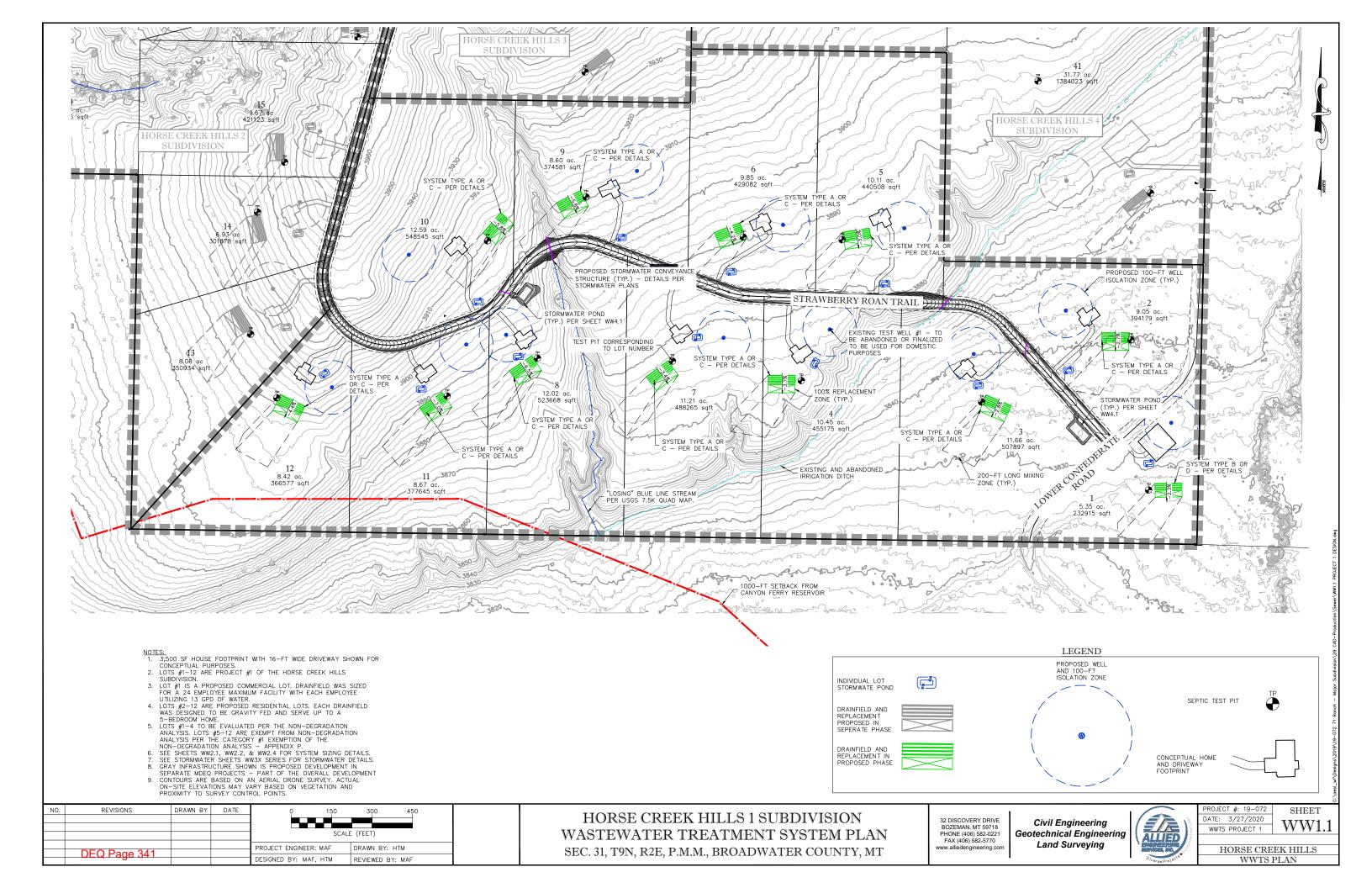


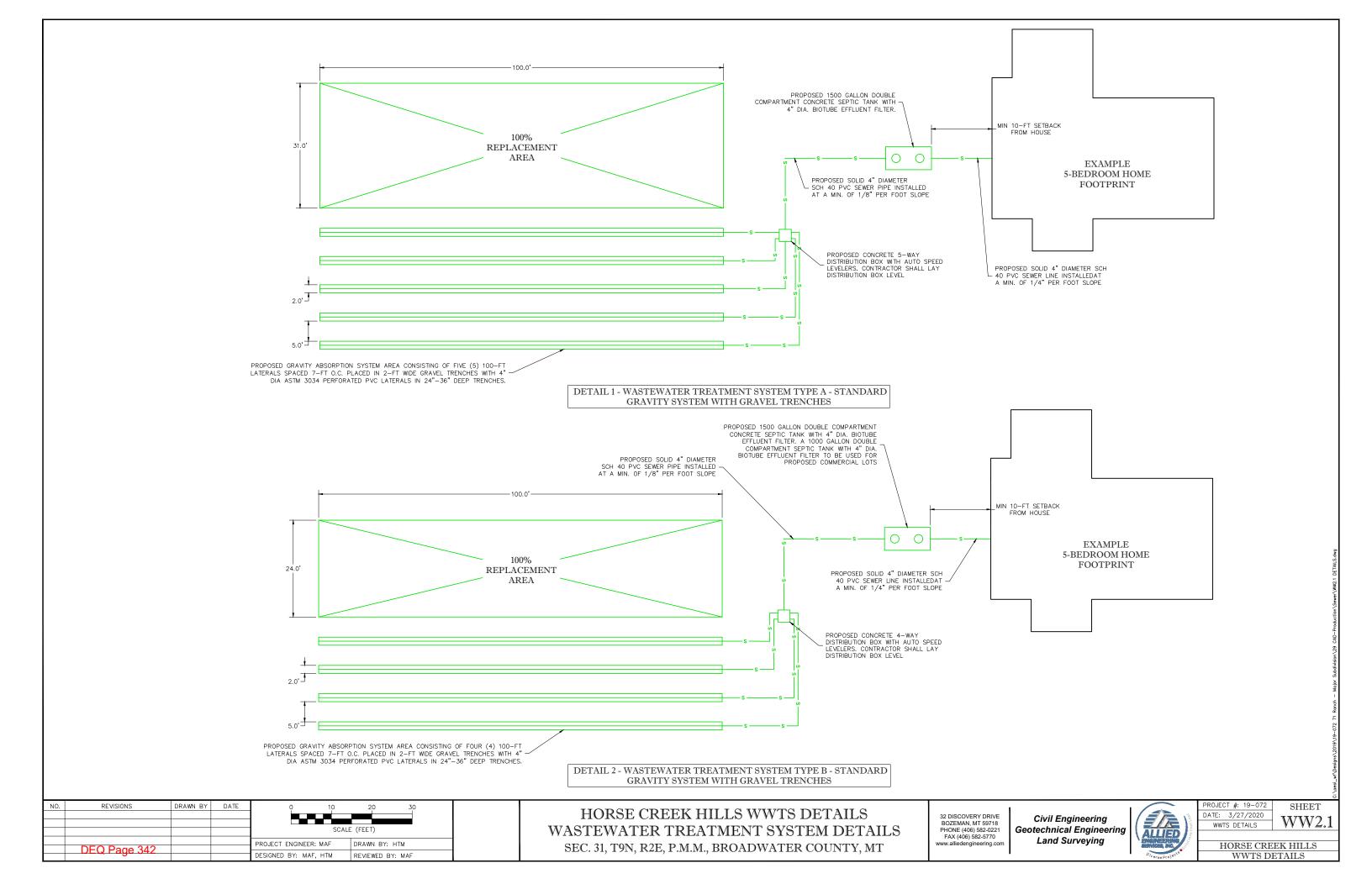
		SCALE	E (FEET)	
		PROJECT ENGINEER: MAF	DRAWN BY: HTM	
EQ Page 338		DESIGNED BY: MAF, HTM	REVIEWED BY: MAF	

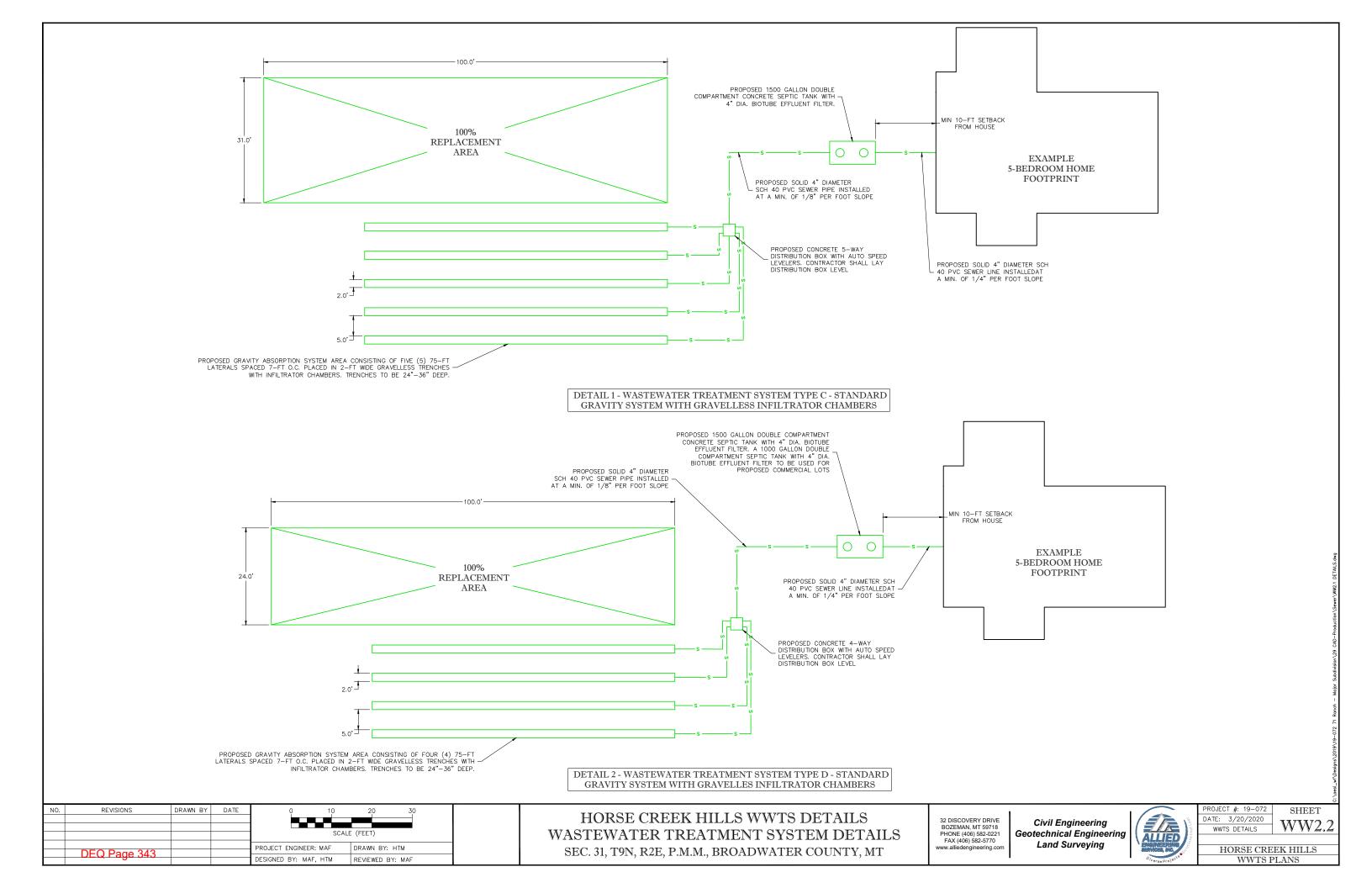
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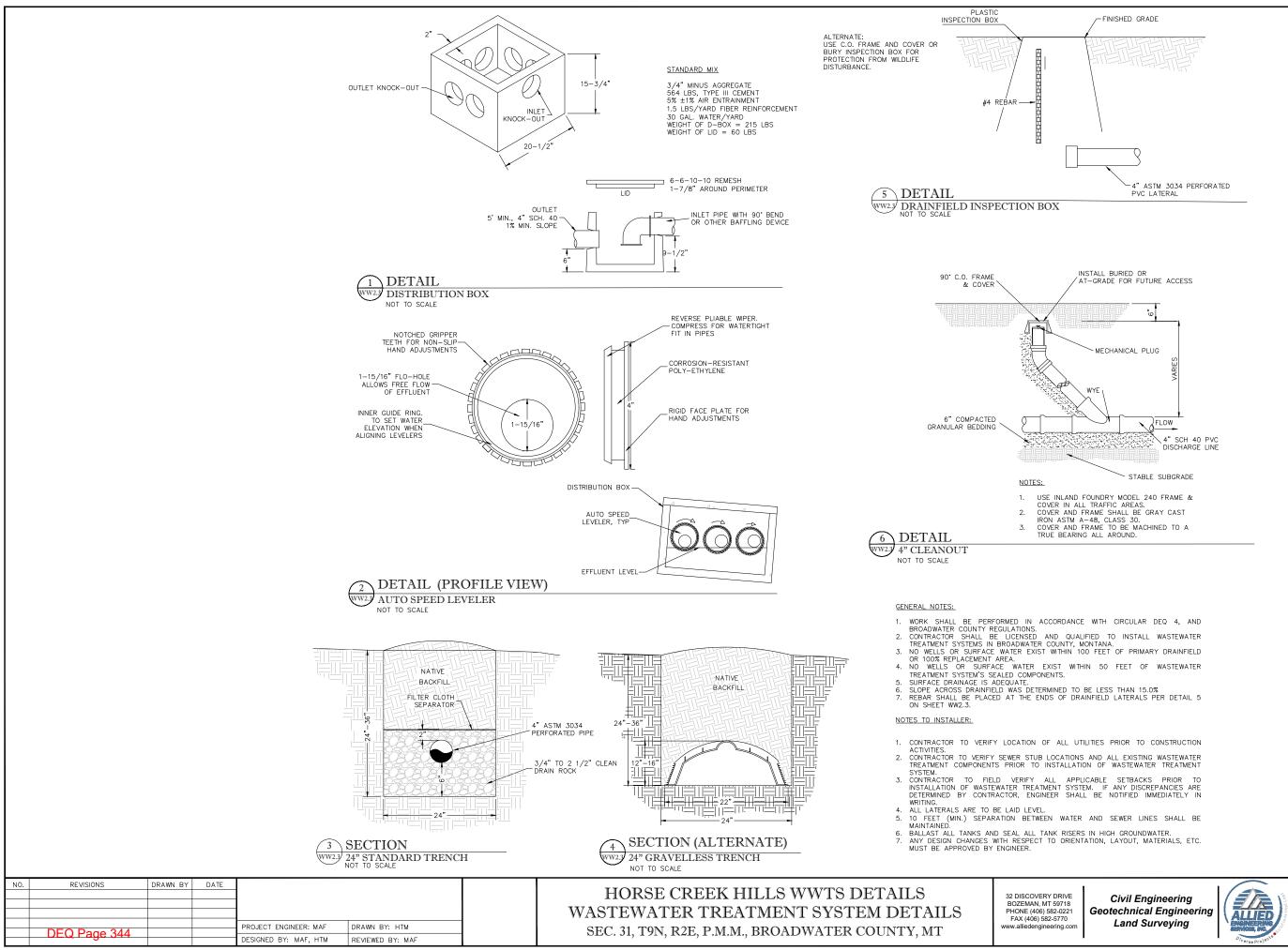




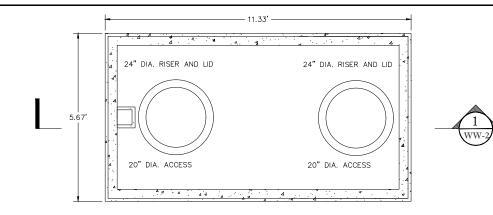








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ROJECT #: 19-072	SHEET
ATE: 3/20/2020	1171177 2
WWTS DETAILS	WW2.3
HORSE CRE	EK HILLS
WWTS I	PLANS



24 HOURS

OR

TANK MUST BE REJECTED.

*INSTALL SAFETY GRATES AT ALL SEPTIC TANK/DOSING TANK OPENINGS. CUT TO FIT AROUND EFFLUENT FILTER HANDLE AND PUMP DISCHARGE PIPING (IF NECESSARY).

<u>ALTERNATE</u> *OWNER MAY INSTALL FIBERGLASS RISERS AND LIDS IN LIEU OF CONCRETE. RISERS AND LIDS (TYPICAL ALL TANKS)

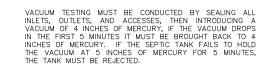
*PRIOR TO PLACEMENT OF TANKS CONTACT ENGINEER IF TANK DEPTHS ARE ANTICIPATED TO EXCEED 4' BURY DEPTH.

MDEQ4 5.1.2.1.:

NOT TO SCALE

DEQ Page 345

LIQUID CONNECTION BETWEEN COMPARTMENTS SHALL CONSIST OF A SINGLE OPENING COMPLETELY ACROSS THE COMPARTMENT WALL OR TWO OR MORE OPENINGS EQUALLY SPACED ACROSS THE WALL THE TOTAL AREA OF THE OPENINGS SHALL BE AT LEAST THREE TIMES THE AREA OF THE INLET PIPE.



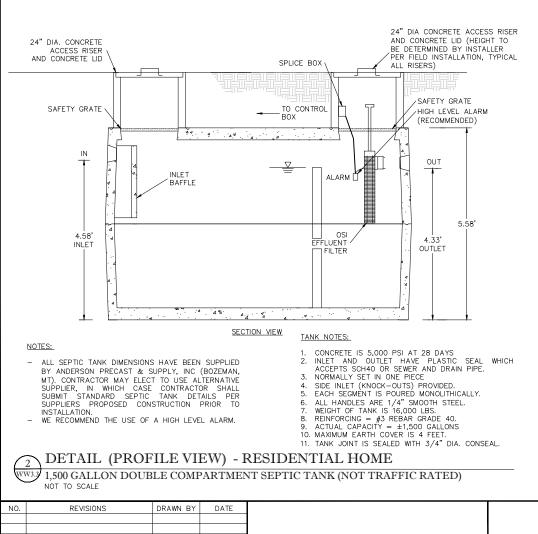
ALL SEPTIC AND DOSING TANKS MUST BE TESTED IN ACCORDANCE WITH MDEQ4 CHAPTER 5 FOR WATERTIGHTNESS.

WATER TESTING MUST BE CONDUCTED BY SEALING THE OUTLETS, FILLING THE SEPTIC TANK TO ITS OPERATIONAL LEVEL, AND ALLOWING THE TANK TO STAND FOR AT LEAST 24 HOURS. IF THERE IS A MEASURABLE LOSS (2 INCHES DEPENDENT OF THE TANK TO STAND FOR ALL AND THE

OR MORE), REFILL THE TANK AND LET STAND FOR ANOTHER

IF THERE IS AGAIN A MEASURABLE LOSS, THE



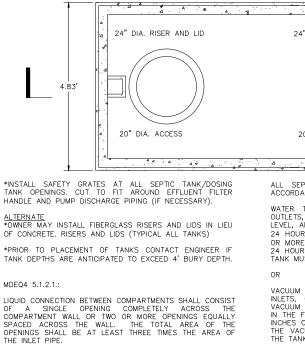


PROJECT ENGINEER: MAF

DESIGNED BY: MAF, HTM

DRAWN BY: HTM

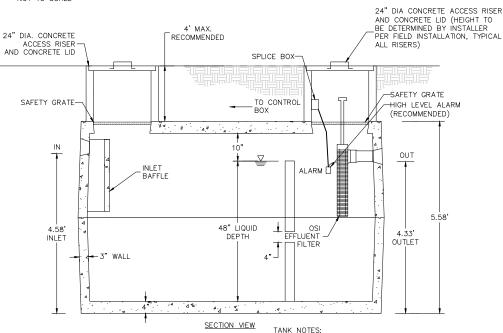
REVIEWED BY: MAF



9.25

3 DETAIL (PLAN VIEW) - COMMERCIAL SHOP WW24 1,000 GALLON DOUBLE COMPARTMENT SEPTIC TANK (NOT TRAFFIC RATED)





10.	TES:
_	ALL SEPTIC TANK DIMENSIONS HAVE BEEN SUPPLIED BY ANDERSON PRECAST & SUPPLY, INC (BOZEMAN, MT). CONTRACTOR MAY ELECT TO USE ALTERNATIVE SUPPLIER, IN WHICH CASE CONTRACTOR SHALL SUBMIT STANDARD SEPTIC TANK DETAILS PER SUPPLIERS PROPOSED CONSTRUCTION PRIOR TO INSTALLATION. WE RECOMMEND THE USE OF A HIGH LEVEL ALARM. SHALL BE DOUBLE COMPARTMENT

(PROFILE VIEW) - COMMERCIAL SHOP

WW24 1,000 GALLON DOUBLE COMPARTMENT SEPTIC TANK (NOT TRAFFIC RATED)

NOT TO SCALE

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HORSE CREEK HILLS WWTS DETAILS WASTEWATER TREATMENT SYSTEM DETAILS SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT

32 DISCOVERY DRIVE BOZEMAN, MT 59718 PHONE (406) 582-0221 FAX (406) 582-5770 www.alliedengineering.co





ALL SEPTIC AND DOSING TANKS MUST BE TESTED IN ACCORDANCE WITH MDEQ4 CHAPTER 5 FOR WATERTIGHTNESS

WATER TESTING MUST BE CONDUCTED BY SEALING THE OUTLETS, FILLING THE SEPTIC TANK TO ITS OPERATIONAL LEVEL, AND ALLOWING THE TANK TO STAND FOR AT LEAST 24 HOURS. IF THERE IS A MEASURABLE LOSS (2 INCHES OR MORE), REFILL THE TANK AND LET STAND FOR ANOTHER 24 HOURS. IF THERE IS AGAIN A MEASURABLE LOSS, THE TANK MUST BE REJECTED.

VACUUM TESTING MUST BE CONDUCTED BY SEALING ALL INLETS, OUTLETS, AND ACCESSES, THEN INTRODUCING A VACUUM OF 4 INCHES OF MERCURY, IF THE VACUUM DROPS IN THE FIRST 5 MINUTES IT MUST BE BROUGHT BACK TO 4 INCHES OF MERCURY. IF THE SEPTIC TANK FAILS TO HOLD THE VACUUM AT 5 INCHES OF MERCURY FOR 5 MINUTES, THE TANK MUST BE REJECTED

CONCRETE IS 5,000 PSI AT 28 DAYS INLET AND OUTLET HAVE PLASTIC SEAL ACCEPTS SCH40 OR SEWER AND DRAIN PIPE. SEAL WHICH NORMALLY SET IN ONE PIECE SIDE INLET (KNOCK-OUTS) PROVIDED. EACH SEGMENT IS POURED MONOLITHICALLY. EACH SEGMENT IS POURED MONOLIHICAL
 ALL HANDLES ARE 1/4" SMOOTH STEEL.
 WEIGHT OF TANK IS 10,500 LBS.
 REINFORCING = #3 REBAR GRADE 40.
 ACTUAL CAPACITY = ±1,000 GALLONS
 MAXIMUM EARTH COVER IS 4 FEET. 11. TANK JOINT IS SEALED WITH 3/4" DIA. CONSEAL.



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PROJECT #: 19-072	SHEET
DATE: 3/20/2020	3373370 4
WWTS DETAILS	WW2.4
HORSE CRE	EK HILLS
WWTS I	PLANS

SUMMARY OF PROPOSED WASTEWATER TREATMENT TYPE CORRESPONDING TO EACH LOT

Lot Numer	# of Bedrooms	GPD of	Texture	Application Rate	Corresponding Percolation Rate	Min. Drainfield	Length of	Min. Drainfield	Infiltrator Size	Min. Drainfield	-	Min. Drainfield	ISVSTem to hel
Lot Numer	# Of Dedioonins	Wastewater	Texture	(gpd/ft^2)	(min/inch)	Area (sf)	Lateral (LF)	Dimensions (ft)	Reduction	Area (sf)	Lateral (LF)	Dimensions (ft)	Utilized
1	24 Employees	312	SiL	0.4	16 - <31	780	390	23 X 100 (Type B)	0.75	585	292.5	23 x 75 (Type D)	BorD
2	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
3	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
4	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
5	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
6	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
7	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
8	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
9	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
10	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
11	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	A or C
12	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
13	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
14	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)	0.75	600	300	23 x 75 (Type D)	
15	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)		600	300	23 x 75 (Type D)	
16	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)	0.75	600	300	23 x 75 (Type D)	
17	5	400	L	0.5	10 - <16	800	400	23 X 100 (Type B)	0.75	600	300	23 x 75 (Type D)	
18	5	400	L	0.5	10 - <16	800	400	23 X 100 (Type B)		600	300	23 x 75 (Type D)	
19	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
20	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
21	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)	0.75	600	300	23 x 75 (Type D)	1
22	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
23	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
24	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	0.75	750	375	30 x 75 (Type C)	
25	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)	0.75	600	300	23 x 75 (Type D)	
26	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
27	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
28	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
29	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
30	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	1
31	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
32	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
33	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	1
34	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	1	750	375	30 x 75 (Type C)	
35	5	400	SL	0.5	10 - <16	800	400	23 X 100 (Type B)		600	300	23 x 75 (Type D)	1
36	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)	1	750	375	30 x 75 (Type C)	1
37	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
38	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
39	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
40	5	400	SiL	0.4	16 - <31	1000	500	30 x 100 (Type A)		750	375	30 x 75 (Type C)	
41	24 Employees	312	SiL	0.4	16 - <31	780	390	23 X 100 (Type B)		585	292.5	23 x 75 (Type D)	

1 DETAIL WW2.5 SUMMARY OF DRAINFIELD DIMENSIONS NOT TO SCALE

NO.	REVISIONS	DRAWN BY	DATE		
				PROJECT ENGINEER: MAF	DRAWN BY: HTM
	DEQ Page 346			DECIONED DY, MAE UTM	DEVENED DV NAS
	0			DESIGNED BY: MAF, HTM	REVIEWED BY: MAF

HORSE CREEK HILLS WWTS DETAILS WASTEWATER TREATMENT SYSTEM SUMMARY SEC. 31, T9N, R2E, P.M.M., BROADWATER COUNTY, MT

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ROJECT #: 19-072	SHEET
ATE: 3/20/2020	
WWTS DETAILS	WW2.5
HORSE CREEK HILLS	
WWTS PLANS	



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